



Performance-based plastic design of steel plate shear walls



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ARTICLE INFO

Article history:

Received 15 April 2013

Accepted 19 July 2013

Available online 25 August 2013

Keywords:

Steel plate shear wall

Performance-based design

Inelastic deformation capacity

Ductility-based design

P-Delta effects

ABSTRACT

The existing codes and design guidelines for steel plate shear walls (SPSWs) fail to utilise the excellent ductility capacity of SPSW systems to its fullest extent, because these methods do not consider the inelastic displacement demand or ductility demand as their design objective. A performance-based plastic design method for SPSW systems with rigid beam-to-column connections is proposed in this work, which sets a specific ductility demand and a preferred yield mechanism as its performance targets. The effectiveness of the proposed method in achieving these targets is illustrated through sample case studies of four- and eight-storey SPSW systems for varied design scenarios. A comparison with the existing AISC method for the same design scenario shows that the proposed method consistently performs better, in achieving these performance-based targets. The proposed method is modified to account for P-Delta effects, wherever necessary. This modified method is found to be more effective than the original proposal, whenever P-Delta effects are significant.

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1. Existing design provisions for steel plate shear walls

During the 1980s and 1990s, a significant amount of research works, both 'analytical' and 'experimental', was conducted on the post-buckling behaviour of thin unstiffened steel plate shear wall (SPSW) systems [1]. These research works, conducted primarily in Canadian and U.S. universities (for example, [2–6]), resulted in the incorporation of design specifications for SPSW systems in design standards/codes. In 1994, the Canadian steel design standard [7] included design provisions for unstiffened thin SPSW, although only as an appendix to the main design code. The 2001 Canadian standard [8] incorporated mandatory clauses on the design of steel plate shear walls. This standard had provisions for both 'limited ductility' and 'ductile' steel plate shear walls. For the limited ductility SPSW, no special requirements were made for the beam-to-column connections and a response modification factor (R) of 2.0 was assigned for these systems. For the ductile SPSW, however, the beam-to-column connections had to be moment resisting and the response modification factor was higher ($R = 5.0$). In order to ensure a ductile failure mode for SPSW structures, this code recommended an indirect capacity design approach. In this approach, a factor B (ratio of the probable shear resistance at the base of the wall for a given plate thickness to the factored lateral force at the base of the wall, obtained from the calculated seismic load) was used to magnify the moments and axial forces in columns obtained from an elastic analysis. This magnification was not required if column forces and moments were obtained from a nonlinear pushover analysis.

Further research on SPSW systems in the last decade, particularly the plastic analysis and design methods for SPSW [9], resulted in newer design provisions, for example, as in the AISC Seismic Provisions [10,11] and the Canadian standard CAN/CSA S16 [8,12].

The AISC SPSW specifications followed the load and resistance factor design (LRFD) format based on the limit state of collapse. The concept of capacity design was incorporated in this standard. For example, all edge/boundary elements ('horizontal boundary elements/HBE' and 'vertical boundary elements/VBE') were designed to resist the maximum forces that could be generated by fully yielded steel 'infill panels'. These provisions also indicated to a preferred mechanism of failure through specifications, such as that the boundary elements were required to be proportioned in order to meet the 'strong-column-weak-beam' criterion, and that in boundary elements plastic hinging was permitted only at HBE ends. The recently published AISC Design Guide 20 for SPSW [13] developed the 2005 AISC Seismic Provisions into a complete design methodology. It included step-by-step design procedures as well as design examples for two types of steel plate shear walls: high-ductility SPSW (with $R = 7.0$) for high-seismic regions and low-ductility SPSW (with $R = 3.0$) for low seismic regions. This design guide was developed in accordance with the then existing relevant standards ASCE7-05 for minimum design loads in buildings [14], ANSI/AISC 360-05 for structural steel [15], and 2005 AISC Seismic Provisions [10].

Although elements of capacity design concepts were incorporated in the latest Canadian and U.S. steel design standards, there are a few limitations when assessed from a performance-based seismic design (PBSD) perspective

1. Significant inelastic deformation capacity (ductility) of SPSW systems cannot be fully utilised by these codes, as the design is primarily

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based on an elastic force/strength-based approach where the inelastic behaviour is implicitly accounted for through a response modification factor, R .

- These guides specify a desirable yield mechanism, however they do not provide specific design equations to attain this yield mechanism [16], especially for the VBE and HBE in the SPSW system.
- These standards do not provide the designer any option to choose a specific yielding hierarchy or failure mechanism for the SPSW structure.

In more recent times, Berman and Bruneau [17] proposed a reasonably accurate and relatively effective capacity design method for SPSW columns (VBE). Their procedure combined a linear elastic model of SPSW and plastic analysis concepts. Research works by [18–21] provided capacity design provisions for boundary beams (HBE) in SPSW systems. These design equations, especially those for ‘anchor beams’ (beams at roof and ground level with infill panels only at one side) were derived considering local collapse mechanism (‘beam mechanism’) with plastic hinges forming at the ends of the HBE and close to the mid-span of the HBE. Vian et al. [19] also recommended the use of ‘reduced beam section/RBS’ at the ends of the HBE to ensure the preferred failure mechanism of the AISC Seismic Provisions.

Over the last decade, the performance-based seismic design philosophy has emerged as a promising and efficient seismic design approach. PBSO explicitly accounts for the inelastic behaviour of a structural system in the design process itself. PBSO approaches based on plastic analysis and design concepts called as performance-based plastic design (PBSD) methods were recently developed for different lateral load resisting systems (such as steel moment resisting frames, steel braced frames, etc.) in the University of Michigan [22,23]. In these design methods a pre-selected yield/failure mechanism and a uniform target drift (based on inelastic behaviour) were considered as performance objectives. The analytical validation of these methods showed that structures designed using these methods were very effective in achieving the pre-selected performance objectives. Details of these methods and step-by-step procedures were later compiled in a book by Goel and Chao [24]. Considering a gradual shift towards PBSO for seismic design methods in general, Ghosh et al. [25] proposed a displacement/ductility-based design methodology for steel plate shear wall systems with pin-connected boundary beams. Similar to the methods developed in the University of Michigan, they also considered the target displacement ductility ratio and a pre-selected yield mechanism as the design criterion; and an inelastic energy balance concept was used in the formulation of the design method. Ghosh et al. validated this method by designing a four-storey SPSW with pin-connected beams subjected to various ground motion scenarios and for different target ductility ratios. Gupta et al. [26] successfully applied the inelastic displacement ductility-based method proposed by Ghosh et al. using standard hot rolled-sections (for boundary elements) available in the U.S. [15] and in India [27]. More recently, while investigating for a suitable (height-wise) distribution of the design base shear for this method, [28] applied this method effectively to SPSW with pin-connected beams of various heights.

2. Objective

Considering that the existing U.S. and Canadian design standards/guides for ‘ductile’ SPSW recommend the use of only rigid beam-to-column connections, an inelastic displacement-based seismic design method similar to that proposed by Ghosh et al. [25] needs to be formulated for SPSW systems with rigid beam-to-column connections. The primary objective of the work presented here, thus, is to develop a PBSD method for SPSW systems with rigid beam-to-column connections, with the following performance goals:

- achieving a target displacement ductility ratio demand considering the inelastic behaviour of the SPSW system, and
- achieving a pre-selected yield/failure mechanism for this inelastic behaviour.

It must be mentioned here that in order to develop a full-fledged PBSD framework for any structural system, the first important task is to define acceptable performance levels in a specific quantitative manner in terms of structural, non-structural and component behaviours. The focus of this work, however, is on the structural design calculations once a performance level is selected and limits are defined in terms of displacement-based quantities. Before we begin with the proposal of a PBSD method for SPSW, the existing design method (based on AISC Design Guide 20) is reviewed through a sample design case and it is checked if this sample design meets the stated performance objectives (Section 3). Section 4 provides the fundamentals and the framework of the proposed PBSD method for SPSW with rigid beam-to-column connections. This method is validated in Section 5 through sample designs of low-rise (four-storey) and medium-rise (eight-storey) SPSW buildings, for different target ductility ratios, and subjected to various earthquake scenarios. Results of this validation are discussed in detail, along with a comparison with the sample design based on existing AISC guidelines. A modification of the proposed PBSD method – to account for P-Delta effects (which are predominant for medium- and high-rise SPSW systems with large displacement ductility demands) – is provided in Section 6. Section 7 presents the significant conclusions of this work and also discusses the limitations thereof. It should however, be noted that the work presented here does not address the issue of formulating the design method in a probabilistic framework, which is the most significant feature for a PBSD methodology, other than the explicit consideration of inelastic behaviour and damage in a structure. We are currently engaged in developing a reliability-based framework for the performance-based plastic design method, which will be reported in future.

