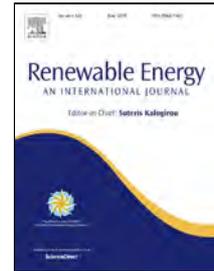


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# Wind Energy Research: State-of-the-Art and Future Research Directions

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## Abstract

This paper reports the findings from the 2016 *Wind Energy Research Workshop* held in Lowell, MA. The workshop examined the state-of-the-art in wind energy research within the following three core topic areas: (A) Wind Turbine Design and Manufacturing including: blades, towers/foundations and nacelle, (B) Wind Farm Development including: offshore installations/siting, flow characterization and loads/waves/wind characterization, and (C) Wind Farm Operations including: controls, power production, wind farms, sensing, diagnostics, testing, structural health monitoring, reliability, energy storage, the grid and power transmission. Research challenges and future directions were discussed and are reported for each sub-topic area.

**Keywords:** Wind Energy; Resource; Design; Manufacturing; Operations;

## List of Abbreviations

ACMA	American Composites Manufacturers Association
AC	Alternating Current
AEP	Annual Energy Production
AMO	Advanced Manufacturing Office
ANSI	American National Standards Institute
API	American Petroleum Institute
AWEA	American Wind Energy Association
BAAM	Big Area Additive Manufacturing
BOEM	Bureau of Ocean and Energy Management
BRC	Blade Reliability Collaborative
BSH	German Federal Maritime and Hydrography Agency
CFD	Computational Fluid Dynamics
CFR	Code of Federal Regulations
CMS	Condition monitoring systems
CNC	Computer Numerical Control
CREW	Continuous Reliability Enhancement for Wind
DC	Direct Current
DD-RANS	Data-driven Reynolds-averaged Navier–Stokes model
DONG	Danish Oil and Natural Gas (DONG) Energy
DNS	Direct Numerical Simulation (of Navier-Stokes Equations)
FLORIS	FLOw Redirection and Induction in Steady state
GIS	Geographic Information System

44	GRC	Gearbox Reliability Collaborative
45	ICC	Initial Capital Cost
46	IEC	International Electrotechnical Commission
47	IPC	Individual Pitch Control
48	IWES	Institute for Wind Energy and Energy System
49	LCOE	Levelized Cost of Energy
50	LES	Large Eddy Simulation (for simulation of the Navier-Stokes Equations)
51	Lidar	Light detection and ranging
52	LRC	Levelized Replacement Cost
53	MCEC	Massachusetts Clean Energy Center
54	MCP	Measurement-Correlation-Prediction
55	MEDIN	Marine Environmental Data and Information Network
56	NREL	National Renewable Energy Laboratory
57	NWTC	National Wind Technology Testing Center
58	O&M	Operations and Maintenance
59	OEM	Original Equipment Manufacturer
60	OTJ	On-the-job
61	RANS	Reynolds Averaged Navier-Stokes Equation
62	ROMs	Reduced Order Models
63	SHM	Structural Health Monitoring
64	SME	Small and Medium Enterprise
65	SNL	Sandia National Laboratories
66	SOWFA	Simulator for Wind Farm Applications
67	SWAN	Simulating Waves Nearshore
68	SWIFT	Scaled Wind Farm Technology
69	U.S. DOE	United States Department of Energy
70	WTTC	Wind Technology Testing Center
71	WRF	Weather Research and Forecasting

## 72 **1.0 Introduction**

73 Wind energy is one of the fastest growing sources of new electricity generation capacity in the  
74 United States of America [1]. As wind energy continues to grow towards the U.S. goal of achieving  
75 20% electricity generation from wind energy by 2030 [2], new challenges and opportunities have  
76 arisen due to: the growing competitiveness of the industry [3], the intermittency of wind energy  
77 production [4-6], operations and maintenance [7-9] as well as power distribution and grid  
78 integration related considerations [10-12]. These challenges are being addressed in part by more  
79 advanced design and control [13, 14], deployment, and condition monitoring [15, 16] in addition  
80 to more robust power electronics [17], grid transmission and advanced energy storage infrastructure  
81 [18-21]. More specifically, these topics include research into larger wind turbines [22, 23],  
82 improvement of wind farm layout [24], examination of offshore wind installations [25], improved  
83 wind/wave load predictions [26], novel approaches to wind turbine and wind farm control [13, 14,  
84 27, 28], as well as improved sensing and monitoring of wind turbines [15, 16]. Ultimately, these  
85 efforts are directed at improving wind energy responsiveness and applicability in the modern  
86 energy landscape.

87  
88 This paper presents the findings of a two-day Wind Energy Research Workshop held in Lowell,  
89 Massachusetts on 15<sup>th</sup>-16<sup>th</sup> March 2016. The goal of the workshop was to bring together a diverse  
90 audience comprising academic, industry and government stakeholders to summarize current state  
91 of the art, understand current trends and define the future directions and opportunities in wind  
92 energy research. Experts, practitioners and participants were invited from around the world and

93 across the United States of America to present and discuss their perspective of the future of wind  
 94 energy research in a series of panel sessions as well as user contributed talks and posters. The key  
 95 findings of this workshop are presented here along with several promising proposed research  
 96 directions. Suggestions were also made for improving sharing, dissemination and collaboration  
 97 amongst wind practitioners, specifically from academia to industry and vice versa.

98 The workshop was designed to spur conversation in three core topic areas. Each of these areas was  
 99 sub-divided into three more specific topical areas that were discussed in panel sessions. The topics  
 100 have broad relevance to academic, industry and government research:

- 101 • **Topic Area A: Wind Turbine Design and Manufacturing**
  - 102 ○ **Section 1:** Blades: Manufacturing, Composites, Materials and Modeling
  - 103 ○ **Section 2:** Towers and Foundations
  - 104 ○ **Section 3:** Nacelle: Gearbox, Rotors and Generators
- 105 • **Topic Area B: Wind Farm Development**
  - 106 ○ **Section 1:** Offshore Installations and Siting
  - 107 ○ **Section 2:** Flow Characterization
  - 108 ○ **Section 3:** Characterization of Loads, Waves and Wind
- 109 • **Topic Area C: Wind Farm Operations**
  - 110 ○ **Section 1:** Controls, Power Production and Wind Farms
  - 111 ○ **Section 2:** Structural Health Monitoring (SHM), Sensing, Diagnostics, Testing and  
 112 Reliability
  - 113 ○ **Section 3:** Energy Storage, Grid and Transmission

114 Summaries of the sub-topic areas are presented in the sections that follow. This paper summarizes  
 115 the panelist presentations, the ensuing panel discussions and the discussions throughout the  
 116 workshop.

117 **2.0 Topic A1: Wind Turbine Blades: Design, Manufacturing, and Testing** (Lead: C.J. Hansen,  
 118 Panelists included: R. Barnhart, *Wetzel Engineering*; S. Johnson *General Electric*; D. Miller  
 119 *Montana State University* and A. Schoenberg *CERL-MCA*)

120 Modern utility-scale wind turbine blades are fabricated from composite materials molded into an  
 121 aerodynamic shape designed to generate aerodynamic lift (i.e., mechanical power) that is  
 122 subsequently transformed by a generator into electricity. Half of the levelized cost of energy  
 123 (LCOE) for wind energy is associated with turbines, and wind turbine blades represent 25% of this  
 124 cost [29]. Over the past decades, installed rotor diameters have grown to increase energy capture  
 125 and reduce LCOE. This underlying trend required innovative approaches to turbine blade designs,  
 126 the materials used to fabricate blades, and blade manufacturing schemes. This section discusses the  
 127 state-of-the-art and future directions in four focal areas critical to wind turbine blades: blade  
 128 designs, manufacturing of blades, materials development and testing for blades, and workforce  
 129 development strategies for the turbine blade industry.

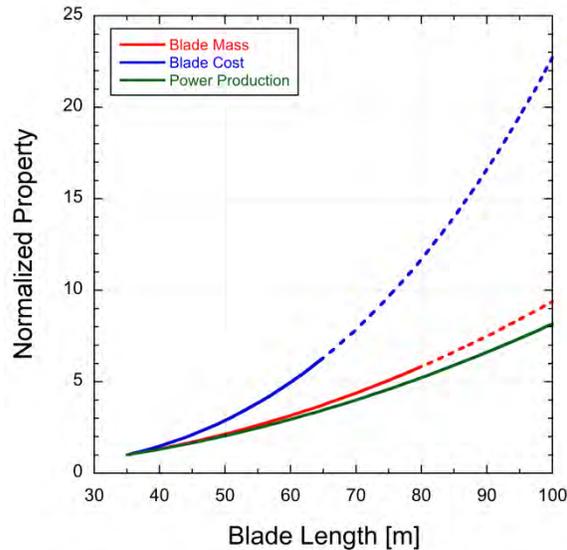
### 130 *2.1 State-of-the-Art*

131 Design of wind turbine blades is driven by the conflicting demands of structural capability (i.e.,  
 132 thicker airfoils) and aerodynamic efficiency (i.e., thinner airfoils). These competing demands  
 133 manifest as four primary aims typical within turbine designs to optimize the aerodynamic blade  
 134 shape for an improved power coefficient, to increase the length of the turbine blades for increased  
 135 swept rotor area and associated energy capture, to design the blade for manufacturing, and to

136 increase field reliability. Typically, computationally predicted airfoil designs are provided to  
137 structural engineers, who establish structural designs that dictate the composite laminate ply lay-  
138 up scheme and structural features. The drive toward longer blades has resulted in higher structural  
139 loads, which in turn result in more slender blade designs to reduce blade loads and materials usage.  
140 Maximum deflections to avoid striking the tower and modal analysis to avoid natural frequencies  
141 have now become dominating constraints. Models must prescribe reasonable manufacturing  
142 approaches and tolerances, particularly for bond gaps within the trailing edge or between the shear  
143 web and skins. Overall, the designer must recognize the need for system- rather than  
144 subcomponent-level optimization that requires iterative design cycles and input from the  
145 manufacturer.

146 Materials and component testing data is key to the longstanding challenge of increased confidence  
147 that designs will translate into robust manufactured turbine blades. As materials comprise up to  
148 50% of the cost of a manufactured turbine blade [30], new materials and materials characterization  
149 offer scope for meaningful cost reductions. Turbine blades are fabricated from fiber-reinforced  
150 polymer composites, which offer advantageous specific modulus and stiffness values. However,  
151 composites possess complex failure modes with statistical failure distributions that necessitate  
152 significant characterization efforts. Since 1989 Sandia National Lab and Montana State University  
153 have partnered to test and report on fiber-reinforced composite materials used in wind turbine  
154 blades. This publicly available database contains over 16,000 tests on 500 materials and includes  
155 both static and fatigue data [31]. Laminates tested include unidirectional,  $\pm 45^\circ$ , and multi-  
156 directional configurations. Neat resins, adhesives, lap shear, ply drops, and environmental effects  
157 have been characterized as well. A significant effort in recent years has focused on the effect of  
158 defects in manufactured materials [32, 33]. Wind turbine blade manufacturers cannot afford the  
159 degree of quality control associated with aerospace composites fabrication and so are susceptible  
160 to defects that significantly impact structural performance. Examples of defects include in-plane  
161 and out-of-plane waviness and wrinkles [34], dry spots, and porosity [35]. Characterization efforts  
162 have produced materials databases, factors of safety, and design rules that are fed into structural  
163 models. Blade certification presently requires a full-scale turbine blade to be tested in static and in  
164 fatigue loading per each new design [36]. The significant cost ( $\sim \$1M$ ) and time ( $\sim 3$  months per  
165 fatigue test, with a 6 month lead time to begin testing) hinders the deployment of new blade designs  
166 and leads to risk-averse, incremental design modifications.

167 The translation of these recent designs and materials into fabricated blades increasingly challenges  
168 composites manufacturers. Average rotor diameters in U.S. onshore installations have increased by  
169 36% to 99.4 meters in the decade to 2014 [37], and blades lengths and masses of 55-60 meters and  
170 14-17 metric tons are now common [38]. Global off-shore wind installations rotor diameters  
171 averaged 115 meters in 2014 and are projected to increase to 153 meters by 2020 [39]. The mass  
172 of the blade grows nonlinearly with their length [40], yet more concerning are costs that increase  
173 at a yet steeper rate (Figure 1); a typical on-shore, 60 meter blade weighs approximately 20 metric  
174 tons and costs  $\sim \$150$ - $250K$ , depending on the manufacturer. The industry cannot afford aerospace  
175 grade tooling, imposing a formidable challenge to consistently achieve millimeter-level accuracies  
176 over distances of greater than 50 meters. State-of-the-art blades increasingly incorporate  
177 aerodynamic enhancement features, including plasma actuator control of vortex shedding [41],  
178 trailing-edge serrations [42], and other noise mitigation techniques [43]. Though schemes for  
179 automated manufacture have been described or demonstrated, prohibitive costs restrict automation  
180 primarily to ply cutting and in drilling of the root section. Hence, blade manufacturing remains  
181 labor-intensive and labor costs contribute 30% to the cost of a blade. The already physically  
182 demanding work of material placement, environmental exposure and interaction with large-scale  
183 structures will be exacerbated as heavier and lengthier blades require more lifting, walking,  
184 grinding, and inspection from the workforce.



185

186 Figure 1. Wind turbine blade mass, cost, and turbine power production as a function of blade length.  
 187 Current trends in data (solid lines) are extrapolated (dotted lines) to blade lengths envisioned for  
 188 projects in the next five years.

