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1 Abstract

Activated carbon from oak tree is used as adsorbent for the removal of noxious anionic dye 2 sunset yellow. The prepared adsorbent is characterized using X-ray diffraction, Scanning 3 4 Electron microscopy equipped with Energy-Dispersive X-ray spectroscopy and Fourier 5 transform infrared spectroscopy. In addition to this, parameters like initial concentration, 6 adsorbent dosage, contact time, pH, and particle size on the uptake of SY dye from wastewater is well investigated and optimized. For maximum adsorption, the initial concentration of 10 mg/L; 7 adsorbent dose of 0.25 g; pH =1; contact time= 35 min and particle size=150-250 µm is found to 8 be optimal value. The adsorption isotherm data at different adsorbent dosage of 0.05- 0.25 g is in 9 agreement with the Langmuir isotherm having Qmax = 5.8377- 30.1205 mg/g. On the other 10 hand, models like, Group Method of Data Handling and multiple linear regression were used to 11 12 forecast of the removal efficiency of noxious anionic dye sunset yellow and from results, it is specified that the GMDH model possess a high performance than MLR model for forecasting 13 removal percentage of SY dye. Hence, activated carbon from oak tree can be efficiently used as 14 adsorbent for the removal of SY dye from wastewater. 15

16 Keywords: Adsorption, anionic dye SY, Adsorption kinetics, Isotherms, Modelling

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- 18 19 20 21 22 23

1 1. Introduction

Groundwater and surface water has been exploited due to several noxious impurities and 2 among all chemical dyes is one of the most detrimental impurity that possess serious 3 environmental side effect on human being and marine life (Garg et al., 2003; Tanzifi et al., 2018; 4 5 Yao et al., 2018 Gupta et al., 2011b; Gupta et al., 2013a). Synthetic dyes and pigments are 6 widely utilized as colorants in different industrial processes including the pharmaceutical, textile, leather, paper, gasoline, food industries etc. and a huge amount of unused synthetic dyes is being 7 released in water streams by various industries worldwide annually. Dyes being colored in nature 8 is visible even at very low concentration and it resistive nature also decreases the sunlight 9 penetration in water. Therefore, their release into the environment presents a major source of 10 contamination (Gupta et al., 2013b; Gupta et al., 2014; Tian et al., 2018). Dyes molecules are 11 12 normally produced from the aromatic structure and their degradation products are toxic or even carcinogenic and mutagenic. In addition to this, it lead to increased biological oxygen demand 13 (BOD) and chemical oxygen demand (COD) levels of aquatic resources (Crini, 2006; Nekouei et 14 al., 2017). Thus, it is the need of today to eliminate the toxic dyes from effluents of industries, 15 before it is released into the environment. 16

Several technologies for instance flocculation–coagulation (Szygula et al., 2009; Wang et al., 2012), photodegradation (Gupta et al., 2011c; Smirnova et al., 2015; Tadjarodi et al., 2013), biodegradation (Li et al., 2004), membrane separation(Bouazizi et al., 2017; Chen et al., 2017; Ruan et al., 2016; Saravan et al., 2013; 2015; Tahri et al., 2016), aerobic or anaerobic treatment (Fernando et al., 2013), electrochemical (Aquino et al., 2010; Riera-Torres and Gutiérrez, 2010), and oxidizing agents (Ghoneim et al., 2011) have been used worldwide for the removal of noxious dyes from wastewater. In spite of the growth of different techniques for treatment of dye

1 effluent, but still there are some specific challenges, for example effective, rapid and economic for treatment of water and wastewater at a commercial level are going on. Among these methods 2 for water treatments, the adsorption technique by solid adsorbents is one of the most efficient 3 approaches for the uptake of dyes from industrial wastewater (Gupta et al., 2011a). The key 4 5 advantage of this technology is that it is scalable and large volume of effluents can be passed in a 6 single run, which lead to high quality of treated wastewaters without the formation of harmful materials (Gupta et al., 2010b). This technique currently can widely be used to remove or 7 minimize diverse kinds of organic and inorganic contaminants from the aqueous media (Jain et 8 al., 2003). One of the best and effective adsorbents, which are the most extensively employed for 9 the treatment of wastewaters containing dyes, is activated carbon (Auta and Hameed, 2011; Li et 10 al., 2011; Martins and Nunes, 2015) which due to its large surface area and high porosity lead to 11 12 high adsorption capacity. However, two factors i.e. expensive and low regeneration rate of the commercial activated carbon restrict their usage (Crini, 2006). A rising interest has recently been 13 observed in the use of alternative low cost non-conventional adsorbents including agricultural 14 waste, industrial waste, etc. for the adsorption dye from wastewater (Malik, 2003; Mall et al., 15 2005; Prakash Kumar et al., 2005). Hence, the studies in order to obtain more efficient and 16 economic adsorbents with the higher adsorption capacity and better reusable are continuing. 17

Nowadays, artificial intelligence (AI) approaches for instance artificial neural networks (ANNs), random forest (RF), adaptive neuro-fuzzy inference system (ANFIS) and support vector regression (SVR) have broadly utilized for modeling of adsorption processes, which these models can be generated more accurate outcomes than conventional techniques. Group method of data handling (GMDH) neural network is one sub-model of ANNs, which has been widely and successfully used in different fields of engineering and science. The researchers showed that