3. Design of a SPSW system following AISC Design Guide 20, and its performance assessment

To assess the seismic performance of a steel plate shear wall structure, which is designed following provisions of AISC Design Guide 20 [13], a four-storey steel plate shear wall building is considered. The configuration of this four-storey building is illustrated in detail in Fig. 1. The building has a five bay by six bay plan, with one SPSW bay along each outer frame. All beams, except those in the SPSW bays, are pin-connected (shear-connected) to the frame, and therefore only the SPSW frames form the lateral load resisting system. The building is assumed to have seismic weights of 4690 kN per floor, except for the roof, where it is 5090 kN. For seismic force calculations, this study building is assumed to be located in downtown San Francisco, CA, USA. The building site is categorised as Site Class D for ‘stiff soil’ and its occupancy category is adopted as

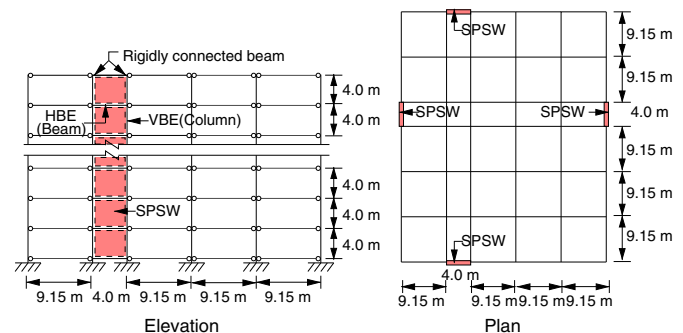


Fig. 1. Configuration of the hypothetical study building(s).

'I', based on its use as an office building. The site location and the soil characteristics considered here are the same as those of the design example II ('high-seismic' design) provided in AISC Design Guide 20 [13].

As mentioned earlier, the seismic force calculations in AISC Design Guide 20 are based on ASCE7 [14], where the inelastic behaviour of a structure is only implicitly accounted for through a response modification/reduction factor, R . For the design of SPSW systems subjected to a 'high seismic' scenario, ASCE7 specifies a response modification factor, $R = 7.0$ and a system overstrength factor, $\Omega_0 = 2.0$. These values were later supported by a detailed numerical study on 44 SPSW designs [29]. Assuming that the structure under consideration does not have any supplemental damping device and also adopting a minimum reliability factor, one can conclude that SPSW systems are designed for a target displacement ductility ratio, $\mu = 3.5$. It should be noted here that ASCE7 and AISC Design Guide 20 do not directly include the displacement ductility ratio of a system in the calculation of the design base shear. The MCE spectral accelerations for this location are, $S_s = 1.70g$ and $S_1 = 0.850g$. Following ASCE7, the design spectral acceleration parameters are calculated: $S_{DS} = 1.14g$ and $S_{D1} = 0.850g$. The design base shear is calculated as 3120 kN following ASCE7 guidelines. The different components of the SPSW system are designed as per the AISC Design Guide 20 and the AISC Seismic Provisions. Here onwards, this design is referred to as the 'AISC method' design. The final dimensions of various components and other features of this design are

- Infill panel thickness (from the first storey upwards) = 5.50, 5.00, 4.00, and 2.30 mm.
- HBE (same section for all floors) = W 27 \times 94
- VBE (same section for all storeys) = W 14X \times 398
- Fundamental time period (T_1), estimated as per ASCE7 = 0.585 s
- Spectral acceleration for T_1 (S_a) = 1.14g.

As per the design specifications, the displacement ductility (ratio) demand for this structure subjected to a design level earthquake should ideally be 3.50, which will exploit the capacity to the fullest without overshooting it. The seismic performance assessment for this structure is based on this perspective. This ductility demand (μ_d) is evaluated using nonlinear response history analyses (NLRHA) subjected to real earthquake records. Three strong motion records (Table 1), scaled to the design S_a of this typical design, are used in these NLRHA. The ductility ratio demand is calculated as

$$\mu_d = \frac{D_m}{D_y} \quad (1)$$

where, D_m is the maximum roof displacement obtained from an NLRHA and D_y is the yield roof displacement. D_y for a SPSW structure is obtained from the conventional nonlinear static pushover analysis

Table 1
Details of earthquake records used for designs of four-storey and eight-storey SPSWs.

Earthquake	Date	Station	Component	PGA (g)	Name
Northridge	Jan 17, 1994	Sylmar converter	Horizontal-052	0.612	SYL
Northridge	Jan 17, 1994	Newhall fire station	Horizontal-360	0.589	NH
Kobe	Jan 16, 1995	KJMA	Horizontal-000	0.821	KJM
Landers	Jun 28, 1992	SCE station 24	Horizontal-000	0.785	LAN
Imperial Valley	Oct 15, 1979	USGS station 5054	Horizontal-140	0.775	IMV
Cape Mendocino	Apr 25, 1992	CDMG station 89005	Horizontal-000	1.497	CM

(NSPA) using the lateral load distribution recommended in the IBC [30]. The base shear (V_b) vs. roof displacement (D) pushover plot is bilinearized using an elastic-perfectly plastic force-deformation behaviour so that the areas under the pushover curve and its bilinear approximation are equal (Fig. 2). From the NSPA, the yield displacement (D_y) is obtained as 0.123 m, with a yield base shear of 3892 kN. The three earthquakes result in μ_d values of 2.36, 2.18 and 1.76 (giving an average of 2.10). These values show that the existing design method do not (always) utilise the excellent displacement capacity of SPSW systems. The three different earthquakes result in very different yielding patterns. The lack of an effective energy dissipation through inelastic activity is also evident from the fact that beams do not form plastic hinges at both ends. Besides, the plasticity is observed to be concentrated more in the second and third storeys, resulting in higher interstorey drift (ratio) demands in these two than the other storeys. Fig. 3 provides the displacement profile for this design at the instant of peak roof displacement for each of the three records, along with an 'ideal' response based on the ductility factor.

4. Proposed performance-based design methodology

The proposed performance-based design method broadly follows the performance-based plastic design methodology recommended by [24] for various other lateral load resisting systems in steel. As mentioned earlier, the proposed design method considers a uniform interstorey drift ratio and a pre-selected yield mechanism as performance targets. Fig. 4 shows a typical one-bay SPSW configuration with rigid beam-to-column connections, along with the selected unidirectional and uniform yield mechanism. This preferred yield mechanism consists of the yielding of all steel infill panels, formation of plastic hinges at the column bases, and formation of plastic hinges at the two ends of each beam (HBE). Capacity design approaches proposed earlier for SPSW systems also specify this as the desired yield mechanism.

The proposed design method adopts the concept of energy balance, in which the inelastic energy demand on a structural system is equated with the inelastic work done, internally, through the plastic deformations. The total strain energy demand to an inelastic single-degree-of-freedom (SDOF) system is estimated as

$$E_e + E_p = \gamma \left(\frac{1}{2} M S_v^2 \right) = \frac{1}{2} \gamma M \left(\frac{T_1}{2\pi} C_e g \right)^2 \quad (2)$$

where, E_e = elastic strain energy demand, E_p = plastic strain energy demand, γ = energy modification factor, M = total seismic

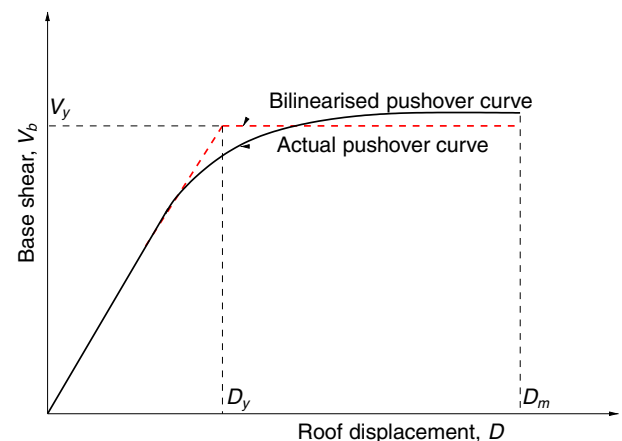


Fig. 2. Obtaining the yield base shear (V_y) and yield displacement (D_y) from the bilinearized pushover plot.

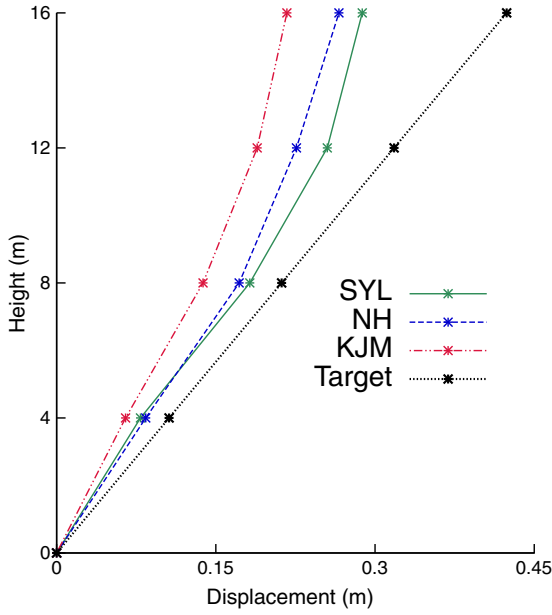


Fig. 3. Displacement profiles for the 'AISC method' design SPSW system, at the instant of maximum roof displacement.