189 An estimated 73,000 full-time workers are employed by the U.S. wind industry [37], and over 200  
 190 workforce training schemes have developed to meet industry needs [44]. Manufacturing plant  
 191 operations staff can be grouped into operators, shift supervisors, and engineers or managers.  
 192 Operators benefit from certificates or similar credit or non-credit bearing formal training that teach  
 193 key knowledge of composites' chemical safety and impacts of material composition and  
 194 reinforcement orientation. Credited programs include the American composites manufacturers  
 195 association's (ACMA) "Certified Composites Technician" program [45] in resin molding and in  
 196 wind blade repair, and associates programs in wind energy offered by community colleges.  
 197 Supervisors benefit from increased training in statistical process control, metrology, and  
 198 composites, training which is acquired at the advanced associates level or at universities. Engineers  
 199 and managers require skills in engineering problem solving, design of experiments, and lean  
 200 manufacturing protocols; these details are available at the university-level, but are not always  
 201 included in undergraduate engineering curricula. The U.S. Department of Energy has conducted an  
 202 in-depth manufacturers needs assessment [44] and frequently updates a catalogue of wind energy  
 203 related education and training programs under the WINDEXchange website [46].

## 204 2.2 New Achievements

205 Several prominent research efforts are expanding capabilities in new designs and manufacturing  
 206 approaches. Blade designs, such as the Segmented Ultralight Morphing Rotor [47], may reduce  
 207 blade mass at large scales by folding in extreme weather, thereby enabling designs for lower loads  
 208 and lighter mass. Design for transport has led Blade Dynamics, Gamesa, LM, and Enercon to  
 209 develop modular blades that are more easily transported on roads, but which require continued  
 210 research into joint design and lifetime. Modularity is also the basis for the U.S. Department of  
 211 Energy Advanced Manufacturing Office (AMO) to additively manufacture wind turbine blade  
 212 molds in an effort to create modular molds that are more rapidly replicated and which can be  
 213 expanded and reused in the future [48]. The "Big Area Additive Manufacturing" (BAAM) printer  
 214 at Oak Ridge National Lab is used to print mold segments, which are post-processed to obtain  
 215 adequate surface finish. Fraunhofer IWES has recently commissioned a BladeMaker

216 Demonstration Center. The demonstration of automation in manufacturing features a 6-axis gantry  
217 robot with a working envelope of 25 x 4.5 x 3 meters capable of a series of automated tasks,  
218 including computer numerical control (CNC) milling for blade mold manufacture, handling of  
219 textile and sandwich preforms, and quality management [49].

### 220 *2.3 Future Research Directions*

221 The relentless drive toward lower LCOE will sustain longstanding trends in wind turbine blades:  
222 larger blades for increased energy capture manufactured at minimal cost. This trend will drive both  
223 incremental and radical innovations in the design, materials, and manufacture of these blades. The  
224 cross-cutting opportunity for systems-level optimization offers greatest scope for progress but will  
225 require unprecedented levels of sophistication and collaboration. An effective implementation of  
226 this optimization requires knowledge and data flow between blade designers, materials suppliers,  
227 blade manufacturers, turbine manufacturers and wind farm owner-operators to transition the  
228 iterative design process presently implemented at the design level to encompass the entire  
229 manufacturing chain. The dominance of vertically integrated wind energy companies is reinforced  
230 in part by their ability to transfer data between all levels of the manufacturing chain, from designers  
231 to the operating turbines in wind farms. These data transfer needs should be established at the outset  
232 of contracts, as data agreements for blades after field deployment have met with limited success.

233 Blade designers will require innovative approaches to meet the structural requirements of future  
234 blades while addressing the materials usage and manufacturing challenges of long blades.  
235 Segmented (or modular) blade designs [50] will continue to be a research focus requiring new  
236 studies into optimal joint designs and designs for robust dimensioning and alignment. In recent  
237 lighter blade designs, reduced materials usage in the skins defining the aerodynamic surface is now  
238 producing buckling-prone designs. Designers are incorporating data from field failures and  
239 increasingly request sensors to collect greater quantities of data. Failure modes of active design  
240 interest include shear web debonds, manufacturing flaws, resistance to lightning strikes, soiling of  
241 the aerodynamic surface, de-icing concerns, and general improvements to damage tolerance.

242 Blade designs will benefit from materials innovations in lowering the cost of materials systems and  
243 from materials and structural testing. Composites will continue to be chosen primarily on a  
244 “stiffness per dollar” basis. Researchers must therefore consider the potential cost impacts of  
245 innovative materials. Research into lowered energy input and cost of carbon fibers are of interest,  
246 but must be placed in the context of continued advances in lowered cost and property improvements  
247 of high-modulus S-glass reinforcements. Improved technical basis for safety factors associated with  
248 manufacturing defects offers scope to reduce blade overdesign; for instance, innovative material  
249 systems (e.g., RodPack technology [51]) and structural components (e.g., pultruded beams [52,  
250 53]) which result in improved quality and specific properties offer potential if they meet cost  
251 targets. Fatigue behavior of composites remains a challenge, with gaps in knowledge regarding  
252 effects of imperfections, porosity, residual stresses, crack initiation and damage evolution, and the  
253 associated safety factors all active research topics. End-of-life concerns regarding recyclability and  
254 disposal threaten the industry with future regulation, due to the sheer material volume associated  
255 with the tens of thousands of blades to be decommissioned in the coming decade. Thermoplastic  
256 matrix composites and recyclable thermosets (e.g., Recyclamine® by Connora Technologies [54])  
257 are foundations upon which new innovations can grow [55]. Use of recycled carbon fiber as  
258 reinforcement [56] in future blades requires research into achieving reliable stiffness at competitive  
259 price points.

260 Manufacturers need to radically rethink the blade manufacturing process in order to address the  
261 unsustainable increase in cost per length of blade. Blade cost projections from evolutionary process

262 changes are insufficient to meet future LCOE targets. Modularity offers a potential solution.  
263 Segmented blade designs result in shorter molds, benefiting both the manufacture and  
264 transportation of lengthy blades. Segmented molds, in which varying central mold lengths join  
265 separate root and tip molds, could amortize the cost of molds over a family of blades of increasing  
266 lengths. Segmented blades require in-field assembly, and yet more radical field-assembly designs  
267 require attention to the environmental impacts (e.g., hygrothermal, contamination) on mechanical  
268 or adhesive joints. Cost-effective automation offers scope to concurrently reduce labor costs per  
269 blade and to improve blade quality via defect count reduction. Finally, for defects that occur, a  
270 scientific basis is needed to decide whether a defect is cosmetic versus critical to structural  
271 performance. Though in-house manufacturer guidelines exist, ad hoc decisions are made regarding  
272 new defect types and whether the repair will be more damaging than the embedded defect.

273 Expansion in the coming decade of a skilled workforce must build on the wind-related workforce  
274 training programs developed in the past decade. These programs required concerted collaboration  
275 between industry and local educational institutions. Exemplary best practices approaches to  
276 develop industry-driven curricula, such as those of Composites Washington, should be adopted  
277 more widely. Constant renewal of curricula is necessary to account for new manufacturing  
278 techniques and to assist existing employees who need professional development. Community  
279 colleges and universities need to reconsider which topics are relegated to on-the-job (OTJ) training  
280 based on industry input; many small and medium enterprises (SMEs) lack the in-house expertise  
281 to offer statistics of materials, design of experiments, lean manufacturing protocols as OTJ training.

#### 282 2.4 Summary

283 Wind turbine blades will continue to evolve in their design and manufacture due to the central role  
284 in influencing LCOE. An emphasis on data sharing and analytics, modular designs, cost-effective  
285 automation, and equipping the future workforce with composites-relevant skills will fuel continued  
286 growth of the wind energy industry and assist in competitive energy production in more challenging  
287 environments, such as locales with poor wind resources and off-shore sites.

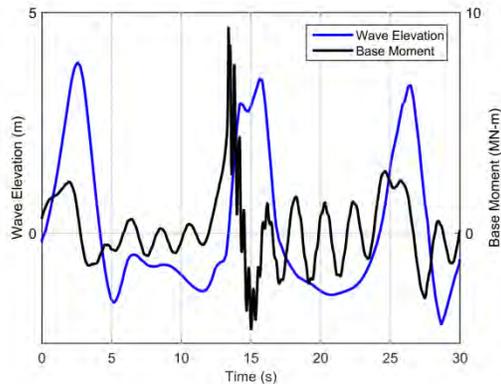
288 **3.0 Topic A2: Towers and Foundations** (Lead: S. Arwade, Panelists included: K. Wei,  
289 *Northeastern University*; Z. Finucane, *Keystone*; S. Ozmutlu, *Vryhof Anchors*; A. Rodriguez,  
290 *Alstom* and S. Hallowell, *Northeastern University*)

291 The towers and foundations that support the turbine are a critical part of the wind energy  
292 infrastructure and their design and maintenance present unique challenges to structural engineers.  
293 This is particularly true in the offshore environment where a combination of unpredictable wind  
294 and wave conditions combine with challenging construction conditions and difficult-to-  
295 characterize geotechnical conditions. In this session, which was focused on offshore systems, a  
296 cross section of academics, designers, and suppliers presented the state-of-the-art in offshore towers  
297 and foundations and thoughts on future challenges and opportunities. As the US embarks upon  
298 offshore wind development, the contributions to this session set the stage for future development  
299 and advancements.

#### 300 3.1 State-of-the Art

301 *Nonlinear analysis of offshore structures and breaking wave analysis:* Dr. Kai Wei and Spencer  
302 Hallowell presented work of research groups at the University of Massachusetts Amherst and  
303 Northeastern University related to the post-elastic assessment of structural performance in the  
304 offshore environment and the role of breaking waves in driving extreme structural loads [57-62].  
305 Consideration of extreme events, such as hurricanes that can produce very high wind speeds and

306 wave heights [63-65], prompts the development of methods for evaluating the performance of  
 307 offshore wind structures after they have exceeded the elastic limit. In a case study of a jacket  
 308 structure, Wei presented methods and results that show how environmental models can be  
 309 converted to predictions of structural reliability, predictions that can inform risk-assessment of the  
 310 offshore infrastructure. Using a case study of the Blyth wind farm in the UK, Hallowell showed a  
 311 novel approach to identifying breaking wave events when only coarse data regarding the sea surface  
 312 elevations and structural response are available, and also quantified the large uncertainties present  
 313 in any assessment of breaking wave effects on offshore wind structures (Figure 2).



314 Figure 2. Method for identifying breaking wave events from recordings of structural response. High  
 315 frequency response in base moment of a monopile indicates slam load associated with breaking wave impact.  
 316  
 317

318 *Design and installation of the support structures for the Block Island wind farm:* Mr. Finucane, the  
 319 Block Island project manager for Keystone Engineering, presented the jacket designs (Figure 3)  
 320 that were installed in the summer of 2015 for the Block Island wind farm [66]. These jacket designs  
 321 build upon the expertise of the US in the design and construction of offshore oil and gas platforms  
 322 and are designed specifically for the US east coast environment, including the use of robustness  
 323 checks to assess the performance of the structures during hurricanes. Some important comments  
 324 were offered regarding the challenges of inspection and the possibility of repowering or extending  
 325 the life of support structures after the initial 20-25 year design life is exhausted. Discussion  
 326 addressed challenges of expanding offshore wind development to scale in the US and although  
 327 significant expertise exists already in the US a major bottleneck is likely to be installation vessels.



328  
 329 Figure 3. Block Island Wind Farm support structures (image courtesy Z. Finucane, Keystone Engineering)  
 330

331 *Anchoring and mooring systems for floating offshore wind turbines:* Mr. Senol Ozmutlu of Vryhof  
 332 Anchors presented current solutions for mooring floating platforms for offshore wind turbines.  
 333 Floating solutions hold the promise of eventually providing the vast majority of offshore wind  
 334 energy due to the mitigation of coastal impacts by the ‘over-the-horizon’ features of deeper water  
 335 development. US west coast development will likely require floating solutions. A very wide

336 variety of anchor types is available, each of which provides different capacities and requires  
 337 different installation systems (Figure 4). In order to make floating systems competitive for offshore  
 338 wind, greater efficiency and more streamlined design processes are needed. Key issues in mooring  
 339 and anchor design include redundancy, installation and retrieval.



340  
 341 Figure 4. Mooring and anchorage systems (Image courtesy S. Ozmutlu, Vryhof Anchors).  
 342

343 *Integrated design processes for wind turbine structures:* Arturo Rodriguez Tsouroukdissian of GE  
 344 Renewable Energy described an integrated design process in which the tower and foundation is  
 345 treated as part of the integrated wind turbine system rather than as a separate system design in  
 346 isolation to support the generating machine. Uncertainties in loading, materials, and design process  
 347 play an important role in developing such an integrated design process since, with integration, those  
 348 uncertainties must be propagated across domain boundaries (e.g. from aerodynamics to structural  
 349 dynamics). Although each of the component analysis models is well developed there is a need for  
 350 greater integration and coupling among the different subsystems and a key aspect is structural and  
 351 foundation damping. Integrated life cycle management framework are also key for post-installation  
 352 projects cost reduction and requires continuous and intensive data collection, which might bring a  
 353 lot of value to the developers and utilities and must be integrated into future developments.  
 354

### 355 3.2 New Achievements

356  
 357 This panel highlighted new achievements in the design, fabrication and installation of towers and  
 358 foundations. Methods for assessing the performance of offshore structures subject to extreme loads  
 359 and with behavior into the nonlinear range will allow more thorough, performance-based design  
 360 approaches to be implemented. The Block Island Wind Farm, first offshore wind farm in the US,  
 361 is now operational and has demonstrated the feasibility of constructing and operating an offshore  
 362 wind farm in US waters. Selection of jacket support structures also highlights the need to integrate  
 363 design, planning, and supply chain considerations. With the Hywind project currently being  
 364 installed off the coast of Scotland, the advent of commercial-scale floating systems has arrived, and  
 365 technologically advanced anchoring systems promise flexible and economical fabrication and  
 366 installation. Finally advances in modeling capabilities is for the first time allowing the support  
 367 structure to be treated integrally with the foundation and turbine in the modeling and design space,  
 368 promising increased efficiency and reliability.

### 369 3.3 Future Research Directions

370 Several promising directions for future research were identified, including:

- 371 • Improved models for operational and extreme structural loads
- 372 • Dramatically better methods for considering soil-structure interaction and
- 373 subsurface effects on structural performance
- 374 • Rationalized and streamlined design procedures for floating systems
- 375 • Increased construction and installation capability for offshore systems generally
- 376 • Risk-based framework for performance assessment of offshore wind structures
- 377 • Demonstration projects to prove numerical methods and environmental challenges.

378

379 *3.4 Summary*

380

381 The initiation of offshore wind construction in the US with the first commercial offshore wind USA  
 382 farm, Block Island, RI project (30MW – 5 GE Haliade 150-6MW) from Deepwater Wind, provides  
 383 opportunities and illustrated challenges as the US moves to deploy offshore wind at scale. In the  
 384 challenging offshore environment, with environmental and geotechnical conditions unique to the  
 385 US, greater attention must be paid to load and geotechnical uncertainty, and continuous monitoring  
 386 of coupled systems is needed to allow a truly integrated design paradigm to prevail.

387 **4.0 Topic A3 – Nacelle: Gearboxes, Rotors and Generators** (Lead: M. Inalpolat, Panelists  
 388 included: P. Haberlein, *Pattern*; R. Schkoda, *Clemson University*; W. Qiao, *University of*  
 389 *Nebraska-Lincoln* and J. Signore, *General Electric*)

390 Although reported to be improving recently [67], the components and subsystems within the nacelle  
 391 still cause the highest reliability and operability problems for a wind turbine in the field. Gearboxes  
 392 cause the longest downtime per failure with significant levelized cost of energy (LCOE) increases  
 393 [67, 68]. Electrical systems and generator problems have the highest failure rate and the average  
 394 downtime for a turbine in an operational year is reported to be ~170 hours [67, 68]. While wind  
 395 turbine OEMs, industrial and governmental agencies, wind farm operators and academic  
 396 institutions have been looking into ways to improve the reliability of the existing turbines, gradually  
 397 increasing size and power generation rates make this a continuously moving target and a  
 398 challenging effort. This section will discuss the main reliability and operability concerns, address  
 399 the gaps in the current state of the practice and the technology and indicate future direction for  
 400 improving the wind turbine nacelle-related components and subsystems. The main focus of the  
 401 discussions will be on the gearboxes (being the most problematic) with some emphases on  
 402 generators and rotors.

403 *4.1 State-of-the-Art*

404 Wind power captured by the blades of a wind turbine is transmitted by the main shaft to the gearbox  
 405 where it is speed-amplified. The mechanical energy transmitted by the gearbox usually has some  
 406 speed/frequency fluctuations and thus it is first frequency-rectified by the electrical inverters and  
 407 later converted into electrical energy by the generator. Wind loads are captured by the blades at  
 408 very low rotational speeds (~10-20 rpm) and high torque levels (depends on the turbine power  
 409 capacity). On the other hand, generators tend to like operating with lower mechanical input loads  
 410 and constant (with some tolerance) and relatively high rotational speed equal to the electrical  
 411 frequency (50 Hz/60 Hz depending on the country etc.) to be generated by the turbine. This requires  
 412 a high capacity and efficiency kinematic chain, gearboxes, to meet the both end goals.  
 413 Consequently, the highest mechanical loads observed in the nacelle are taken by the first planetary  
 414 gear stage of the gearbox generating relatively frequent mechanical failures. Unsurprisingly, the  
 415 bearings and gears in this stage along with the higher speed parallel axis gear stage have historically  
 416 been the most problematic parts of the gearboxes and the nacelle [68].

417 Drivetrains and gearboxes have been reported to be one of the major root causes of failures that  
418 cause the longest wind turbine downtime [67-69]. In fact, the majority of wind turbine gearbox  
419 failures (76%) are caused by the bearings per the latest reports by U.S. DOE NREL (National  
420 Renewable Energy Laboratory). An average size wind turbine gearbox is cost prohibitive (~  
421 \$500K) and in some cases costs even more to maintain over the lifecycle. This factor increases the  
422 importance of maintenance and the clever designs that allow shorter period and cost friendly  
423 maintenance cycles for keeping the turbines running[70]. Recently, the most pronounced  
424 challenges regarding the wind turbine gearboxes have been planetary gear bearing axial cracks due  
425 to dynamic loads and torque reversals, the lack of monitoring capabilities with high signal-to-noise  
426 ratio sensing, and difficulties in applying the outcomes learned from the laboratory and unison test  
427 boxes on the wind turbines.

428 Axial cracks that form on the bearings of the high- and intermediate-speed stages are the leading  
429 cause for bearing failures and are the focus of a joint research effort by NREL and Argonne  
430 National Laboratory to identify the root causes and develop mitigation measures. The recent  
431 investigations indicate that unexpected transient loads and load reversals cause frequent rolling  
432 element bearing failures in wind turbines in the field [71-73]. Several institutions in collaboration  
433 with NREL have initiated detailed investigations. NREL's GRC is well-aligned with this research  
434 effort and has unique experimental capabilities including a large-scale gearbox test dynamometer.  
435 The information about the test article and the dynamometer used is given in the previous NREL  
436 reports [74, 75]. Many researchers have also developed different scale and complexity analytical  
437 and computational models. Simplified lumped parameter and more advanced finite element based  
438 computational models were developed to model the dynamics of the test rigs and for benchmarking  
439 reasons [76-80]. The Ohio State University (GearLab), Technical University of Munich (FZG),  
440 Pennsylvania State University (GRI), NASA Glenn Research Center, Newcastle University, and  
441 Aachen University are some of the institutions with significant gear testing capability. More  
442 specific to wind turbines, Clemson University has a unique nacelle testing capability [81]. They  
443 have one 7.5 MW test facility readily available for testing the nacelle components by applying non-  
444 torque loads and measuring their effects on the mechanical as well as electrical systems. They also  
445 have a grid simulator to perform the tests on the electrical parts. University of Massachusetts  
446 Lowell, with its Center for Wind Energy Research, has the unique capabilities to perform the  
447 modeling and data processing for wind turbine drivetrain modeling [82, 83].

448 The condition monitoring technologies specifically developed for wind turbine gearboxes have  
449 mostly been matured to an extent. There are multiple monitoring hardware and software developers  
450 including General Electric's (GE) Bently & Nevada [84], Siemens' Gram & Juhl [85], Bachmann  
451 Electronics [86], Bosch Rexroth [87], Wolfel [88] along with many others in this market. Their  
452 gearbox monitoring technologies mostly rely on accelerometer-based vibration and thermocouple-  
453 based oil temperature measurements. Magnetic particle filters are also used in many new turbine  
454 gearboxes to filter out small chips and metallic particles that is generated and down to ~5  
455 micrometers in size [89].

456 However, it is challenging to implement the gearboxes with internal sensors because of the limited  
457 space and the harsh environment due to lubrication. This restricts some of the important  
458 components of the operations technology which are: (i) detection, (ii) accessibility, (iii)  
459 reparability, and (iv) reliability[70]. It also limits the achievable signal to noise ratios from the  
460 sensors used for the monitoring system. Development in feasible harsh environment sensing  
461 capabilities and high sensitivity measurement systems are clearly needed for further development  
462 of the wind turbine gearbox monitoring technologies.

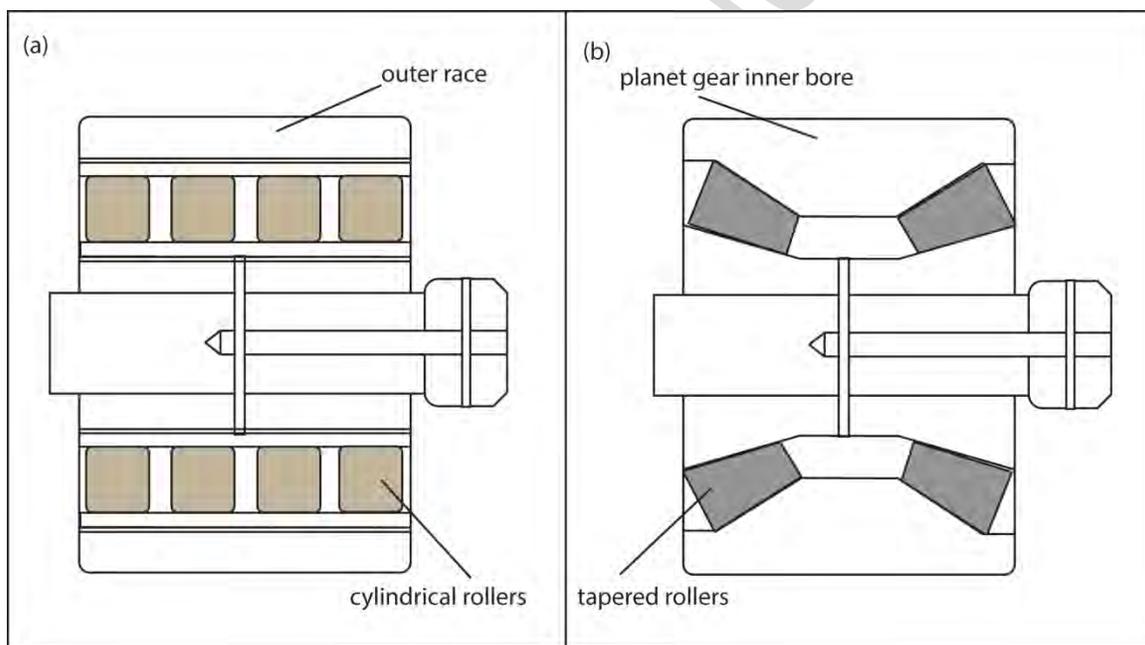
463 Continuously increasing rotor sizes requires not only architectural changes and optimization of the  
464 drivetrain designs, but also requires better understanding and controls of the system loads.  
465 Moreover, delivering reduced LCOE values drives more accurate and tighter design margins. This  
466 can be achieved by better system level modeling approaches and laboratory tests where the lessons  
467 learned can actually be applied on the full-scale turbine gearboxes. One of the gaps in this area is  
468 the need to find ways to measure the real-time loads on the drivetrain due to misalignments, bending  
469 moments, temperature variations and torque fluctuations. This is extremely challenging to do on a  
470 full-scale turbine up-tower. Consequently, the common practice is to do laboratory and unison tests  
471 on the ground [90]. This has been reported to generate loads, vibration levels etc. different than  
472 what has been experienced up-tower [91]. Better quasi-static and dynamic loads of the drivetrains  
473 and laboratory tests with less uncertainties, realistic boundary conditions and loads would close the  
474 gap in the future allowing greatly improved products. Some of the more recent adaptations by the  
475 wind industry to solve some of the other reliability and design problems have been using case  
476 hardened gears and bearings with higher contact fatigue endurance levels to avoid surface initiated  
477 pitting and subsurface initiated micropitting and cracking. Integrated outer race planet bearings  
478 used for the planetary gear stages have also been reported to increase the useful life of the gearboxes  
479 [92]. Flexible planet pins significantly improving the planet to planet load sharing is also reported  
480 to be a good design implementation for wind turbine planetary gears [93]. The main shaft has not  
481 been reported to be as problematic and has limited to no growth space in the research and  
482 development side. However, as the rotor sizes grow different bearing arrangements, balancing  
483 requirements and their relation to rotor bows and cracking will still be of interest and a focus area  
484 for researchers.

485 Generators are the key subsystems for power generation and their size, configuration and capacity  
486 selection becomes critical in determining the power generation capability of a wind turbine (along  
487 with other component sizes-blades, gearboxes etc.). Different generator types and technologies are  
488 available with certain misunderstanding and disagreements on which one is the best for certain  
489 turbine types. The three generalized categories for wind turbine generators are (i) DC generators,  
490 (ii) AC Synchronous generators, and (iii) AC Asynchronous generators [94]. Doubly-fed induction  
491 generator is a type of AC asynchronous generators and dominates the medium to large size wind  
492 turbine market at the moment. Permanent magnet synchronous generators are a type of AC  
493 Synchronous generators and dominate the small scale wind turbine market. The trend in generator  
494 applications and selection is towards variable speed and brushless types with reduced cost, weight  
495 and failure frequencies. Generator selection is also critical for new generation ideas such as “Direct  
496 Drive” turbines, where the drivetrain does not have a gearbox and only consists of a multiple pole  
497 generator that rotates at low speeds. The coupling between the mechanical components and  
498 subsystems and the electrical components should be investigated closely to understand the  
499 influence of torque ripples and generator feedback on the drivetrain etc. this requires better  
500 electromechanical models of the drivetrain coupled with the electronic components (inverters etc.)  
501 and the generator. The torque ripples generated by the input torque coming through the blades and  
502 feedback from generators back to the gearbox components have been observed to cause failures  
503 [95]. This may be avoided up to an extent using torque limiting couplings. However, these coupling  
504 cannot filter the dynamic torque ripples unless above a certain preset large value. Better health  
505 monitoring for avoiding these failures is needed. Use of generator output voltage fused with the  
506 vibration signals obtained from the driveline should be studied for better health monitoring. Further  
507 research and developments are also needed on prognostics of the drivetrain components and the  
508 generators to enable better remaining useful life prediction and smart maintenance scheduling.