mass of the structure, S_v = spectral velocity corresponding to T_1 , and C_e = elastic force coefficient. Based on the study by Akiyama [31], the elastic vibrational energy can be written, assuming that the entire structure is reduced into a SDOF system:

$$E_e = \frac{1}{2} M \left(\frac{T_1 V_b}{2\pi W g} \right)^2. \quad (3)$$

W is the total seismic weight of the structure and V_b is the base shear. The energy modification factor (γ) comes from the equal displacement law, and is calculated based on the target displacement ductility ratio of the system (μ_t) and the ductility-based reduction factor (R_{μ}):

$$\gamma = \frac{2\mu_t - 1}{R_{\mu}^2}. \quad (4)$$

Any suitable ' R - μ - T ' relation can be used to estimate R_{μ} . Here, we use the relationships suggested originally by Newmark and Hall [32]. Based on recent findings [33], the effects of material strain-hardening are neglected in this work, although the proposed method can be easily modified to incorporate this aspect. The elastic force coefficient is expressed in terms of the design pseudo-acceleration (S_a) or the design yield base shear (V_{by}), as

$$C_e = \frac{S_a}{g} = \frac{S_v T_1}{2\pi g} = \frac{V_{by}}{W}. \quad (5)$$

The structure is idealised as an elastic-perfectly plastic (EPP) equivalent single degree system by selecting the preferred yield mechanism up to the peak monotonic drift demand (Fig. 4). The elastic part of the total strain energy demand is calculated by replacing V_b with the yield base shear (V_{by}) in Eq. (3). Substituting this in Eq. (2), we get

$$E_p = \frac{W T_1^2 g}{8\pi^2} \left[\gamma C_e^2 - \left(\frac{V_{by}}{W} \right)^2 \right]. \quad (6)$$

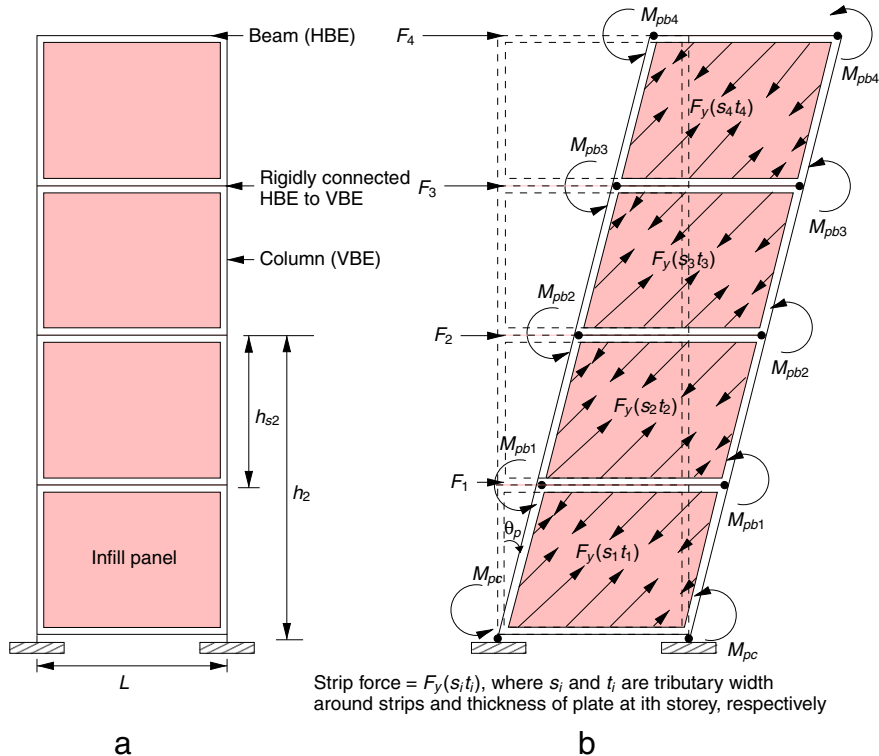


Fig. 4. (a) Schematic of a SPSW system with rigid beam-to-column connections; and (b) the selected uniform and unidirectional yield mechanism.

This plastic energy demand is the same as the work done by the equivalent lateral forces F_i (Fig. 4) going through the inelastic drift (θ_p):

$$\frac{WT_{1g}^2}{8\pi^2} \left[\gamma C_e^2 - \left(\frac{V_{by}}{W} \right)^2 \right] = \left(\sum_{i=1}^n F_i h_i \right) \theta_p = V_{by} \left(\sum_{i=1}^n C_{vi} h_i \right) \theta_p \quad (7)$$

where, h_i is the height of i th floor measured from the ground, and C_{vi} is the lateral force distribution factor for this floor. Recent research by Kharmale and Ghosh [28] recommended that any commonly followed lateral force distribution (that is, C_{vi}) can be adopted in the inelastic displacement-based design method for SPSW systems. In this work, the distribution recommended by ASCE7 is adopted. Eq. (7) can be rearranged in the form of a quadratic equation and its solution provides an expression for the required yield base shear for this performance-based design:

$$V_{by} = W \left(\frac{-\alpha + \sqrt{\alpha^2 + 4\gamma C_e^2}}{2} \right) \quad \text{where, } \alpha = \left(\sum_{i=1}^n C_{vi} h_i \right) \frac{8\theta_p \pi^2}{T_{1g}^2} \quad (8)$$

Once V_{by} is obtained, a preliminary design of the steel infill panels is considered first. Assuming that each infill panel takes the full storey shear (V_i), the initial thickness of the panel at the i th storey (t') is obtained, similarly as by Ghosh et al. [25]:

$$t'_i = \frac{2V_i}{0.95F_y L} \quad (9)$$

where, F_y is the material yield stress and L is the infill panel width. The selection of the column section is primarily based on the minimum (strength and) stiffness requirement prescribed in the Canadian standard [8] and the AISC Seismic Provisions [10], which ensures that there will be no premature buckling of a column under the pulling action of the infill plate:

$$I_{ci} \geq \frac{0.00307 t'_i h_{si}^4}{L} \quad (10)$$

where, I_{ci} is the moment of inertia of the i th storey column about its bending axis, and h_{si} is the i th interstorey height. The floor beams are designed in order to properly anchor the panel tension fields. The SPSW system is assumed to have rigid floor diaphragms at all floor levels due to the existence of a composite steel deck. The assumption of a rigid floor diaphragm results in zero axial force in all floor beams. The selection of the beam section is an iterative procedure which involves the assumption of the angle of tension field (α_t) in the steel plate panel and the successive calculation of the beam cross-sectional area. The following expression, suggested by Timler and Kulak [3] for α_t in the i th storey infill, is used to calculate the beam area required:

$$\tan^4 \alpha_t = \frac{1 + \frac{t'_i L}{2A_{bi}}}{1 + t'_i h_{si} \left(\frac{1}{A_{bi}} + \frac{h_{si}^3}{360 I_{ci} L} \right)} \quad (11)$$

where, A_{bi} and A_{ci} are the cross-sectional areas of the boundary beams and columns, respectively. Although this equation was originally developed for SPSW with pinned beam-to-column connections, it can also be used for SPSW with rigid beam-to-column connections, since the value of α_t is not really sensitive to the flexural stiffness of boundary beams [13].

In order to update the infill panel thicknesses, the virtual work principle is used by equating the inelastic work done by the equivalent forces (F_i) with the inelastic work done in the plates and in the plastic hinges in boundary elements. The plastic deformations, in this case, are obtained from a unidirectional monotonic loading up to the target drift. The formation of plastic hinges and the

yielding of infill plates are assumed to occur simultaneously, at a yield drift θ_y . The required shear capacity of the plate (P_i) at the i th storey is obtained from the following equation:

$$\left(\sum_{i=1}^n F_i h_i \right) \theta_p = 2M_{pc} \theta_p + 2 \sum_{i=1}^n M_{pbi} \theta_p + \sum_{i=1}^n P_i h_{si} \theta_p \quad (12)$$

where, n is the number of storeys in the structure, M_{pc} is the plastic moment capacity at each column base, and M_{pbi} is the plastic moment capacity of the i th floor beam. The revised plate thickness is obtained as

$$t_i = \frac{2P_i}{0.95F_y L} \quad (13)$$

The design axial force (P_c) on the columns is calculated based on the moment equilibrium about the base. The final column section is then selected from a steel table (for example, the AISC steel table [15]) for these demands on the basis of the code prescribed 'P-M interaction' and compact section criterion. This design is checked for if the demand (μ_d) is satisfactorily close to the target (μ_t). Otherwise, the HBE dimensions are changed and the plate thicknesses are recalculated. For both the VBE and HBE, the requirement of a minimum moment of inertia [11] is satisfied. A design flow-chart is provided in Fig. 5, which gives the details of individual design steps as discussed in this section.

5. Validation of the proposed design method

The proposed performance-based design methodology for SPSW systems is validated through the design and the following performance assessment of one four-storey and one eight-storey SPSW systems. These two buildings are selected to represent typical symmetric-in-plan low-rise and medium-rise office buildings. Both buildings have the same plan configuration, including the location of the SPSW bay in the outer frames of the building (Fig. 1). Their elevations are also the same except for that the eight-storey frame has four similar additional storeys. For the four-storey building, the floor-wise seismic weights are the same as those for the 'AISC method' design building considered in Section 3. For the eight-storey SPSW building, a uniform seismic weight of 5160 kN is considered at each floor.

The single-bay SPSW systems of these study buildings are designed following the proposed PBPD method, subjected to

- different earthquake records using their elastic pseudo-velocity response spectra,
- different target displacement ductility ratios (μ_t), and
- different aspect ratios of the infill panels (by changing the length of the SPSW frame in plan).