509 *4.2 New Achievements*

510 There have been significant developments both in hardware and software related to the components  
 511 and subsystems in the nacelle. Some of the developments that were highlighted during the 2016  
 512 Wind Energy Research Workshop included: i) integral planet gear bearings, ii) stiffened dual row  
 513 tapered roller bearings for planet gears, iii) use of super-finishing for improved bearing/gear contact  
 514 surfaces, iv) case hardened ring gears, v) use of cleaner steel for manufacturing, vi) improved on-  
 515 line condition monitoring systems, vi) new system-level modeling and simulation tools, vii) hard  
 516 bearing coatings, and viii) improved drivetrain torque dampers. The benefits of these new  
 517 developments are summarized in this section.

518 Integral planet gear bearings are used mostly in the first planetary gear stage of the wind turbine  
 519 gearboxes. The inner bore of the planet gear is used as the outer race for the bearing that supports  
 520 this gear (see Figure 5). The motivation for using this integral design comes from the need for  
 521 higher power density, lower weight, better planet-to-planet load sharing, and reduced fretting on  
 522 the bearing races. Moreover, reduced number of parts help increase overall system reliability. The  
 523 use of new dual tapered roller bearings further increase system stiffness while keeping the planet  
 524 branches relatively flexible in the tangential direction that improves the planet-to-planet load  
 525 sharing. Tapered cylindrical rollers allow preloading of the bearing and thus the stiffness increases.  
 526 The combination of these two new design features have been reported to significantly reduce planet  
 527 gear rim deflections providing a life improvement of more than 150% [96-98].



528

529 Figure 5. The schematic description of (a) conventional four row cylindrical roller bearings, (b)  
 530 new integral dual row tapered roller bearings.

531 The new heat treatment and coating options also improve the overall gearbox reliability. Instead of  
 532 the conventional through-hardened gears, manufacturers now prefer case hardened (carburized)  
 533 gears. This way, they obtain gears with harder outer surface with higher strength and resistance to  
 534 contact fatigue, fretting and wear. At the same time, by only diffusing carbon into the outer surface  
 535 of the steel help retain a substantially lesser hardness levels in the gear core. As a result, the core is  
 536 protected from becoming brittle and retains a higher damping value in average. The use of cleaner,  
 537 white-etching resistance steels with fewer impurities and hard coatings assist with the mission of  
 538 increasing reliability of the gearbox. Recently, torque dampers have been developed to dissipate

539 the torsional shock loads on the drivetrain components, including gearboxes and rotors [99].  
 540 Moreover, wind farm owner and operators have much better handle in real-time operational  
 541 signature of drivetrain and generator with the improved on-line condition monitoring systems.  
 542 These systems mostly monitor the gearbox (mostly using accelerometers and thermocouples), main  
 543 shaft and generator bearings and main shaft (accelerometers) in real time and are helpful in  
 544 converting unscheduled maintenance into scheduled maintenance scenarios that are much less  
 545 expensive. There have also been new developments in software and modeling. System level  
 546 modeling tools allow design, analyze and optimize wind turbine nacelle components. These models  
 547 range from materials based simulation tools to topology optimization tools [100-102] and  
 548 immensely helpful in understanding system level fatigue life, dynamics and reliability.

549 **5.0 Topic B1: Offshore Installations and Siting** (Lead: D. Kuchma, Panelists included: T. Quiroz,  
 550 *Fraunhofer IWES*; J. Borkland, *APEX* and D. Degroot, *University of Massachusetts Amherst*)

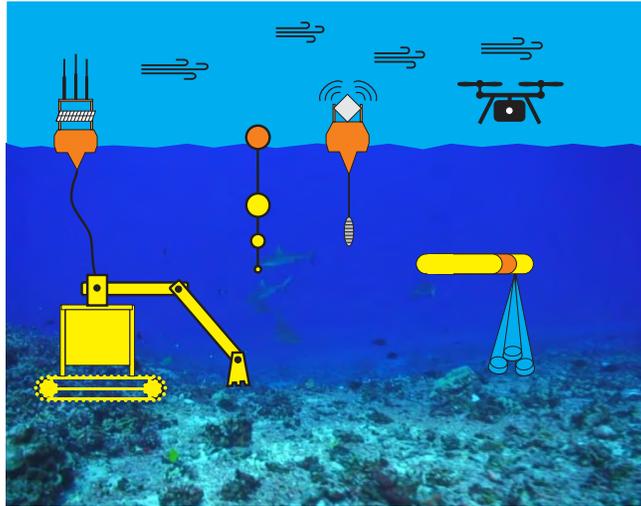
551 The objectives of this session were to: (i) provide a broad introduction to regulations controlling  
 552 the siting, installation and design of offshore wind turbine support structures; (ii) present an  
 553 example of recently completed site characterization study; (iii) present challenges in the US  
 554 environment, opportunities for improvement; and (iv) and describe the state-of-the-art in research  
 555 on installations.

556 *5.1 State-of-the-Art (as Presented by Four Panel Members)*

557 *“Regulation Frameworks and Requirements”* Dan Kuchma (Tufts University): There are a broad  
 558 array of national and international regulations that control the siting, design, and installation of  
 559 offshore wind turbine support structures[103]. They are developed and maintained by a number of  
 560 organizations including the American Petroleum Institute (API) [104], the International  
 561 Electrotechnical Commission (IEC) [105-107], the US Code of Federal Regulations (CFR), the  
 562 American Wind Energy Association (AWEA) [108], the American National Standards Institute  
 563 (ANSI), and others [109-112]. Most of these regulations are high-level documents that do not  
 564 provide comprehensive rules and guidance, and many of them were originally written to serve the  
 565 offshore oil and gas industry. Several organizations, including the Bureau of Ocean and Energy  
 566 Management (BOEM), the National Renewable Energy Laboratory (NREL), and AWEA, produce  
 567 guidelines and tools for working within this complex regulatory environment. The current state-of-  
 568 the-art is much less mature than for other types of structures and foundations (i.e. bridges and  
 569 buildings) for which there are comprehensive standards that have been developed by strong national  
 570 technical communities and matured over many decades. A particularly challenging aspect of  
 571 fulfilling regulatory requirements is that of site characterization. For this, BOEM is responsible for  
 572 ensuring compliance of lease holders and developers with CFR Part 585 – Renewable Energy and  
 573 Alternate Uses of Existing Facilities on the Outer Continental Shelf [113]. This includes the  
 574 conduct of surveys to assess wind, waves, currents, marine habitats, as well as the physical  
 575 characteristics of the seabed.

576 *“Integrated Geotechnical Engineering Site Investigation Practice for Offshore Wind Farm  
 577 Development”* Don Degroot (UMass-Amherst): Significant information is needed on the properties  
 578 of the seabed to properly select and design foundations, determine installation requirements, and  
 579 predict the short and long-term performance of offshore wind turbine support structures [114].  
 580 Surveys are used to obtain necessary information on Stratigraphy (soil types, spatial distribution,  
 581 slope stability), Initial State Variables (current and past geologic stress states), and Engineering  
 582 Properties (strength, stiffness, cyclic behavior). This survey information is gathered using  
 583 geophysical (acoustic methods) and geotechnical (borings and penetration) tests (see Figure 6).  
 584 Major challenges in conducting these surveys are the very large size of Wind Energy Areas

585 (WEAs), the high variation in local conditions, and that these very expensive investigations need  
 586 to be done with speculative monies (i.e. prior to a permit and in advance of power purchase  
 587 agreements). To illustrate this point, consider that the UK Dogger Bank WEA is one third of the  
 588 size of the state of Massachusetts, has extensive boulders that effect the location and installation of  
 589 the foundations elements (monopiles and other anchors), and the cost of the site investigation was  
 590 several tens of million pounds.



591

592 Figure 6. Approaches used for offshore site characterization.

593 *“Site Characterization and Installation”* Jay Borkland (APEX Corporation): The CFR that governs  
 594 site surveys are nearly identical to the requirements for the oil and gas industry. Factors that dictate  
 595 the cost of this work include the required spacing and width of measurement lines; resolution,  
 596 accuracy and types of required data; possible variation in soil properties; and how marine habitats  
 597 need by protected. Since creating the final development plan is often multiyear process, this survey  
 598 work usually needs to be done 2-4 times. Another challenge is that the data collected is often too  
 599 coarse to ensure ease of installation, with the effect of expensive problems in the field; daily costs  
 600 of installation vessels can exceed \$1M. European developers have gained substantial experience in  
 601 conducting site investigations, but in a notably different regulatory environment than in the US.  
 602 The ability to conduct more effective site surveys in the US will depend on the size of the pipeline  
 603 of projects (controls value of developing new technologies), and the regulatory authority’s interest  
 604 in adopting and promoting the use of improved technologies, methods, and requirements.

605 *“Improving Installation of Foundations for Offshore Wind Turbines by Realistic Testing”* Tulio  
 606 Quiroz López (Fraunhofer IWES): The Fraunhofer Institute for Wind Energy and Energy System  
 607 (IWES) technology has 500 employees and has created several state-of-the-art research facilities  
 608 for testing many of the components of an offshore wind energy system. This includes the support  
 609 structures test facility located at the University of Hannover which has a large soil pit (14m x 9m  
 610 x 10m) onto which different foundation systems can be installed and loaded. This facility makes it  
 611 possible to scientifically study different methods of installation (i.e. pounding, vibrating, pushing)  
 612 and the effect of high-cyclic loadings on the changing stiffness and strength of support conditions  
 613 for multiple types of foundation systems. The data collected from research in this facility is  
 614 critically important to the selection, design, and installations of foundation systems, and to validate  
 615 models used in the design, operation, and life-span assessment of offshore wind turbine support  
 616 structures.

617 *5.2 New Achievements*

618

619 There have been several recent developments that point to revolution changes in offshore siting  
 620 and installations. One the promising new directions in siting is that some countries and regions are  
 621 taking responsibility for conducting much of their own site characterization work (i.e. evaluating  
 622 winds, currents, waves, habitats, ecosystems, and engineering properties of the seabed). For  
 623 example, the Netherlands conducted detailed site characterization studies for the Borssele I-IV  
 624 wind energy areas prior to going to tender. This yielded by far the lowest strike price bid for wind  
 625 energy of its time in 2016 of €72.7/MWh by Danish Oil and Natural Gas (DONG) Energy. The  
 626 large reduction in cost is largely attributed to the de-risking of the project by the site  
 627 characterization. The German Federal Maritime and Hydrography Agency (BSH), which is the  
 628 regulator for German wind energy areas, has followed the lead of the Netherlands and is now  
 629 conducting their own site characterization in advance of the bid process. The New York State  
 630 Energy Research and Development Authority is also looking into directly funding the conduct of  
 631 site characterization in their wind energy areas. In addition to driving down price, the other  
 632 motivation for a country or region conducting the site characterization work is that the collected  
 633 data can be used for advancing science and other wind development projects; in the traditional  
 634 approach where the wind energy developer pays for the site characterization studies, the data is  
 635 nearly all proprietary. Another recent achievement is that public/private initiatives have been  
 636 maturing to provide data portals for public data; two examples of these are the UK's Marine Data  
 637 Exchange [115] and the Marine Environmental Data and Information Network (MEDIN) [116].

638

639 Major advancements and changes are also underway in installations. While >95% of offshore wind  
 640 energy foundations are monopiles, which are now up to 8 m in diameter and more than 80 m long,  
 641 many other foundation solutions are being developed and deployed in both demonstration and  
 642 commercial projects. The most significant of these are the use of "jackets", which is the type used  
 643 in the Block Island Wind Farm (see Figure 3). There are also a large number of foundation types  
 644 in projects in various phases of development that do not require pounding piles into the seabed.  
 645 These new developments include: (i) mono-suction buckets in Lake Eric; (ii) concrete gravity-base  
 646 structures that are floated to site and ballasted to rest on the ocean bed, as being deployed by BAM-  
 647 Nuttall in the Blyth field; (iii) floating spar buoys as used in Statoil's Hywind Scotland project; (iv)  
 648 the VoltturnUS floating concrete structures to be deployed off the coast of Maine in 2019; and (iv)  
 649 the Articulated Wind Column by ODE, MEES & DORIS Engineering that is designed for water  
 650 depths of 70-200 m. There are more than a dozen other foundation concepts that have been  
 651 developed and/or deployed. Most of these concepts are expected to have less environmental impact,  
 652 particularly in the area of noise effects on habitats. It is expected that the range of new foundation  
 653 types will greatly affect the needed regulations, and the areas of needed scientific and engineering  
 654 advancements, and of industrial developments.

655 *5.3 Future Research Directions*

656 Several directions for future research were identified. These include existing challenges as well as  
 657 promising future research directions.