Three strong motion records from the 1994 Northridge, USA and the 1995 Kobe, Japan earthquakes (Table 1) are used for the design and subsequent performance assessment of these study frames. In the case of the eight-storey SPSW frame, these records have to be scaled up in order to avoid unrealistically thin steel plate panels. The four-storey SPSW system is designed for $\mu_t = 2.0, 3.0$ and 4.0 and the eight-storey SPSW system is designed for $\mu_t = 4.0$ and 5.0 . Although a ductility capacity of 5.0 may not be very realistic, it is set as a target for the eight-storey frame because the design base shear and the infill panel thicknesses become very low for smaller values of μ_t . Different steel panel aspect ratios ($h_s:L$) are considered for these frames: 1:1, 1:1.5 and 1:2 for the four-storey; and 1:1 and 1:1.5 for the eight-storey frames. The elevation in Fig. 1 shows an aspect ratio of 1:1. The other two aspect ratios are obtained for

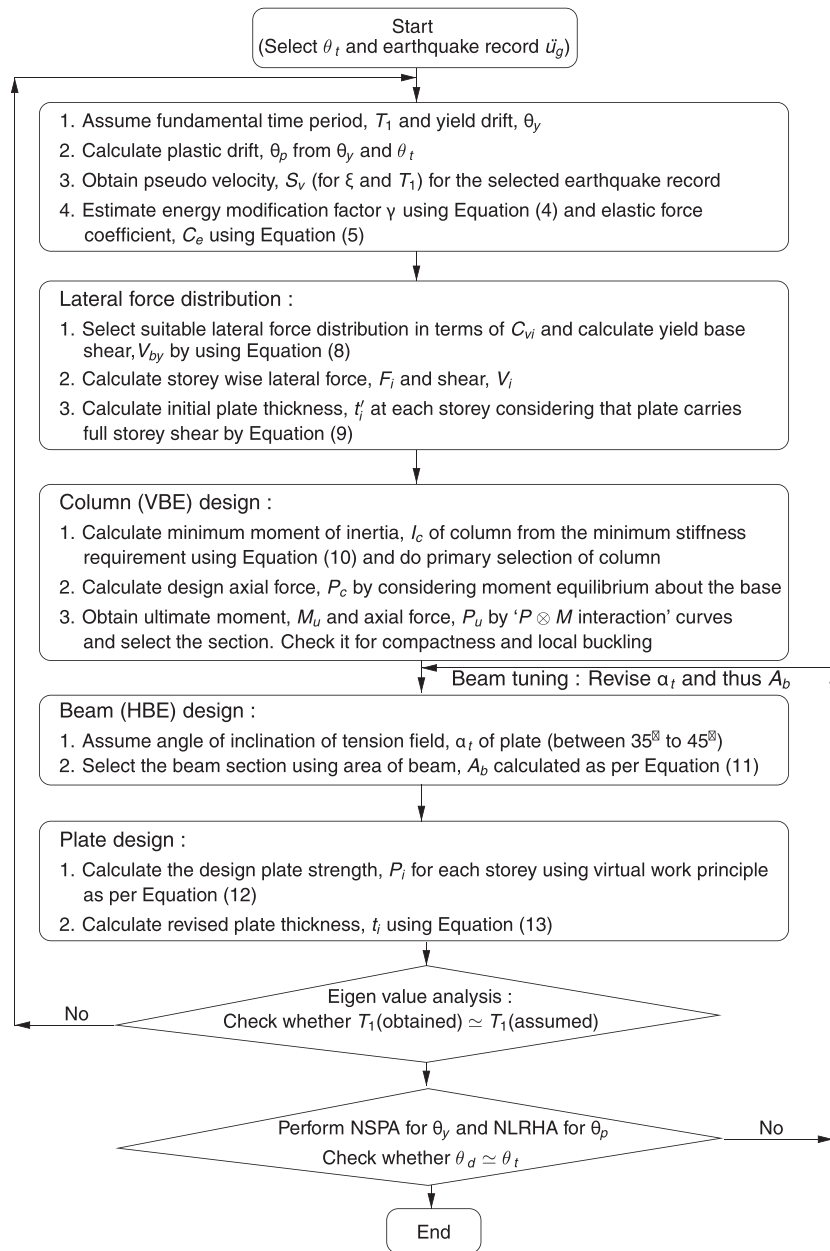


Fig. 5. Flowchart for the proposed performance-based plastic design of SPSW systems with rigid beam-to-column connections.

both the buildings by changing the length (L) of the SPSW bay, while keeping every other dimension unchanged. Overall, the different hazard scenarios, the different performance targets and the different aspect ratios result in 27 design cases for the four-storey and 12 design cases for the eight-storey SPSW systems.

Like most other seismic design procedures, the proposed procedure also needs an initial assumption of the fundamental time period (T_1), for which the design process may involve iterations. For a preliminary estimate of T_1 , the expression for T_{eq} given by Chopra and Goel [34] can be used, because the equation prescribed in ASCE7 gives a T_1 on average 17% lower than its actual value [35]. In addition, we also need to assume an initial value of the yield drift (θ_y). The assumption of a suitable yield drift is based on the observed behaviour of SPSW systems. We recommend a value between 0.75% and 1.0%. θ_y is later calculated from a NSPA of the SPSW system using the ASCE7 recommended lateral force distribution. For this, the roof displacement versus base shear plot is bilinearised by

equating the areas under the actual pushover curve and the approximate one.

The SPSW systems are designed following the steps in the design flow-chart (Fig. 5). The actual required thicknesses of the SPSW panels as per the design calculation are provided, without any due consideration to the availability of such precise thicknesses for steel sheets. The required column and beam sections are selected from the AISC steel table [15]. For the four-storey SPSW system, the column and beam sections are kept uniform for all storeys, whereas for the eight-storey frame, two sets of sections are used, one set for the lower four storeys and the other for the upper four storeys. These sections are checked for their plastic rotation capacities, that are found to be larger than rotation demands calculated from NLRHA subjected to the design earthquakes. For the selection of beam sections, α_t is varied between 35° to 45° , in order to achieve ductility demand closer to the target. The effects of this beam 'tuning' are discussed in detailed later in Section 5.3.

The effectiveness of the proposed design method is checked using NLRHA-based performance assessment of the 27 four-storey designs and the 12 eight-storey designs. This effectiveness is measured in terms of how close the NLRHA-based ductility demand (μ_d) is to the target displacement ductility ratio (μ_t) using the quantity '% Diff.':

$$\% \text{Diff.} = \frac{\mu_d - \mu_t}{\mu_t} \times 100. \quad (14)$$

Similarly, '% Diff.' also used to measure the difference between the maximum interstorey drift (θ_m) with respect to target drift ($\mu_t \theta_y$),

$$\% \text{Diff.} = \frac{\theta_m - \mu_t \theta_y}{\mu_t \theta_y} \times 100 \quad (15)$$

μ_d is measured using Eq. (1). D_m and θ_m are obtained from a NLRHA subjected to the selected ground acceleration time-history. D_y (and θ_y) is obtained from the bilinearised pushover curve as mentioned earlier. Both the NLRHA and NSPA are performed using the structural analysis programme DRAIN-2DX [36].

In addition to these 27 design cases, three additional designs are also included in this study to check the sensitivity of the proposed design methodology to selected strong motion records. These three extra design cases are for the four-storey SPSW system ($h_s:L = 1:1$, $\mu_t = 4.0$) considering three new strong motion records from Landers (1992), Imperial Valley (1989) and Cape Mendocino (1992) earthquakes (Table 1). The results for these three design cases are presented separately.

The SPSW system is modelled using the multi-strip idealisation technique [2], with centreline dimensions. The infill panel strips and the boundary elements are modelled using the nonlinear truss and beam-column elements, respectively, in DRAIN-2DX. The material is assumed to be elastic-perfectly plastic steel with a yield stress (F_y) of 345 MPa and without any overstrength factor. For the time-history analysis, a lumped mass model with 5% Rayleigh damping (in the first two modes) is considered. Effects of geometric nonlinearity and the nominal lateral stiffness offered by the gravity frames are neglected. The hysteretic behaviour of the structure is assumed to be stable without strength/stiffness degradations and pinching [37].

5.1. Summary of results for the four-storey SPSW designs

Tables 2–4 present the summary of results for the 27 designs of the four-storey SPSW system. Each design is identified here with the specific earthquake record and the target displacement ductility ratio it is designed for. For each design, D_y , D_m and θ_m values are also presented in these tables. However, the most important data in these tables are in the '% Diff.' columns, which give a measure of the effectiveness of the proposed design method. **The mean ('Average') and the**

Table 3

Results summary for designs of four-storey SPSW systems having $h_s:L = 1:1.5$.

Design	Record	μ_t	D_y (m)	D_m (m)	μ_d	% Diff.	$\mu_t \theta_y$	θ_m %	% Diff.
X	SYL	2	0.0863	0.182	2.11	5.50	0.0108	0.00901	−16.6
XII	SYL	3	0.0829	0.248	2.99	−0.333	0.0155	0.0169	9.37
XII	SYL	4	0.0745	0.301	4.04	1.00	0.0186	0.0180	−3.36
XIII	NH	2	0.0894	0.169	1.89	−5.50	0.0112	0.0120	7.38
XIV	NH	3	0.0855	0.260	3.04	1.33	0.0160	0.0150	−6.43
XV	NH	4	0.0744	0.276	3.71	−7.25	0.0186	0.0190	2.15
XVI	KJM	2	0.0902	0.193	2.14	7.00	0.0113	0.0100	−11.3
XVII	KJM	3	0.0957	0.287	3.00	0.000	0.0179	0.0160	−10.8
XVIII	KJM	4	0.0833	0.330	3.96	−1.00	0.0208	0.0220	5.64
Average						0.0833			−2.66
AbsMax						7.25			16.6

absolute maximum ('AbsMax') values of % Diff. for all design scenarios belonging to a specific steel panel aspect ratio are also provided in these tables.

For μ_d , the mean % Diff. is found to be 0.389, 0.0833 and −1.73, and for θ_m this mean is found to be 6.37, −2.66 and −7.01, for aspect ratios ($h_s:L$) of 1:1, 1:1.5 and 1:2, respectively. The corresponding values of AbsMax are 11.0, 7.25 and 6.00 for μ_d and 28.0, 16.6 and 15.8. These very low average and AbsMax values clearly show that the proposed design method is able to achieve its performance targets very efficiently (specifically for the roof displacement ductility ratio). The accuracy is slightly on the lower side for achieving the target interstorey drift ratio. It is also evident from these results that this efficiency is maintained for different ground motion records, different target ductility ratio values (μ_t), and for different steel panel aspect ratios. In addition to the ductility demand in terms of the peak roof displacement, the displacement profiles are also studied in order to check for any localised concentration of plasticity in any storey. Fig. 6 presents displacement profiles at the instant of peak roof drift for all nine design cases with $h_s:L = 1:1$. These displacement profiles demonstrate an almost uniform distribution of the interstorey drift over the height. Similar displacement profiles are also observed for the other 18 design cases belonging to $h_s:L = 1:1.5$ and 1:2. This indicates that the structure closely follows the assumed yield mechanism with uniform interstorey drift along the height, and there is no severe concentration of plasticity in any specific storey.

The results summary for the additional three design cases (Designs XXVIII, XXIX and XXX, for three other earthquakes) is presented in Table 5. The mean and the AbsMax of the values of % Diff. for μ_d are −1.73 and 6.00, and for θ_m are −4.41 and 9.28, respectively. These values show that the proposed method remains effective for these earthquakes as well, which indicates the robustness of the proposed method subjected to a variety of strong motion records.

Table 2

Results summary for designs of four-storey SPSW systems having $h_s:L = 1:1$.

Design	Record	μ_t	D_y (m)	D_m (m)	μ_d	% Diff.	$\mu_t \theta_y$	θ_m	% Diff.
I	SYL	2	0.103	0.212	2.06	3.00	0.0129	0.0160	24.3
II	SYL	3	0.0987	0.300	3.04	1.33	0.0185	0.0190	2.67
II	SYL	4	0.107	0.418	3.89	−2.75	0.0268	0.0281	4.67
IV	NH	2	0.103	0.220	2.13	6.50	0.0129	0.0150	16.5
V	NH	3	0.0912	0.270	2.96	−1.33	0.0171	0.0159	−6.43
VI	NH	4	0.0910	0.334	3.89	−2.75	0.0228	0.0250	9.89
VII	KJM	2	0.100	0.220	2.19	9.50	0.0125	0.0160	28.0
VIII	KJM	3	0.0957	0.290	3.03	1.00	0.0179	0.0140	−22.0
IX	KJM	4	0.0963	0.343	3.56	−11.0	0.0241	0.0242	0.312
Average						−1.85			6.37
AbsMax						11.0			28.0

Table 4

Results summary for designs of four-storey SPSW systems having $h_s:L = 1:2$.

Design	Record	μ_t	D_y (m)	D_m (m)	μ_d	% Diff.	$\mu_t \theta_y$	θ_m	% Diff.
XIX	SYL	2	0.078	0.152	1.94	−3.00	0.00980	0.00900	−8.16
XX	SYL	3	0.081	0.235	2.92	−2.67	0.0151	0.0160	6.00
XXI	SYL	4	0.080	0.302	3.76	−6.00	0.0201	0.0200	−.535
XXII	NH	2	0.075	0.155	2.06	3.00	0.00940	0.0100	6.38
XXIII	NH	3	0.082	0.242	2.94	−2.00	0.0154	0.0130	−15.8
XXIV	NH	4	0.076	0.300	3.96	−1.00	0.0189	0.0170	−10.3
XXV	KJM	2	0.084	0.168	1.99	−0.500	0.0105	0.00900	−14.7
XXVI	KJM	3	0.074	0.218	2.95	−1.67	0.0139	0.0120	−13.4
XVIII	KJM	4	0.074	0.290	3.93	−1.75	0.0184	0.0170	−7.86
Average						−1.73			−7.01
AbsMax						6.00			15.8

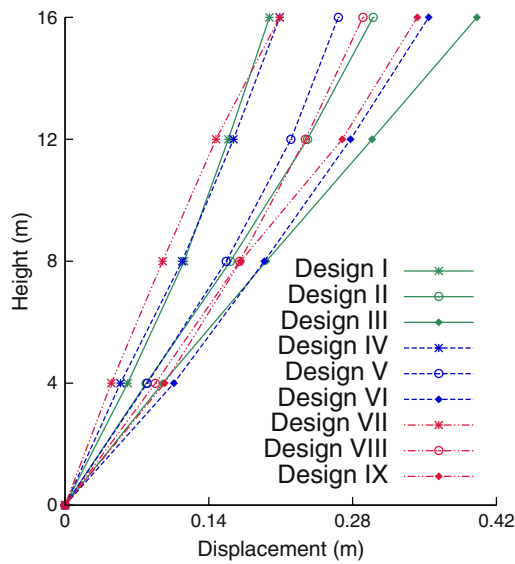


Fig. 6. Displacement profiles of the four-storey designs with $h_s:L = 1:1$, at the instant of maximum roof displacement.

5.2. Summary of results for the eight-storey SPSW designs

The results for the 12 eight-storey designs are presented in a similar (to that of the four-storey designs) manner in Tables 6–7. These tables also provide the scale factor applied to the original acceleration record for each individual design. These same scaled ground motion records are used in their performance assessment. Considering roof displacement ductility as performance objective, the average % Diff. values are observed to be -7.32 and -2.03 for steel panel aspect ratios of 1:1 and 1:1.5, respectively, and the corresponding values of AbsMax are 15.0 and 5.80. The average % Diff. values for θ_m are -0.353 and -5.54 for steel panel aspect ratios of 1:1 and 1:1.5, respectively, and the corresponding values of AbsMax are 17.2 and 18.5. These results show that the proposed method is equally effective for medium-rise SPSW systems, as well. Fig. 7 presents displacement profiles at the instant of peak roof drift for all the six design cases with $h_s:L = 1:1$. These profiles show that system follows nearly the same deformation profile as assumed in the design formulation, and that there is no concentration of damage in any specific storey.

5.3. Beam tuning and yielding hierarchy

The proposed PBPD method does not provide a specific design equation for selecting beam sections. This selection is an iterative procedure here, which involves the assumption of the angle of tension field (α_t) of steel plate panels and the calculation of the required beam cross-sectional area using Eq. (11). To check the effects of selecting a particular beam section and corresponding α_t , trial designs with varying

beam sections and α_t are used for a single design scenario in order to achieve μ_d closer to μ_t . α_t is varied between 34° and 46° based on prior experience. Results for Design II of the four-storey building (with $\mu_t = 3.0$) and Design I of the eight-storey building (with $\mu_t = 4.0$) are discussed here.

Six trial designs are obtained for the four-storey SPSW system by varying α_t between 34° and 44° , at an interval of 2° . Fig. 8 presents the beam tuning results summary in terms of the variation in μ_d with respect to α_t . The beam section used in each is also marked in this plot. This figure shows that trials with a lower value of α_t ($= 34^\circ$, 36° and 38°) result in lighter beam sections and higher demand (μ_d), and vice versa. The trial design, with $\alpha_t = 40^\circ$ and a relatively heavier section (W12X120), results in μ_d closest to the target ductility ratio ($\mu_t = 3.0$). α_t also affects the sequence of yielding in different elements of the SPSW system subjected to a monotonic push. Figs. 9–11 show the base shear versus roof displacement ‘pushover’ plots with yielding hierarchy/sequence for three design trials: with $\alpha_t = 34^\circ$ (lowest), 40° (μ_d closest to μ_t) and 44° (highest). In these plots, the commencement of plastic hinge formation in boundary elements is marked by solid circular dots for the left column base or the left end of a beam, and solid triangular dots for the right column base or the right ends of a beam. The lowest α_t (Fig. 9) corresponds to comparatively lighter beam sections and thicker plates. The beams start yielding almost as soon as the lateral loads are applied and forms plastic hinges at both ends long before the columns or the infill panels yield. This essentially renders the system to a SPSW with pin-connected beams, which is not desirable. In contrast, the SPSW with the highest α_t (Fig. 11) – with very heavy beams and very thin infill panels – behaves somewhat like a moment resisting frame. The yielding of different elements is almost simultaneous, whereas a gradual yielding is preferred to give sufficient warning to the occupants of a building. The design with $\alpha_t = 40^\circ$ provides a balance between these extremes, with a good interaction (sharing of lateral force effects) between the infill panels and the boundary elements, and gradual yielding (Fig. 10). Shishkin et al. [38] also recommended the use of $\alpha_t = 40^\circ$ for design of SPSW, although based on a different approach.