- 658 - Review gaps and inconsistencies in regulations, and the challenge and value of improving  
 659 regulations
- 660 - Review the decision making process and identify opportunities for improvement and design  
 661 iteration
- 662 - Update CFR 585 site characterization requirements to be offshore wind specific and flexible
- 663 - Study formats for all survey data, and develop data structures and digital archival formats

- 664 - Identify opportunities for making proprietary data public, including the development of GIS
- 665 (geographic information system) based maps of existing and future WEAs (wind energy areas)
- 666 - Develop and/or improve material, component, and system testing standards
- 667 - Develop strategies for learning from installation and survey practices
- 668 - Investigate application of high resolution acoustic methods for determining boulders and other
- 669 seabed features that are impediments to installing monopiles and other anchor systems
- 670 - Develop methods to enable geophysical studies to better inform geotechnical investigation
- 671 - Develop improved and more cost-effective methods for guarding against disturbing marine
- 672 habitats
- 673 - Advancing laboratory testing techniques so to be able to conduct more fully realistic tests of
- 674 soil-foundation interaction, installation methods, and the impact of multi-degree of freedom,
- 675 complex, and high-cycle loading regimes
- 676 - Use of a next generation of measurement strategies in laboratory testing and field work so to
- 677 develop, calibrate, and validate models that have predictable accuracy.
- 678 - Investigate the use, and further develop, the capabilities of Autonomous Vehicles (underwater,
- 679 surface, and flying) for conducting multi-metric measurements
- 680 - Identify regulatory changes that would spur improvements in methods

681 The efforts of US federal organizations that support offshore wind should be better coordinated so  
 682 that a system-level approach to site characterization, impact assessment, design, installation,  
 683 operation, and analysis can be pursued. This system level approach should enable uncertainty  
 684 analysis, model validation, and the assessment of benefits of innovations on first costs, operational  
 685 costs, and lifespans.

#### 686 *5.4 Summary*

687 Offshore installations and siting practices are challenged by the multitude of regulatory  
 688 requirements, the deficiencies of many requirements, the size and complexity of the seabed, the  
 689 expense and difficulty of making site investigations, and the deficiency of our scientific  
 690 understanding of the short and long-term performance of the many different types of installations.  
 691 None of this should be surprising since the heavy offshore industry is only about a decade old, and  
 692 that the size and characteristics of the developments advance anything that mankind has previously  
 693 done in such a complex environment and ecosystem. There are many opportunities to improve  
 694 regulations and US practices, and this can be done providing that there is a pipeline of projects to  
 695 warrant the effort, incentives to make improvements, and an adaptive regulatory environment.

696 **6.0 Topic B2: Flow characterization** (Lead: R. Barthelmie, Panelists included: G. Qualley,  
 697 *Pentalum*; S.C.Pryor, *Cornell U.*; J. Manwell, *University of Massachusetts Amherst* and M.  
 698 *Wosnik, University of New Hampshire*)

699 One of the great challenges in wind energy is characterizing flow because meaningful time and  
 700 space scales cross many orders of magnitude. Natural and anthropogenic climate changes impact  
 701 wind resources and operating conditions on decadal and smaller time scales [117]. Quantifying  
 702 turbulence at sub-second time scales is important for fatigue loading [118]. In between these time  
 703 scales, annual variability of wind resources, seasonal and diurnal variability and planning of  
 704 maintenance and short term forecasting are examples of other timescales that are relevant for the  
 705 operation and economics of wind farms.

#### 706 *6.1 State-of-the-Art*

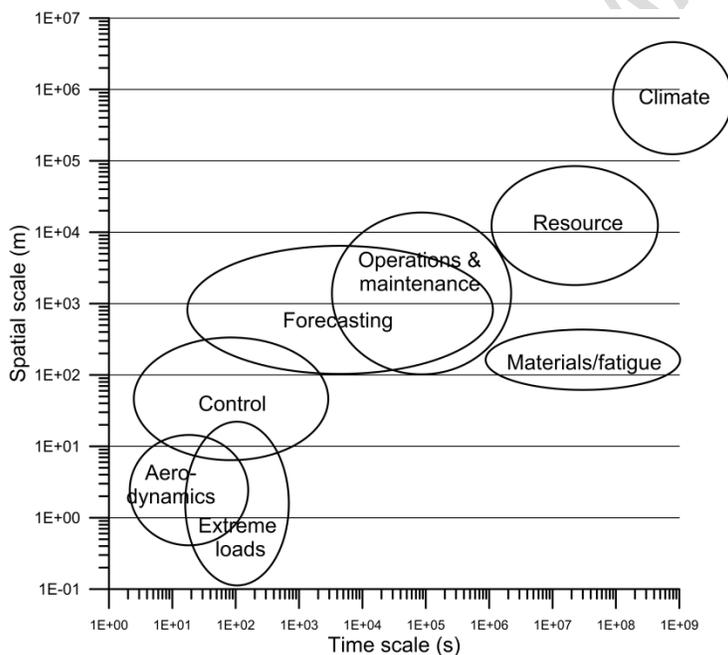
707 The state of the art in flow characterization includes a large range of measurement techniques from  
708 remote sensing (satellite derived observations [119] and ground based light detection and ranging  
709 or lidar) for wind and turbulence [120] to direct techniques including turbine mounted condition  
710 monitoring [121]. Professor R.J. Barthelmie, Cornell University, discussed the importance of wind  
711 turbine wake losses to overall power production and loads in large wind farm and their dependence  
712 on meteorological conditions [122]. There is a need to advance wake modeling that requires field  
713 measurements for wake characterization. Lidars are excellent tools for quantifying wake  
714 characteristics but are challenging in terms of defining scanning strategies, developing processing  
715 protocols and managing large data volumes [123]. It is essential for funding to become available  
716 for these type of full-scale field measurements using lidar, which are expensive, but quantifying  
717 the details of wake characteristics and behavior in the atmosphere cannot be found by model  
718 simulations alone. Grant Qualley from Pentalum described the SpiDAR lidar which operates by  
719 direct detection. The SpiDar [124] has a vertical range between 30-200m. The laser beam is directed  
720 in eight directions at an angle of 5 degrees from the vertical and thus makes a density map of  
721 aerosols in the atmosphere from which it can detect the volume of maximum reflection and the  
722 speed and direction in which it is moving. The small cone angle is better suited to deriving wind  
723 speeds in complex terrain where velocity can change rapidly in small change of height. It has a  
724 temperature range of  $-40^{\circ}\text{C}$  to  $60^{\circ}\text{C}$  and an easy user interface and is low power so can be operated  
725 with a portable solar panel and backup batteries. It is well suited to power curve measurements.  
726 Professor J. Manwell from UMass Amherst focused on the need for offshore wind data to estimate  
727 potential energy production. Data are essential to the design process of offshore wind turbines and  
728 their support structures [125] so is critical for developing and evaluating design conditions. It is  
729 likely that turbines deployed offshore will continue to grow in size (height and rotor diameter) so  
730 extending observations and model to beyond the surface layer (lowest 100 m of the atmosphere)  
731 will continue to be an urgent research need. Beyond using tall towers with anemometers at multiple  
732 heights, lidar is the only realistic option. Lidar are much cheaper to build and operate than tall  
733 towers in deep waters and can quantify wind shear and turbulence profiles. Lidar can be operated  
734 from fixed or floating platforms.

735 Similarly, a range of models is required from fundamental fluid dynamics through wind farm  
736 operation and modeling of turbine responses. Professor S.C. Pryor gave a comprehensive account  
737 of how and why climate change might impact regional wind resources operating conditions [126].  
738 Most current wind development areas are in mid-latitude storm tracks and so wind speeds are  
739 affected by the location of mid-latitude cyclone storm tracks, their frequency and intensity. These  
740 are driven by the intensity of the equator to pole temperature gradient the location of the storm  
741 tracks steered by the jet stream and the intensity of cyclones is impacted by momentum transport  
742 and the latent energy from water vapor. Global climate models can simulate these changes but  
743 downscaling to the regional level is required using either dynamical or probabilistic methods [127].  
744 There is great potential for improved modeling future wind climates using new and advanced  
745 techniques such as the application of adaptive grid global model, finding optimal resolution for  
746 regional model applications and hybrid downscaling including statistical techniques such as  
747 machine learning.

748 In addition to the range of available numerical simulations (RANS, LES, DNS), full-scale and  
749 scaled wind farms Professor Martin Wosnik from the University of New Hampshire elaborated the  
750 role of wind tunnels of varying scales in modeling large wind farms. Over these multiple scales for  
751 testing, full scale measurements and SWiFT [128] have to manage varying conditions while large  
752 rotor scale facilities work in controlled conditions but cannot model the far downstream wake. For  
753 example, very large wind tunnel such as the one at New Hampshire [118] have controlled  
754 conditions and can evaluate wake evolution to 20 D downstream.

## 755 6.2 New Achievements

756 As indicated, flow characterization is complex because of the order of scales that have to be  
 757 resolved in both time and space for a very wide range of applications in wind energy (Figure 7).  
 758 The introduction of lidar suitable for measuring wind speeds to the required precision and accuracy  
 759 has been the greatest achievement in measurement technology in recent years and new  
 760 developments are continuing to expand the range of scales that can be measured (both larger and  
 761 smaller than the first vertical lidars that measured over a similar range to sodar i.e. about 200 m in  
 762 the vertical at a resolution of 10-20 m). In addition, a number of companies are working on  
 763 introduction of lidars at reduced cost – these may have a reduced measurement range or be used  
 764 for specific functions such as power curve measurements. For offshore, lidar have a big advantage  
 765 in that, even if a specific platform is required, the foundations need not be as extensive as required  
 766 for a very tall mast. Further, developments in floating and nacelle-mounted lidar may eliminate the  
 767 need for fixed platforms altogether. The availability of lidar that can scan in detail over large  
 768 volumes are starting to provide process-level detail of wind turbine wakes and their interactions.  
 769 Nonetheless, most applications in wind energy are model-based. The increased availability of  
 770 computing resources means that variability of wind resources can be characterized over long-scales  
 771 and the drivers of this long-term variability can be understood and included in economic forecasts  
 772 and risk assessment. Improvements in model including the development of large-eddy simulation  
 773 models for smaller scales (<1 km) but developments in computing and modeling techniques are  
 774 expanding the range and types of issues that can be tackled. Further work is needed to bridge the  
 775 scales of modeling. Lastly, experiments in wind tunnels enable the conditions to be controlled to  
 776 evaluate process-level responses. The development of new large-scale wind tunnel facilities is  
 777 enabling high Reynolds number experiments that are more similar to atmospheric flows.



778

779 Figure 7. Integration of wind energy systems crosses many orders of magnitude in both temporal  
 780 and spatial scales.

## 781 6.3 Future Research Directions

782 In terms of future research funding the importance of inter-disciplinary research is likely the most  
 783 critical element. As elaborated above there is no individual model or experimental technique that  
 784 can answer all questions regarding flow across so many temporal and spatial scales. In addition to  
 785 modeling and measurements/experimental validation of wind farms and wind turbine wakes that  
 786 extend to tip heights and across multiple scales beyond are required. New approaches are needed  
 787 such as development of a continuum of finite models could be built into a platform that is truly  
 788 elastic across spatial and temporal scales. More integration of numerical tools for full physics based  
 789 engineering models for turbine-atmosphere interactions will start to produce more integrated  
 790 simulations on both power and turbine loading that can then start to address realistic control  
 791 strategies. More effort needs to be expended in quantifying assessment of variability on longer-  
 792 time scales and potential changes in turbine operating conditions. Many industries already use  
 793 limited modeling but the industry is not ready for more advanced models until better  
 794 characterization of wind farms is available.

795 Lastly, beyond the critical element of research funding, some challenges that could be addressed  
 796 include better sharing of resources and leveraging of existing data and closer ties between industry  
 797 and academia. Last but not least we need to create a more inclusive environment to encourage more  
 798 women and minorities to join the wind energy field.

799 **7.0 Topic B3: Characterization of Loads, Waves and Wind** (Lead: A. Myers, Panelists included:  
 800 A. Kirincich, *WHOI*; L. Manuel, *University of Texas Austin*; A. Yamaguchi, *University of Tokyo*,  
 801 D. Arora, *Alstom* and Z. Finucane, *Keystone*)

802 Designing structures for the offshore environment is a fascinating example of a multi-hazard  
 803 situation where hazards, such as wind speed and turbulence intensity, wave height and period,  
 804 current and others contribute to structural loads. While all of these hazards can be generated by  
 805 multiple sources, extreme values of these hazards often result from a common source, such as a  
 806 hurricane or winter storm. This creates important correlations of the hazard in both space and in  
 807 time. In this session, the focus was characterization of wind, wave and loads for offshore wind  
 808 energy structures. Specific topics covered included (1) estimation of metocean conditions for  
 809 offshore wind farms in regions exposed to loads from tropical cyclones, (2) the evolution of coupled  
 810 loading from wind, wave and current during hurricanes, (3) the use of lidar to characterize wind  
 811 speed shear and low-level jets and evaluate power performance for offshore sites, (4) remote  
 812 sensing of spatially varying offshore winds using land-based radar, and (5) the loads analysis used  
 813 for the design of the support structures for the US's first offshore wind farm off the coast of Block  
 814 Island, Rhode Island.

815 *7.1 State-of-the-Art, (as Presented by Five Panel Members)*

816 *"Estimation of metocean conditions for offshore wind farms in tropical cyclone-prone regions"*  
 817 Atsushi Yamaguchi (University of Tokyo): The most widely used design standard, IEC 61400-  
 818 3[105], requires that the design of offshore wind turbines include loading from storm conditions,  
 819 defined as the wind speed, wave height, and current with a 50-year recurrence period. The most  
 820 common method for estimating these conditions is the Measurement-Correlation-Prediction (MCP)  
 821 method with statistical extrapolation of measurements [129]. This method has been successfully  
 822 applied to the design of many wind farms across Northern Europe, however, farms at these  
 823 locations are not exposed to risk of tropical cyclones. As wind farms begin to be installed in  
 824 locations exposed to tropical cyclone risk, there are many questions about how the MCP method  
 825 compares with alternative approaches, such as Monte Carlo simulation of synthetic tropical  
 826 cyclones [130], which are designed specifically to assess tropical cyclone conditions. The Monte  
 827 Carlo approach is shown to be a useful tool for assessing condition in locations exposed to tropical

828 cyclones. Wind speed can be modeled with the Monte Carlo approach using a standard pressure  
829 field model, combined with a tropical cyclone specific vertical wind profile model and site-specific  
830 local terrain modification based on CFD. Wave height can be modeled with the Monte Carlo  
831 approach with numerical models such as SWAN [131-133], but it's important to also consider the  
832 contribution of winds outside of the tropical cyclone wind field.

833 *“The influence of offshore wind turbines of couple wind, waves, and currents during large-scale*  
834 *storms”* Lance Manuel (University of Texas Austin): An “integrated” framework to assess design  
835 loads for wind turbine loads would combine loads with external conditions determined by a coupled  
836 physics model of the air and sea and their interface [134]. This is a complex engineering problem,  
837 but shows promise for refining future editions of design standard and load cases. One particular  
838 coupled model, developed at the University of Miami, [135, 136] combines a hurricane atmospheric  
839 model (WRF) [137] with a wave model (UMWM) [138] and an ocean model (HYCOM) [139] with  
840 an interface model to couple and air-sea physical processes. This model has been applied to study  
841 the relative importance of swell versus wind seas for hydrodynamic loading, aerodynamic versus  
842 hydrodynamic loading including second-order wave kinematics, and the effect of yaw  
843 misalignment on loads for a monopile during Hurricane Ike and a jacket during Hurricane Sandy  
844 [140]. These applications of this coupled model have shown that realistic inputs are possible to  
845 assess coupled offshore conditions during hurricanes, but requires some scale bridging to achieve  
846 turbine-scale resolution [134].

847 *“Wind profile characterization for offshore mid-Atlantic US”* Dhiraj Arora (General Electric):  
848 Extensive measurements in the onshore environment have shown that winds in a stable atmospheric  
849 boundary layers have higher wind shear than winds in an unstable or neutral atmospheric boundary  
850 layer and that the stable atmospheric boundary conditions frequently result in low level jets [141].  
851 In the offshore environment, similar measurements are scarce, but the limited existing data from  
852 Europe has suggested that a stable atmospheric boundary layer does not occur over the ocean.  
853 Recently, lidar measurements of wind for two offshore sites in the US (in the Atlantic Ocean near  
854 Virginia [142] and in Lake Michigan [143]) have shown that the winds were highly sheared, often  
855 showing characteristics of low level jets, unlike the European measurements which showed  
856 infrequent occurrence of low level jets. The presence of the low level jets at the two US sites can  
857 reduce power performance by 2-5%.

858 *“High resolution remote observations of oceanic surface winds using HF radar”* Anthony  
859 Kirincich (Woods Hole Oceanographic Institution): The efficiency of offshore wind installations  
860 can be increased with (1) better estimates of the spatially-distributed wind energy resource at  
861 various locations and (2) more accurate short-term forecasts of the spatially dependent wind field.  
862 A novel approach, based on an existing network of onshore high frequency radar sensors, has the  
863 potential to provide both of these improvements by empirically relating surface wind speeds with  
864 measurements of radar energy loss due to scatter caused by sea surface waves. For wind speeds  
865 between 2 and 6 m/s, the optimal range for the frequency of the radar, this method is shown to  
866 estimate spatially distributed wind fields with accuracy of ~1 m/s. This approach has potential to  
867 improve offshore site characterization, monitoring and forecasting.

868 *“Block Island wind farm loads analysis”* Zach Finucane (Keystone Engineering): The first utility-  
869 scale offshore wind farm in the United States is located off the coast of Block Island, Rhode Island  
870 [66]. The farm includes five 6MW turbines, each supported by a four-legged 400t jacket and a 300t  
871 deck. This project is the first of its kind in many regards and required the clearing of several  
872 technical and practical obstacles. In particular, the loads analysis for these structures was based on  
873 the novel “Partially-Coupled” methodology. In this methodology, aero- and hydrodynamic loads  
874 are analyzed in GH Bladed [144]. The results of these analysis are combined with a detailed

875 structural model of the jacket in SACS [145] to obtain rational estimates of combined aero- and  
 876 hydrodynamic loads. The jacket and deck structures for this project were installed in Summer 2015  
 877 and the turbines and towers are expected to be installed in Summer 2016.

## 878 *7.2 New Achievements*

879 The information in this panel highlighted several new achievements relevant to the offshore wind  
 880 energy industry including (1) demonstration of comparable uncertainty in the estimation of extreme  
 881 winds during tropical cyclones using Monte Carlo and MCP methods and demonstration of the  
 882 importance of modeling wind conditions outside of the tropical cyclone wind field when estimating  
 883 extreme wave heights, (2) showcasing of the potential of a coupled air-sea model in estimating  
 884 loads on offshore wind energy structures, (3) evidence of the frequency of occurrence of low level  
 885 jets for locations off the United States Atlantic coast and the negative impact of these jets on the  
 886 power output of offshore wind turbines, (4) a description of a novel idea, which uses existing high  
 887 frequency radar sensors to estimate wind field information and short-term forecasts that can  
 888 increase the efficiency of offshore wind turbines, and (5) a summary of the novel loads analysis  
 889 which was used to design the first utility-scale offshore wind farm in the United States.

## 890 *7.3 Future Research Directions*

- 891 - Develop consensus for considering tropical cyclone/hurricane conditions in the design of  
 892 offshore wind turbines
- 893 - Advance coupled physical models of the air and sea to improve characterization of offshore  
 894 environmental conditions during storms and estimation of structural loads during such  
 895 conditions
- 896 - Understand the character of the vertical wind profile at offshore wind locations in the U.S. and  
 897 use this understanding to better estimate wind farm performance and structural loads.
- 898 - Develop cheaper, more accurate and spatially-distributed methods for measuring the offshore  
 899 wind resource and making short-term forecasts of the wind field
- 900 - Identify and investigate design approaches and software tools for rationally estimating coupled  
 901 aero- and hydrodynamic loads on offshore structures

## 902 *7.4 Summary*

903 Offshore structures, such as those supporting offshore wind turbines, require the accurate  
 904 estimation of environmental offshore conditions during extreme events such as hurricanes and  
 905 during operational conditions. Such estimates should ideally consider both measurements and  
 906 models of the environment. If offshore structures are to be designed optimally, the environmental  
 907 conditions must then, in turn, be linked to accurate estimates of structural loads and power  
 908 performance. This session considered several innovations with potential to improve environmental  
 909 modeling, structural loads modeling, environmental measurements and structural design.

910 **8.0 Topic C1: Controls, Power Production and Wind Farms** (Lead: M. Rotea, Panelists  
 911 included: J.W. vanWingerden, *TU Delft*; A. Wright, *NREL* and F. D'Amato, *General Electric*  
 912 *Global Research*)

913 Wind turbine and wind farm control schemes play a significant role in lowering the levelized cost  
 914 of energy (LCOE) and increasing the installed wind energy capacity. The market has created  
 915 several areas where controls have or are expected to have a strong influence: increasing power

916 capture, reliability and grid responsiveness, lowering the LCOE, and accelerating the turbine and  
917 farm design cycles.

918

### 919 *8.1 State-of-the-Art*

920

921 Successful wind turbine and wind farm control systems require effective implementation of  
922 sensors, algorithms and actuators. Current single turbine control algorithms [146-149] yield a wide  
923 range of results under different conditions. Collective blade pitch actuation has been studied  
924 extensively, however current research suggests that individual pitch control (IPC [150, 151]) and  
925 advanced control surfaces[13] may have some advantages. In regards to wind farm control  
926 algorithms [27, 152, 153], efforts are being made to develop and unify control algorithms in a  
927 systematic multivariable framework. However there still exist open fundamental questions  
928 concerning the most desirable wind farm control mechanisms as well as control system  
929 architectures and algorithms. Axial based control mechanisms, such as adjusting the rotor speed  
930 [154] or blade pitch angle [155] have received more attention from researchers. Yaw based wake  
931 steering [156] appears to offer another viable alternative in regards to farm-scale production  
932 maximization and steady/unsteady blade load reduction.

933

934 Several models are being developed to study axial and yaw based control approaches. SOWFA  
935 (Simulator for Wind Farm Applications [27]) is a high fidelity, multi-scale dynamic model under  
936 development by NREL that is attempting to unify farm-scale control schemes with farm-scale  
937 dynamic simulation in mesoscale atmospheric boundary layers. Currently, line actuator models and  
938 lookup tables are used to characterize the turbine blades. Yaw based optimization has been  
939 performed with encouraging results. UTD-WF [157] is another high fidelity Large Eddy Simulation  
940 package to predict power in wind farms and loads in the turbines. This code uses actuator line  
941 models or actuator disk model to compute forces and it incorporates an immersed boundary method  
942 to model turbine details and topography. These high fidelity simulation tools typically aim to  
943 capture larger scale wake turbulence evolution and dissipation while using lower fidelity models to  
944 represent the impact of the turbine blades on the flow. Lower fidelity models are commonly used  
945 to represent the turbine due to the large disparity in turbulence scales observed in the turbine blade  
946 boundary layer versus the overall wind turbine wake. On the other end of the fidelity spectrum,  
947 farm-scale ROMs (Reduced Order Models) are also in use and under development. These lower  
948 fidelity models are popular due to their rapid estimation of the turbine performance and wake  
949 evolution. To gain the benefit of computational efficiency, these models do not simulate the  
950 detailed flow around the turbine or the wake and often rely on integral conservation of mass,  
951 momentum and/or energy expressions. The models typically require some parameter tuning or  
952 some dimensional reduction from higher fidelity computational simulations or experiments. The  
953 FLORIS (FLOw Redirection and Induction in Steady state [152]) model employs enhanced  
954 versions of classical analytic formulations with site specific tuning parameters, wake deflection  
955 models and wake deficit blending schemes. A dynamic extension is also being developed  
956 (FLORDyn [153]) that uses a time lag approximation to convect wake parameters downstream.  
957 DD-RANS [158] is a data-driven Reynolds-averaged Navier–Stokes model for estimation of wake  
958 effects and power production. These models are sufficiently fast to perform optimization and  
959 control studies and retain accuracy through careful reduction of the model physics and/or data  
960 assimilation. Finally, methods using differential deficit control volume analysis are being examined  
961 to decrease solution time while retaining fast simulation times [159]. Overall, despite the reduced  
962 fidelity, reduced order computational models are still powerful tools for modeling and optimizing  
963 windfarm power output.

964

965 Low cost sensors and actuators help lower the LCOE and contribute to a successful wind farm  
966 control scheme. Lidar technology has become an effective, relatively low cost solution for

967 estimating large area wind fields. Lidar is a tool that can deliver real-time site information to a  
968 dynamic model and execute real-time dynamic optimization. However, the use of lidar for wind  
969 farm control is yet to be explored.

970

## 971 *8.2 New Achievements and Future Research Directions*

972

973 Many challenges exist in implementing advanced controls. Control algorithms are typically  
974 a *hidden* technology. The turbine manufacturer under the manufacturer's contract maintains the  
975 control software. This may represent an intellectual property hurdle for innovation in the control  
976 space. In addition, there are still fundamental questions concerning control strategies. These  
977 questions require experimental testing (wind tunnel, field experiments) to obtain answers that guide  
978 future development. Some studies have looked at load reduction, others have examined power  
979 optimization; however, the integration of the two is work in progress.

980

981 Advanced wind farm controls will require dynamic models, efficient solvers, and robust objective  
982 functions that can account for the uncertainty associated with the wind resource knowledge. At  
983 present there is nothing available to industry in terms of a reliable dynamic model that is capable  
984 of farm optimization. Future models may be physics based and data driven. Model-based control  
985 solutions need to be complemented with model-free approaches for wind farm control. A promising  
986 model-free approach requiring further investigation is extremum seeking control for wind farms  
987 [160, 161]. This method has been field tested in a single experimental turbine with encouraging  
988 results; i.e., 12% and higher improvements were demonstrated in the energy capture of the NREL  
989 600 kW experimental turbine known as the CART 3.

990

991 Integrated design is another significant area for future development. Controllers and turbine  
992 properties can be optimized in an aero-structural simulation environment. Rotor design  
993 methodology can be advanced by developing fast and robust models to aid in design optimization.  
994 This may lead to new control surface designs that employ IPC as well as individual blade surface  
995 control. Structural control is also envisioned as a means to allow for the larger turbines of the  
996 future[162].

997

998 New technologies must also be investigated. Several of potential new research areas were  
999 identified. A pumping system was discussed wherein a cluster of turbines may pump water to a  
1000 single central generator, similar to Garcia-Gonzalez [151]. The potential of movable offshore  
1001 turbine platforms was also discussed briefly. These platforms could be repositioned on-the-fly  
1002 based on current wind knowledge and simulations. A similar concept was identified by Haier [163].