Similar results are obtained for Design I of the eight-storey SPSW system. Five trial configurations for this design scenario are achieved by varying α_t between 39.75° and 43.75° at an interval of 1° . Fig. 12 presents the beam tuning results summary for this design case. The trial design with $\alpha_t = 41.75^\circ$ with ‘moderate’ beam sections (W 14 \times 213 up to the fourth storey and W 14 \times 193 above) results in μ_d ($= 3.99$) closest to the target ($\mu_t = 4.00$).

5.4. Comparison with the ‘AISC method’ design

In order to assess the benefits and limitations of the proposed method versus the standard design practice till date, it is essential to compare the outcomes for the same scenario. Section 3 provides a typical design of a four-storey SPSW system based on the AISC Design Guide 20. An alternative design for the same building (Fig. 1) is obtained for the same design scenario using the proposed PBPD method. The design scenario is defined by the same (ASCE7) design spectrum and $\mu_t = 3.50$. The SPSW is designed following the flow-chart in Fig. 5. The NLRHA in beam tuning is performed using the record SYL (Table 1), after scaling it to the same S_d as the design spectrum. This design is referred to as the ‘Proposed method’ design. The design details are as follows:

- Infill panel thickness (from the first storey upwards) = 3.25, 3.00, 2.40, and 1.45 mm.
- HBE (same section for all floors) = W 14 \times 99
- VBE (same section for all storeys) = W 36 \times 194
- T_1 , based on an eigenvalue analysis = 1.02 s
- S_a (at T_1) = 0.833 g.

Table 5
Results summary for designs considering three additional records.

Design	Record	μ_t	D_y (m)	D_m (m)	μ_d	% Diff.	$\mu_t\theta_y$	θ_m	% Diff.
XXVIII	LAN	4	0.0970	0.354	3.65	−8.75	0.0243	0.0220	−9.28
XXIX	IMV	4	0.101	0.362	3.58	−10.5	0.0252	0.0242	−3.96
XXX	CM	4	0.096	0.357	3.74	−6.50	0.0240	0.0240	0.000
Average						−1.73			−4.41
AbsMax						6.00			9.28

Table 6Results summary for designs of eight-storey SPSW systems having $h_s:L = 1:1$.

Design	Record	μ_t	Scale factor	D_y (m)	D_m (m)	μ_d	% Diff.	$\mu\theta_y$	θ_m	% Diff.
I	SYL	1.20	4	0.247	0.985	3.99	−0.250	0.0308	0.0340	10.1
II	SYL	1.30	5	0.234	1.08	4.61	−7.80	0.0365	0.0400	9.41
III	NH	1.30	4	0.232	0.837	3.61	−9.75	0.0290	0.0240	−17.2
IV	NH	1.50	5	0.219	1.03	4.72	−5.60	0.0342	0.0318	−6.85
V	KJM	1.40	4	0.208	0.786	3.78	−5.50	0.0260	0.0250	−3.85
VI	KJM	1.90	5	0.238	1.01	4.25	−15.0	0.0372	0.0390	4.87
Average							−7.32			−0.353
AbsMax							15.0			17.2

The performance of the 'Proposed method' design is assessed in the same way as of the 'AISC method' design, using the same three ground motion records (Table 1). The records are scaled to have $S_a = 0.833$ g for the NLRHA and the estimation of D_m . The modelling idealisations in performing the NSPA and NLRHA remain the same as for the 'AISC method' design. From the NSPA, the yield displacement (D_y) is obtained as 0.0717 m, with a yield base shear of 3100 kN. The three earthquakes result in μ_d values of 3.02, 3.10 and 2.79 (giving an average of 2.97). These values are quite close to the target ($\mu_t = 3.50$) as opposed to the corresponding 'AISC method' design's values of 2.36, 2.18 and 1.76, respectively. Fig. 13 shows the displacement profiles at the instant of maximum roof displacement based on NLRHA using the three scaled records. These profiles are close to the 'ideal' profile set as a design target. These displacement profiles also indicate that there is no concentration of plasticity in any specific floor. From the NSPA performed, it is observed that the 'AISC method' design exhibits no proper sequence of yielding, and moreover, there is no formation of plastic hinge at the left end of floor beams (HBE). For the 'Proposed method' design, the yield mechanism is the same as the one assumed in the design method formulation. Also, the yielding is gradual and in proper sequence. These indicate that the performance-based design targets are achieved in the 'Proposed method' design, while the 'AISC method' design fails to use the ductility capacity of the SPSW system properly.

6. Modified PBPD method for SPSW considering P-Delta effects

P-Delta effects (structure-level secondary moment effects due to geometric nonlinearity) can sometimes be significant for structures, especially for high-rise buildings. Seismic design standards and guidelines (for example, [10,39,40]) generally specify a simple but reasonably accurate method for incorporating the P-Delta effects in the seismic demand estimation. The general practice is to apply a 'stability factor/coefficient' to amplify the seismic demands based on a linear elastic static analysis of the structure. However, these demands may not realistically represent the 'actual' demands obtained

using a NLRHA including the P-Delta effects [41]. So far, very little research work is reported in the published literature regarding P-Delta effects on SPSW systems [33]. The PBPD method proposed in this paper allows the designer to select a target ductility based on the estimated capacity of the SPSW system and do design for that. The P-Delta effects may be significant in the case of a high-rise building designed to undergo large inelastic deformations (due to the selected μ_t) subjected to a strong earthquake. Considering this, the proposed PBPD method is modified to take into account the P-Delta effects wherever necessary.

6.1. Incorporating P-Delta effects in the design formulation

P-Delta effects are incorporated in the proposed PBPD method by modifying the design base shear. The modified design base shear is obtained based on a formulation similar to Eqs. (2)–(8). For the modified formulation, the multistorey SPSW system is idealised as an inelastic SDOF system having a total seismic mass of M (total seismic weight, $W = Mg$), and the fundamental modal height of H_1 . To simplify the formulation, the seismic mass/weight on each floor is assumed to be the same (although a similar modification can also be proposed for varying floor masses). The P-Delta load at each floor comes from the seismic mass at each floor, and thus the total P-Delta load for the structure, $P_D = W$. Fig. 14 shows sample bilinearised pushover curves for multi-storey SPSW systems, which also represent the force-deformation behaviour of inelastic SDOF systems the SPSW structures are idealised to. Fig. 14.a corresponds to a SPSW system where P-Delta effects are not accounted for. It also shows the deformed shapes of the idealised SDOF system at $D = D_y$ and $D = D_m$. The pushover curve without P-Delta effects has an elastic-perfectly plastic behaviour with yield base shear V_{by} at the yield roof displacement (D_y). Fig. 14.b corresponds to an SPSW system where P-Delta effects are included. This part of the figure includes two deformed shapes (at $D = D_y$ and $D = D_m$) and a bilinearised pushover curve, as well. As P-Delta effects are accounted for in the behaviour, the SDOF system shows a softening behaviour beyond its yielding ($D > D_{y1}$). With an assumption that

Table 7Results summary for designs of eight-storey SPSW systems having $h_s:L = 1:1.5$.

Design	Record	μ_t	Scale factor	D_y (m)	D_m (m)	μ_d	% Diff.	$\mu\theta_y$	θ_m	% Diff.
VII	SYL	1.20	4	0.226	0.867	3.84	−4.00	0.0282	0.0230	−18.6
VIII	SYL	1.30	5	0.192	0.962	5.00	0.000	0.0300	0.0290	−3.33
IX	NH	1.30	4	0.218	0.881	4.04	1.00	0.0272	0.0280	2.75
X	NH	1.50	5	0.194	0.954	4.92	−1.60	0.0303	0.0270	−11.0
XI	KJM	1.40	4	0.177	0.697	3.93	−1.75	0.0221	0.0200	−9.61
XII	KJM	1.90	5	0.171	0.805	4.71	−5.80	0.0267	0.0240	−10.2
Average		−5.54					−2.03			−5.54
AbsMax							5.80			18.6

the inelastic energy demand on the system remains the same, irrespective of including or excluding P-Delta effects, the modified design yield base shear (V_{by1}) is obtained in a two-step process. In the first step, the 'original' design yield base shear, V_{by} , is calculated considering no P-Delta effects in the design formulation Eq. (8). In the second step, V_{by1} is obtained by equating the areas under the pushover curve for the system without P-Delta effects (Fig. 14.a) and for the system with P-Delta effects (Fig. 14.b):

$$\frac{1}{2}(2D_m - D_y)V_{by} = \frac{1}{2}V_{by1}D_{y1} + \frac{1}{2}(V_{by1} + V_{b1})(D_m - D_{y1}). \quad (16)$$