1003

1004

1005

## 1005 *8.3 Summary*

1006

1007 Numerical simulation, model reduction, and frameworks for control system design and analysis are  
1008 seen as areas where government and academia have aligned interests and may be able to work  
1009 together. Academic research works well when risks are high. Universities tend to have the resources  
1010 to develop new algorithms. Government can bring ideas from academia to industry through field-  
1011 testing, proof of concept studies, and equipment testing/monitoring. Common themes across the  
1012 presentations and question session were that controls are driving the current generation of wind  
1013 development and advanced controls can drive the next generation. The speakers highlighted  
1014 research opportunities related to all three aspects of wind-farm control: sensing, algorithms and  
1015 actuation. The potential exists for field testing new wind-farm control concepts in facilities such  
1016 as the Scaled Wind Farm Technology (SWIFT) facility that possesses 3 fully instrumented wind

1017 turbines. This could lead to fruitful collaborations and assets leveraging between government,  
1018 academia and industry.

1019

1020 **9.0 Topic C2: SHM, Sensing, Diagnostics, Testing, Reliability** (Lead: C. Niezrecki, Panelists  
1021 included: S. Sheng, *NREL*; N. Post, *NREL*; L. Breuss, *Bachmann* and J. Paquette, *Sandia*)

1022

1023 One of the most important metrics for wind turbine performance and successful implementation is  
1024 the levelized cost of energy (LCOE). The LCOE is the net present value of the unit-cost of  
1025 electricity over the lifetime of a generating asset and is typically considered as the average price  
1026 that the generating asset must receive in a market to break even over its lifetime. The factors that  
1027 structural health monitoring (SHM) systems and turbine component testing influence in the  
1028 calculation of the LCOE include: the Initial Capital Cost (ICC), Levelized Replacement Cost  
1029 (LRC), Operations and Maintenance Costs (O&M), and the Annual Energy Production (AEP).  
1030 SHM systems and testing do add cost to a turbine thereby increasing the ICC, however as an  
1031 example for blades, it has been estimated that blade SHM systems yield an \$807/year/turbine cost  
1032 benefit over the same turbine with no blade SHM system [164]. SHM systems and testing increase  
1033 performance, reliability, and turbine availability, which positively affect the LRC, O&M, and the  
1034 AEP. Advancements in SHM and testing systems will enable new technologies that will reduce  
1035 the time and cost required for unnecessary wind turbine down time, maintenance, and failures. An  
1036 improvement in reliability will help to accelerate the deployment of U.S. and global based wind  
1037 energy by lowering the LCOE.

1038 *9.1 State-of-the-Art*

1039 Condition monitoring systems (CMS) are typically used for monitoring rotating machinery  
1040 including the drivetrain components (e.g. main bearing, gearbox) and the generator [165-169]. The  
1041 most common approach uses accelerometers to measure vibration along with temperature sensors  
1042 for transformer and generator monitoring. Gearbox oil CMS focuses primarily on measuring the  
1043 particle contamination in the lubricant fluid and is not widespread in the industry. Borescopes are  
1044 used by some to perform visual inspections internally of gearboxes and also some blades. One of  
1045 the primary challenges that exists with respect to CMS systems is the large number of components  
1046 involved with complicated and multiple failure modes. Approximately 76% of gear box failures is  
1047 due to bearings and about 17% of failures are due to gears. A large issue is white etching cracks,  
1048 which is a dominant failure mechanism for almost all bearings. Several root cause hypotheses have  
1049 been developed, but none have been completely verified.

1050 For blades the primary downtime issues include: rotor imbalance, trailing edge disbonds, leading  
1051 edge cracks and erosion, edge-wise vibration, lightning, and icing (see Figure 8). Manufacturing  
1052 induced defects (in- and out-of-plane laminate waves), typically in the spar cap can lead to stress  
1053 amplifications that cause cracks and premature failure. Icing is an issue that impacts performance  
1054 and reliability and current algorithms to detect icing sometimes shut turbines down leading to loss  
1055 of energy production.

1056

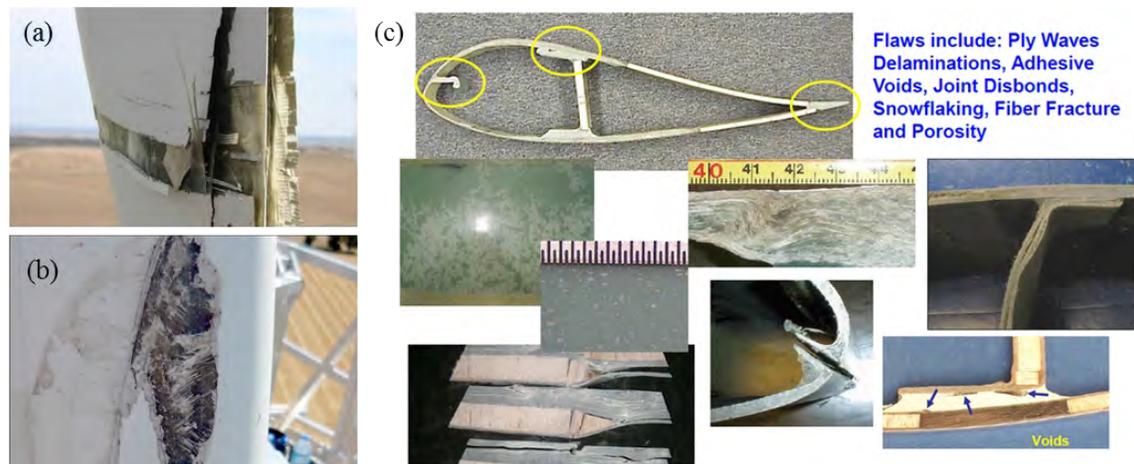


Figure 8. (a) Trailing edge blade damage [170]; (b) leading edge blade damage; (c) various blade inspection areas and common flaw types of interest [171].

Lightning strikes are an issue in the USA primarily in the region between Texas to Manitoba and approximately one lightning strike occurs per turbine per year. In North America Vaisala [172] can identify the location where lightning strikes have occurred. In other areas it would be beneficial to put in an equivalent system to track lightning strikes. A diverter strip usually only works once because a lightning strike will usually decouple the strip from the structure. Unfortunately, the responsibility is put on the owners by the OEMs to demonstrate that the lightning protection system did not work if installed and the OEM will typically claim extenuating circumstances to void warranties. Lightning strikes are somewhat random, sometimes hitting the leading or trailing edge and leading to the puck at the tip of the blade. There can be extenuating circumstances that make it difficult to assess that the lightning protection systems work. For example, water or hydraulic system leaks tend to flow to the tip of the blade causing degradation of the electrical protection. The lightning systems seem to work but the significant problem is catching the damage and effecting repairs in a timely manner before the damage grows. Although lightning damage doesn't always result in a blade being removed from service, it usually will lead to eventual blade failure.

SHM systems have advanced over the last two decades and some of the related background can be found in [173-176]. SHM for wind turbines typically includes the blades, tower, and foundation. The traditional sensing approaches (e.g. strain-gage networks, acoustic emission sensors, fiber optic cables, ultrasonic, laser-Doppler sensing, and piezoelectric transducers) heavily depend on contact-type measurement sensor arrays that are either difficult to instrument, challenging to maintain, unreliable, costly, ineffective in identifying and localizing distributed damage, or are impractical to be implemented in service. For example, accelerometers are generally used for detection of icing on blades but not for damage detection. Likewise, past research has demonstrated conclusively that modal frequencies [177, 178] and mode shapes [179] are by themselves poor indicators of damage. Significant changes in experimental mode shapes and natural frequencies exist only in the presence of very severe damage. Most commercially available SHM systems rely on sensing vibration (e.g. accelerometers) or strain. For blades, there are very few commercially available monitoring systems and they are generally only used to monitor for ice accretion by observing changes to the blades resonant frequency. A laser based position sensitive system is commercially available by Bachmann that can measure blade deflection in the flap-wise direction. As the blade ages, the stiffness is reduced which leads to an increased blade deflection for a given amount of power. The increased deflection due to decreased stiffness can be used to help predict remaining life. Another approach to measure blade damage includes using the blade cavity

1095 acoustics via active and passive measurement techniques [180]. A ground-based microphone was  
1096 able to measure the acoustic Doppler shifts of a rotating turbine in which external acoustic pressure  
1097 fluctuations were a direct result of blade damage and infrared cameras have been used to detect  
1098 thermo-elastic and frictional heating from damaged blade material due to cyclic loads [181].  
1099 Thermal imaging is starting to be done during operation to identify leading and trailing edge splits.  
1100 Thermography is used to detect localized damage in blades by using a heat source and observing  
1101 damage. These blades are inspected on the ground. Tower vibration monitoring systems are also  
1102 being used track tower motion and perform rainflow fatigue analysis.

1103  
1104 To assist in improving turbine reliability and performance several testing facilities exist. The Wind  
1105 Technology Testing Center (WTTC) in Charlestown, MA and the National Wind Technology  
1106 Testing Center (NWTC) in Boulder, CO have the capability to test and certify utility-scale blades  
1107 and are operated by the Massachusetts Clean Energy Center and NREL respectively (see Figure 9).  
1108 There are also other blade test facilities at the University of Maine and Clarkson University. These  
1109 facilities measure dynamic loads for model verification, perform nondestructive evaluation and  
1110 accelerated structural testing, as well as blade certification. Testing is typically performed in a  
1111 single axis (flapwise or edgewise) or bi-axis configurations by exciting the first flap or first lead-  
1112 lag mode shape using a moving mass (shaker) on the blade or a hydraulic actuator. During a test  
1113 the mode shape (bending moment distribution) is adjusted by adding masses as required. The  
1114 torsion strain measurement needs to be accounted for when considering the bending moments and  
1115 forces on the blade, and should be applied to models and fatigue testing. Significant errors occur  
1116 when not accounting for cross-sensitivity using strain gages to make bending moment  
1117 measurements on wind turbine blades.

1118  
1119 Sandia National Laboratories (SNL) runs the Scaled Wind Farm Technology (SWiFT) facility that  
1120 possesses 3 instrumented wind turbines that are being used to help understand turbine wakes (see  
1121 Figure 9). With a suite of mechanical, aerodynamic, and wake imaging sensors capable of making  
1122 high-fidelity measurements, the facility will help model validation and verification data gathering.  
1123 SNL also runs the Blade Reliability Collaborative (BRC) while NREL runs the Gearbox Reliability  
1124 Collaborative (GRC) that help to resolve issues related to manufacturing, transportation,  
1125 installation, and operation of blades and gearboxes that can have large effects on COE as failures  
1126 can cause extensive down time and lead to expensive repairs. SNL also possesses a Wind Turbine  
1127 Blade Test Specimen Library in which different researchers can quantify the performance of  
1128 different inspection techniques on prepared samples. One objective is to generate industry-wide  
1129 performance curves to quantify how well current inspection techniques are able to reliably find  
1130 flaws in wind turbine blades. Montana State University possesses a Multi-Scale, Multi-Axis Test  
1131 Facility to test sub-components in a variety of test configurations (combined loading: flexural  
1132 bending plus and torsion). The facility allows for characterizing materials as an intermediate step  
1133 between coupon and full-scale testing. NREL's GRC investigates gearbox dynamic responses  
1134 under different loading conditions through both dynamometer and field testing of utility-scale wind  
1135 turbine gearboxes, along with modeling & analysis to identify possible gaps in gearbox design  
1136 standards, compiling gearbox failure event statistics to catalog top failure components and modes,  
1137 and condition monitoring to improve operations and maintenance of wind turbines with a focus on  
1138 gearboxes. To characterize wind turbine and wind plant reliability performance issues and identify  
1139 opportunities for improving reliability and availability performance within the wind industry, SNL  
1140 also runs the Continuous Reliability Enhancement for Wind (CREW) Database and Analysis  
1141 Program [183].

1142



1143  
1144

1145 Figure 9. (a) SWIFT Facility, Lubbock, TX [170] ; (b) Flap fatigue test at Wind Technology  
1146 Testing Center, Boston, MA-NREL from NREL Image Gallery #34756; (c) Inertial mass flap  
1147 fatigue test at National Wind Technology Center, Boulder, CO, from NREL Image Gallery #16269  
1148 [182].

1149

1150 It is also important to mention that NREL and Clemson University can test multi-MW drivetrains  
1151 and nacelles at the Dynamometer Test Facility at the NWTC and the SCE&G Energy Innovation  
1152 Center in Charleston, SC, respectively. Additionally, both the NWTC and the Clemson facility  
1153 allow for testing of wind turbine generators and have Hardware-In-the-Loop grid simulators  
1154 allowing manufacturers to test both mechanical and electrical characteristics of their machines in a  
1155 controlled and calibrated environment.

## 1156 9.2 Future Research Directions and New Achievements

1157 There are several new technologies that have the potential to disrupt wind turbine monitoring and  
1158 reliability. The first is a new inspection technique for blades that leverages infrared scans for blades.  
1159 This approach scans a turbine while a blade is in operation during the night. The scans reveal  
1160 the presence of defects and damage due to an increased heat radiation from the damaged area [184,  
1161 185]. Another approach uses microphones to identify the presence of cracks and holes in blades  
1162 either in a passive or active monitoring configuration [186, 187]. Finally, the recent increase in  
1163 performance and capability of unmanned aerial vehicles (drones) to perform inspection of a wind  
1164 turbine or farm is currently revolutionizing how turbine inspection and monitoring is being  
1165 performed. Several companies are actively involved in wind turbine drone inspection (e.g.  
1166 Advanced Aerial Inspection Resources, AeroVision Canada, AirFusion, Availon, Brains4Drones,  
1167 LLC, Cyberhawk, Deutsche Windtechnik, ECI, GeoDigital, HUVRData, InspecTools, Pro-Drones,  
1168 Skeye B.V., SKYDRONE UAVs, Sky-Futures, SkySnap, Strat Aero, UpWind Solutions, Ventus  
1169 Wind, WindSpect, and others) [188].