The force-deformation behaviour in Fig. 14.b gives the reduced the base shear V_{b1} at $D = D_m$:

$$V_{b1} = V_{by1} - \frac{P_D}{H_1}(D_m - D_{y1}). \quad (17)$$

Considering that the initial/elastic stiffness for the two SDOF systems is the same, and subsequently $V_{by}/D_y = V_{by1}/D_{y1}$, Eq. (16) can now be written without D_{y1} and V_{b1} :

$$\begin{aligned} & \left(2V_{by} + \frac{P_D}{H_1}D_y\right)D_yV_{by1}^2 - 2\left(V_{by} + \frac{P_D}{H_1}D_y\right)V_{by}D_mV_{by1} \\ & + \left((2D_m - D_y)V_{by} + \frac{P_D}{H_1}D_m^2\right)V_{by}^2 = 0. \end{aligned} \quad (18)$$

The solution of this quadratic equation gives the design yield base shear including P-Delta effects (V_{by1}), in terms of V_{by} and other 'known' parameters:

$$V_{by1} = \frac{\left(V_{by} + \frac{P_D}{H_1}D_y\right)V_{by}D_m}{\left(2V_{by} + \frac{P_D}{H_1}D_y\right)D_y} + \frac{\sqrt{\left(V_{by} + \frac{P_D}{H_1}D_y\right)^2V_{by}^2D_m^2 - \left(2V_{by} + \frac{P_D}{H_1}D_y\right)\left((2D_m - D_y)V_{by} + \frac{P_D}{H_1}D_m^2\right)V_{by}^2D_y}}{\left(2V_{by} + \frac{P_D}{H_1}D_y\right)D_y}. \quad (19)$$

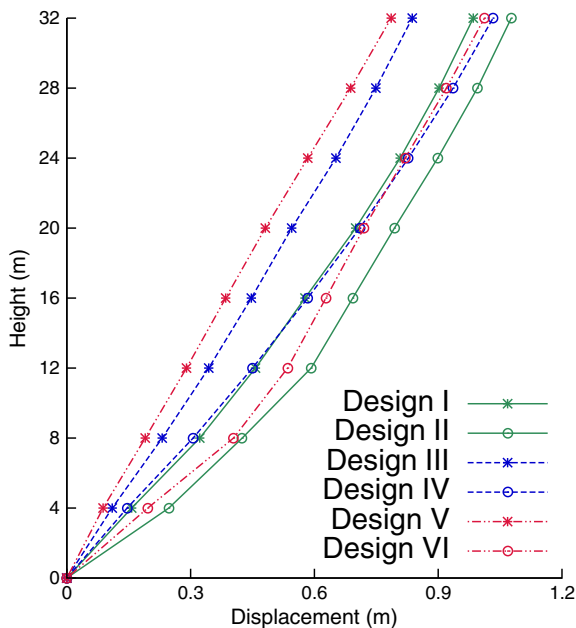


Fig. 7. Displacement profiles of the eight-storey designs with $h_s:L = 1:1$, at the instant of maximum roof displacement.

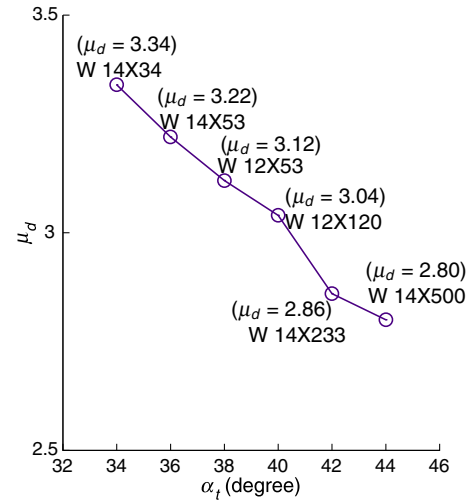


Fig. 8. Change in μ_d due to beam tuning, for Design II of the four-storey SPSW system.

The fundamental modal height, H_1 can be calculated as

$$H_1 = \frac{\sum_{i=1}^n h_{si}m_i\phi_{i1}}{\sum_{i=1}^n m_i\phi_{i1}} \quad (20)$$

where, ϕ_{i1} is the i th floor element in the fundamental mode shape vector, and m_i is the lumped mass at the i th floor. After obtaining V_{by1} , the rest of the modified design procedure (which includes the design of various components of the SPSW system) remains the same as illustrated in the design flow-chart of Fig. 5.

6.2. Validation of the modified design method

Sample design scenarios for the eight-storey SPSW system (Designs II, IV and VI, with an aspect ratio $h_s:L = 1:1$ and Designs VIII, X and XII

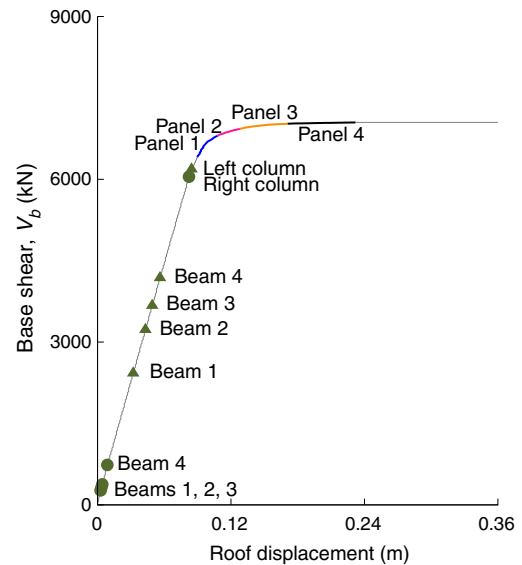


Fig. 9. Pushover plot with yielding hierarchy for Design II of the four-storey SPSW system, with $\alpha_c = 34^\circ$.

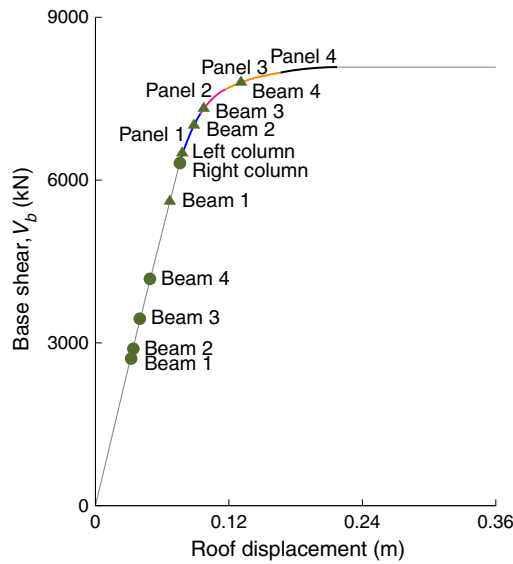


Fig. 10. Pushover plot with yielding hierarchy for Design II of the four-storey SPSW system, with $\alpha_t = 40^\circ$.

with an aspect ratio $h_s:L = 1:1.5$) are considered here to check the effectiveness of the modified PBPB method including P-Delta effects. The target displacement ductility ratio is kept the same for these redesigns ($\mu_t = 5.0$). The P-Delta load on each floor is considered to be equal to the seismic weight on each floor. These redesigns as well as the original designs (Section 5) are assessed using NSPA and NLRHA, while including the P-Delta effects in these analyses. Tables 8 and 9 provide results summary for these redesigns. These tables also provide a comparison with the original designs in terms of μ_d , '% Diff.', 'Average' and 'AbsMax'.

For redesigns with $h_s:L = 1:1$ (Table 8), the average % Diff. is -12.5 , as opposed to -22.1 for the original designs. The corresponding AbsMax values are 15.4 and 24.4 for redesigns and original designs, respectively. Table 8 shows that for each design scenario considered

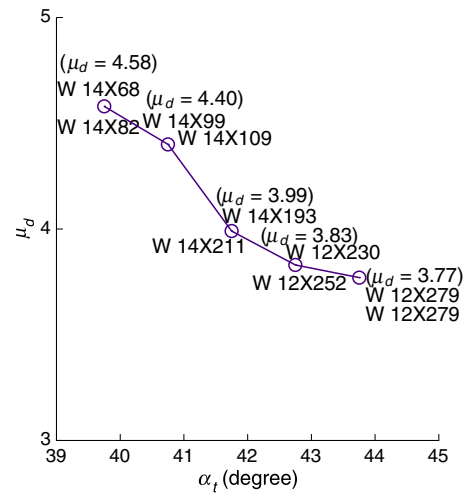


Fig. 12. Change in μ_d due to beam tuning, for Design I of the eight-storey SPSW system.

here, the modified design methodology is more efficient in achieving μ_d closer to μ_t . Results for $h_s:L = 1:1.5$ (Table 9) put the modified design method in an even better position. Here, the average % Diff. ($= -21.0$) of the original designs is reduced to -9.87 for the redesigns. Similarly, the AbsMax ($= 23.6$) of the original designs is also reduced to 13.0 for the redesigns.

7. Summary and conclusions

A performance-based plastic design procedure, considering a selected displacement ductility ratio and a yield mechanism as the performance targets, is proposed in this paper for steel plate shear wall systems with rigid beam-to-column connections. 30 design cases of four-storey (low-rise) and 12 design cases of eight-storey (medium-rise) SPSW configurations, varying in target displacement ductility ratio, design ground motion, and steel panel aspect ratio, are achieved using the proposed PBPB method. Performance assessment of these designs clearly shows that, for a large variety of design scenarios, the

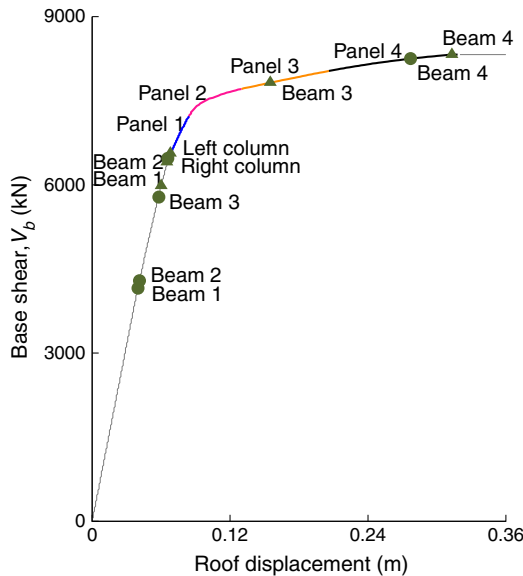


Fig. 11. Pushover plot with yielding hierarchy for Design II of the four-storey SPSW system, with $\alpha_t = 44^\circ$.

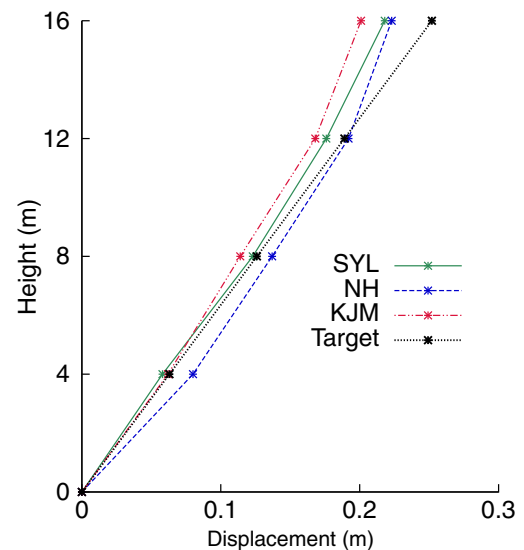


Fig. 13. Displacement profiles for the 'Proposed method' design SPSW system, at the instant of maximum roof displacement.

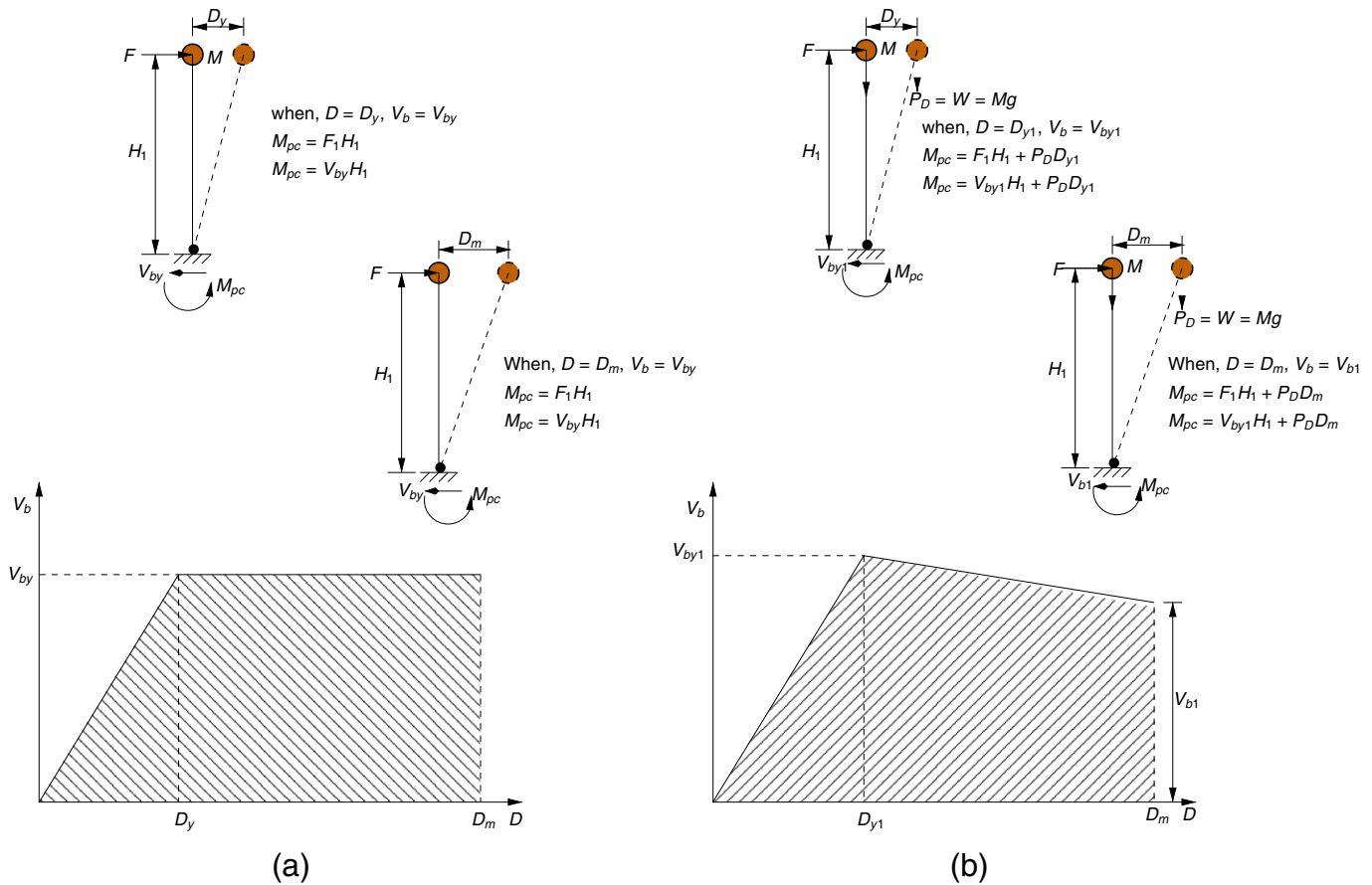


Fig. 14. Force-deformation curves of idealised SDOF systems for SPSW (a) without accounting for P-Delta effects, and (b) with P-Delta effects.

proposed design method is very effective in achieving the performance targets.

The proposed design method is also compared with the existing AISC design guide for steel plate shear walls, through the sample design case study of a four-storey system. Both design methods are used to obtain designs for the same design scenario. While the proposed design is able to reach very close to its stated performance targets, the AISC method design fails to properly utilise the ductility capacity offered by the SPSW system.

The proposed PBPD method is modified to account for P-Delta effects wherever necessary. A design equation is proposed to modify the design yield base shear in case P-Delta effects are expected. Six design case studies for the eight-storey SPSW system, with a target displacement ductility ratio of 5.0, show that the modified PBPD method is more effective in achieving the performance targets

compared to the PBPD method proposed originally in this work. The modified method still remains to be tested for high-rise SPSW systems, where P-Delta methods are even more. However, on a relative scale, the modified method is expected to be still more effective for such cases, compared to the original PBPD proposed here.

While both PBPD methods (original and modified for P-Delta) provide step-by-step procedures to obtain designs that are very effective in achieving displacement-based performance targets, these methods lack in offering a very precise beam (HBE) design method. Experience of the designs presented here suggests that beams tuned to α_t around 38°–42° typically provide an 'optimum' design. However, future studies in this area should come up with more precise design guidelines/equations for beams in an SPSW system. Number of iterations involved in the design process is another issue that needs to be

Table 8

Results summary for redesigns and original designs of eight-storey SPSW systems having $h_s:L = 1:1$.

Design	Record	Scale factor	μ_t	Modified method		Original method	
				μ_d	% Diff.	μ_d	% Diff.
II	SYL	1.30	5	4.23	−15.4	3.87	−23.4
IV	NH	1.50	5	4.58	−8.40	4.07	−18.6
VI	KJM	1.90	5	4.31	−13.8	3.78	−24.4
Average					−12.5		−22.1
AbsMax					15.4		24.4

Table 9

Results summary for redesigns and original designs of eight-storey SPSW systems having $h_s:L = 1:1.5$.

Design	Record	Scale factor	μ_t	Modified method		Original method	
				μ_d	% Diff.	μ_d	% Diff.
VIII	SYL	1.30	5	4.80	−4.00	4.10	−18.0
X	NH	1.50	5	4.35	−13.0	3.93	−21.4
XII	KJM	1.90	5	4.37	−12.6	3.82	−23.6
Average					−9.87		−21.0
AbsMax					13.0		23.6

dealt with in the following studies in this area. Similar to any other design method, the number of iterations can of course be reduced as we build our experience in the proposed PBPD methods. Besides these, material strain-hardening is another aspect that remains to be incorporated in the proposed design methods. As mentioned earlier, the proposed PBPD methods also need to be put into a probabilistic design framework, which is a work in progress by our research team, and performance levels should be defined in terms of interstorey drift ratio or displacement ductility ratio for SPSW.

Acknowledgement

The authors of this paper gratefully acknowledge the guidance received over the past years from Prof. Subhash C. Goel. The work presented here is funded by a sponsored research grant from the Department of Science and Technology (DST), Govt. of India. However, results and opinions presented in this paper are solely of the authors, and not necessarily representing the views of DST. The authors would also like to thank the reviewers for their suggestions which enhanced this paper.

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