1170

1171 There is a need in both CMS and SHM to identify new techniques or technology to improve sensing.  
1172 For SHM and inspection, distributed and large area sensing techniques are needed and currently  
1173 fall short because of cost, implementation challenges, wiring, or data transmission issues. It is  
1174 highly desirable for a small number of sensors to be able to interrogate what is happening  
1175 throughout the structure. Current sensors largely do not provide details about the health or status  
1176 of the blade. Normal blade inspection is primarily performed using ground-based telescopes, but  
1177 drones are starting to be used. The software behind the drone and the experience of the  
1178 interpretation of the operator or engineer is what adds value. The drone itself is not a significant  
1179 cost. Drone inspection is in its infancy and presents numerous opportunities for future blade and  
1180 tower inspections.

1181

1182 For blades, inspection techniques are needed that can identify and quantify flaws and damage that  
1183 include: ply waves (in- and out-of-plane), delaminations, adhesive voids, joint disbonds,

1184 snowflaking, fiber fracture, and porosity. Ultrasonic inspection is effective, but can only scan a  
 1185 small area and it is time consuming and impractical to analyze a large blade. The structural integrity  
 1186 of a composite laminate repair or the effect of an embedded defect compared to an undamaged  
 1187 structure in wind blades is poorly understood. Water droplets and sand can impact leading edge  
 1188 erosion and there is no field evaluation of whether water or sand is more significant. The  
 1189 performance of leading edge protection systems are dependent on who applies them and their long-  
 1190 term effectiveness remains unclear. The meteorology and understanding of the icing problem is  
 1191 not well understood. A better understanding of the performance of a lightning protection system's  
 1192 effectiveness is needed along with a better assessment of what quantifies a lightning strike. The  
 1193 interpretation of the IEC standard is somewhat unclear. It remains unclear if moisture build up in  
 1194 the blade composite or within the blade cavity impact the blades. Some would argue that a  
 1195 breathing phenomenon that initiates the bond stresses leads to transverse cracks in blades, but this  
 1196 phenomenon is not well understood. A better understanding of how the resonant frequency on an  
 1197 installed blade or turbine changes over time when the blade is operating in normal use is needed.  
 1198

1199 There are no physical measures on the actual turbine blades in operation. A better set of distributed  
 1200 sensors is needed to understand the loads imparted on the blades while in operation. There appears  
 1201 to be a gap between the actual loads that are applied to the operating blade compared to the loads  
 1202 that are applied during design, modeling, and blade testing. The correlation between damage  
 1203 assessed in testing to the damage assessed in the field is unclear.

1204 With regard to signal processing and monitoring, improvements in diagnostic decision making is  
 1205 needed. There needs to be more confidence and better interpretation of the data for damage  
 1206 detection (e.g. fatigue damage accumulation assessment), prediction, and prognosis for wind farm  
 1207 operators. Once condition based damage is identified during operation, maintenance needs to be  
 1208 made easier, streamlined, and automated.

### 1209 *9.3 Summary*

1210 SHM, CMS, and testing systems for wind turbines are continually advancing but numerous places  
 1211 for improvement exist. As improvements are made, so will come a more reliable and efficient  
 1212 turbine that is less expensive both to install and to operate. These advancements will help to drive  
 1213 down the LCOE and make wind energy systems more cost competitive and widespread.

1214

## 1215 **10.0 Topic C3: Energy Storage, Grid, & Transmission** (Lead: J. Hunter Mack, Panelists include: 1216 S. Blazewicz, *National Grid*; D. Alderton, *NEC Energy*; F. Brushett, *MIT* and A. Sakti, *MIT*)

1217 An increase in electricity from renewable resources presents a new set of technological challenges  
 1218 not previously faced by the grid. This includes the variability of renewable sources and the location  
 1219 of renewable resources far from population centers [189]. The variability of renewable resources,  
 1220 due to characteristic weather fluctuations, introduces uncertainty in generation output on the scale  
 1221 of seconds, hours and days [190]. Greater uncertainty and variability can be dealt with in a few  
 1222 ways: (1) by switching in fast-acting conventional reserves as needed on the basis of weather  
 1223 forecasts, (2) by installing large scale storage on the grid, and/or (3) by long distance transmission  
 1224 of renewable electricity enabling access to larger pools of resources in order to balance regional  
 1225 and local excesses or deficits.

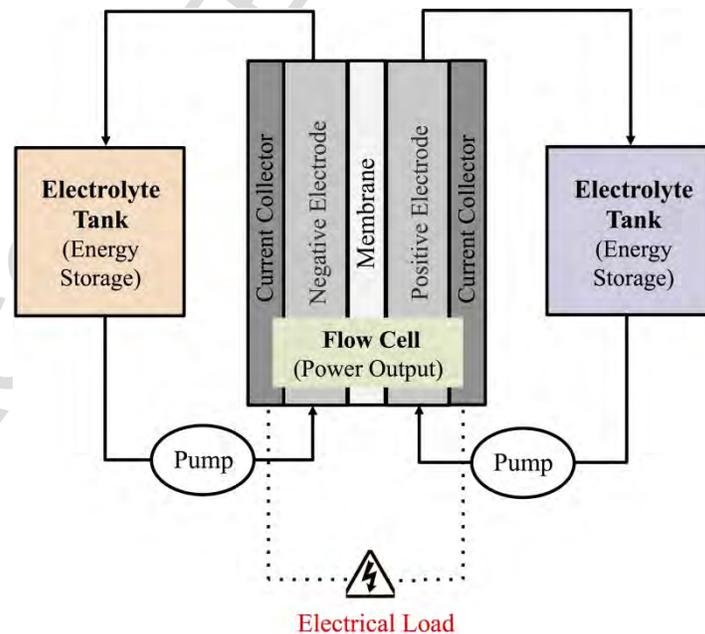
### 1226 *10.1 State-of-the-Art*

1227 Currently, a number of approaches are being proposed as possible energy storage solutions  
 1228 including pumped hydro, compressed air, batteries, thermal storage, and flywheels [191]. Each  
 1229 technology is able to address variances in the electricity supply caused by the intermittent nature  
 1230 of renewable energy sources (such as wind), though their efficacy is varied with respect to short-  
 1231 term and long-term storage. The most well developed approach is pumped hydro, where excess  
 1232 electricity is used to transport water to a higher elevation. When this electricity is required, the  
 1233 water is then run downhill and converted to back to electricity using a turbine or other mechanical  
 1234 conversion approaches. While this approach is inherently geographically limited, it still receives  
 1235 significant interest due to relatively high efficiencies and ease-of-use considerations [192].

1236 Compressed air energy storage is currently in use commercially in a few different configurations  
 1237 [193]. The approach uses energy to compress air, either in large underground caverns or smaller  
 1238 distributed containers; the air is then used to power a turbine to generate electricity on demand  
 1239 [194]. Flywheels store energy by accelerating a rotor and maintaining the energy in the system as  
 1240 inertial energy [195]. One advantage of flywheels is a relatively fast response rate, which makes  
 1241 them quite suitable to peak-shaving applications.

1242 Another proposed storage approach stores energy as chemical energy in the form of hydrogen, most  
 1243 likely generated via the electrolysis of water. The hydrogen can then be stored, blended with other  
 1244 fuel streams, or converted to electricity using a fuel cell or internal combustion engine. Hydrogen-  
 1245 based storage technologies have a great potential for long-term storage applications, but the main  
 1246 challenge to their adoption is related to economic uncertainty due to high system costs [196].

1247 Several types of batteries are used for large-scale energy storage including lead-acid batteries,  
 1248 lithium-ion batteries, nickel-cadmium batteries, sodium-sulfur batteries, and flow batteries such  
 1249 as vanadium redox or zinc-bromine [197]. One of the problems with lithium-ion and sodium-  
 1250 sulfur batteries, which can have high power and energy densities with high efficiencies, is that they  
 1251 have high production costs [190, 198]. Redox flow batteries exhibit very high potential for several  
 1252 reasons, including power/energy independent sizing, high efficiency, room temperature operation,  
 1253 and extremely long charge/discharge cycle life [199, 200]. An example of a redox flow battery is  
 1254 shown in Figure 10.



1255

1256 Figure 10. Diagram of a redox flow battery for energy storage (courtesy: Ertan Agar)

1257 In terms of transmission and the grid, much of the infrastructure is aging and unable to handle non-  
1258 traditional generation sources and large-scale storage. Investment and clear policy guidelines are  
1259 needed to support the continued evolution of how electricity is distributed reliably and at a low-  
1260 cost to the consumer. Wind energy faces distinct siting challenges that other renewable sources  
1261 such as solar do not, which adds to the complexity of transmission infrastructure.

#### 1262 *10.2 New Achievements*

1263 A significant amount of progress has been made towards increasing efficiencies and lowering costs  
1264 of the various approaches to energy storage highlighted above. The continued development of  
1265 advanced materials, including graphene-based materials, zeolites, aluminophosphates, and metal-  
1266 organic frameworks promises to push the boundary of these technologies [201, 202]. Since the  
1267 widespread adoption of energy storage not only relies on technological advances, but also systems-  
1268 level analysis and validation [203]. Therefore, progress in the techno-economic analysis of  
1269 deployments, based on both early-stage and demonstration projects, has helped quantify and  
1270 elucidate the benefits of energy storage. Furthermore, an increased interest in micro-grid and smart  
1271 grid applications, has shown promise in limited applications with the potential to positively affect  
1272 the current approach to transmission [204].

#### 1273 *10.3 Future Research Directions*

1274 The continued expansion of energy storage within the grid relies heavily on advancing the current  
1275 portfolio of proposed solutions and identifying new approaches, all while creating a regulatory and  
1276 infrastructure backbone that supports the efforts. The adoption of grid-scale energy storage to  
1277 complement the expansion of intermittent renewable energy sources faces many key challenges  
1278 [205], including:

- 1279 • Understanding the economics of each proposed storage technology for different scales and  
1280 applications
- 1281 • Development of new materials with respect to both electrochemistry and mechanical  
1282 properties
- 1283 • Improved system-level compatibility and performance
- 1284 • Pursuit of revolutionary designs, concepts, and architectures that can significantly reduce  
1285 capital and maintenance costs with low environmental impact
- 1286 • Improved safety and reliability

1287 As personal transportation increasingly relies on electric vehicles, the increased battery  
1288 development has helped drive costs down through design and manufacturing improvements while  
1289 increasing efficiencies and reliability [206, 207]. Research in advanced materials and mechanical  
1290 design show promise in improving the performance of high-speed and low-speed flywheels. The  
1291 efficient splitting of water into hydrogen and oxygen has further enabled fuel cell and internal  
1292 combustion engine approaches; advanced thermodynamic approaches such as the argon power  
1293 cycle getting increased traction [208]. The cost of flow batteries, both aqueous and nonaqueous, is  
1294 progressively seen as a viable approach [209].

#### 1295 *10.4 Summary*

1296 A variety of grid storage solutions currently exist, each of which has distinct advantages or  
1297 disadvantages based on economics, capacity, and geography. Technological advances, in

1298 conjunction with clear policy and regulatory approaches [209, 210], will shape how wind energy  
1299 and other renewable resources are integrated into the electrical grid. Continued research into  
1300 material challenges facing mechanical, thermochemical, and other conversion technologies will  
1301 undoubtedly target issues with cost, efficiency, and reliability in order to address the needs of the  
1302 grid.

### 1303 **11.0 Overall Paper Summary and Conclusions**

1304 This review paper presented the findings of the 2016 Wind Energy Research Workshop. From the  
1305 summary of the current state of the art, it is clear that in the past two decades significant progress  
1306 has been made on improving and deploying wind energy. Federal funding of wind energy research  
1307 coupled with positive policy has encouraged researchers, government laboratories as well as  
1308 industry to commit to the improvement of wind energy as not just a viable player, but a leader in  
1309 the renewables market.

1310 The future research directions that derived from this workshop illustrate the vibrant and exciting  
1311 potential wind energy research has in academia, government laboratories and industry. As wind  
1312 energy research continues into the future, industry-academia-research laboratory collaborations  
1313 will be critical in defining productive pathways forward. Finally, the sharing of information at this  
1314 workshop prompted further calls for sharing information, data and research results in a timely and  
1315 open manner between industry, academia and government researchers. While this poses challenges  
1316 in a competitive market economy, it is believed that significant benefit could be derived for all in  
1317 such an endeavor.

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## Highlights

### **Wind Energy Research: State-of-the-Art and Future Research Directions**

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- This paper summarizes the 2016 Wind Energy Research Workshop held in Lowell MA:
  - Wind Turbine Design and Manufacturing (Blades, Towers/Foundations, and Nacelle)
  - Wind Farm Development (Offshore Installations, Flow/Load/Wave Characterization)
  - Wind Farm Operations (Controls, Structural Health Monitoring, Energy Storage/Grid)