GMDH tool could be utilized as a successful technique in the modeling of various processes 1 (Abdolrahimi et al., 2014; Atashrouz et al., 2014; Najafzadeh and Azamathulla, 2012). Recently, 2 Yousefi and Razavi used the GMDH network to estimate the amounts of glucose release from 3 native and modified wheat starch gels during digestion under simulated gastrointestinal 4 5 conditions (Yousefi and Razavi, 2017). Varamesh et al. (Varamesh et al., 2017) developed the 6 GMDH as a predictive modeling method for estimation of the critical properties of pure chemical compounds. Dargahi-Zarandi et al. (Dargahi-Zarandi et al., 2017) utilized GMDH as modeling 7 technique for forecasting the viscosity of pure hydrocarbon and gas mixtures including heavy 8 components and impurities for instance nitrogen, carbon dioxide and helium. Barzegar et al. 9 (Barzegar et al., 2017) developed a hybrid wavelet-GMDH model for prediction of groundwater 10 level fluctuations. 11

There were no reports on the use of the GMDH model for prediction of the adsorption process. This led us to use GMDH for forecasting the uptake of SY onto AC prepared from oak tree wood as cost-effective adsorbent. The produced adsorbent was considered by XRD, SEM-EDX and FT-IR spectroscopy techniques. The uptake efficacy of AC was considered under the important variables including particle size, contact time, concentration of dye, adsorbent dosage and pH of solution. Furthermore, the kinetics and isotherm of the adsorption process was considered.

19 **2. Materials and methods**

20 **2.1. Materials and instruments**

All chemicals i.e. SY dye (Molecular Structure is shown in Fig.1a), FeCl₃, HCl, NaCl and NaOH were supplied from Merck (Darmstadt, Germany). The dye concentration of the solution is determined using a Perkin Elmer UV–Vis spectrophotometer (Lambda 25, USA) and the pH

of the solution is measured using a Metrohm 686 pH meter (Herisau, Switzerland). A Bruker
AXS powder X-ray diffractometer (D8 advance, Bruker, Germany) was used to obtain the X-ray
diffraction (XRD). A scanning electron microscope (SEM, VEGA3 TESCAN model) equipped
with energy dispersive spectroscopy (EDS) was used to consider the morphology and elemental
composition of the prepared AC. Fourier transform infrared spectroscopy (FTIR) was achieved
by a Perkin Elmer Fourier transform infrared spectrometer (spectrum 65, USA).

7 2.2. Preparation of AC

Oak tree trunk timbers (OT) were employed as a precursor to prepare the activated 8 carbon. In order to eliminate the foreign materials, distilled water is used for washing, which is 9 later on dried at 120 °C for 12 h and cut into smaller pieces of about 2-3 mm. The materials were 10 mixed with 15 % FeCl₃ solution (ratio of 1g: 10mL), and soaked at room temperature for 24 h. 11 12 Then, the extra of FeCl₃ solution was decanted and modified OT pieces were then dried at 110 °C for 24 h. The treated TO pieces were exposed for carbonization for 1 h at 550 °C under 13 vacuum using a muffle furnace. It is later on cooled to room temperature and then soaked in 0.1 14 mol/L hydrochloric solution acid (ratio of 1g: 10mL) for chemical activation of the activated 15 carbon at room temperature for 24 h and then washed with distilled water several times, the 16 obtained washed product is then finally dried at 120 °C. These ACs were sieved to acquire the 17 required particle size to study adsorption. 18

19 **2.3. Adsorption experiments**

The dye stock solution in the concentration of 1000 mg/L was used to prepare the dye solutions at specified concentrations using distilled water. The NaOH and HCl solutions were applied for adjusting the dye solutions pH. Each experimental run was performed in 100 mL Pyrex glass beaker including 50 mL of dye solutions with required concentration, quantity of

adsorbent, pH, contact time and particle size at room temperature. At the end of each
 experimental run, the solutions were filtered with Whatmann filter paper and the dye
 concentration was determined using the collected supernatant. The following equations were
 used to calculate the percent of removal (R%) and capacity of uptake (q), respectively.

5
$$R \% = \frac{(C_0 - C_t)}{C_0} \times 100$$
 (1)
6 $q_t = \frac{(C_0 - C_t)V}{W}$ (2)

where C_0 shows the dye initial concentration (mg/L), C_t represents the time t the dye concentration (mg/L), V indicates the solution volume (L), W displays the adsorbent weight (g) and q_t shows the time t uptake capacity of adsorbent (mg/g).

10 **2.4. Group method of data handling (GMDH)**

The GMDH (Fig. 1b) is a heuristic self-organizing principle-based learning machine in which a quadratic polynomial function was used to obtain each layer. Volterra–Kolmogorov–Gabor (VKG) polynomial can evaluate the relation between the input variables and the output variable. Ivakhnekoin as shown in the following equation has firstly suggested the general polynomial function of GMDH model (Ivakhnenko, 1968).

16
$$\hat{y} = a_0 + \sum_{i=1}^n a_i x_i + \sum_{i=1}^n \sum_{j=1}^n a_{ij} x_i x_j + \sum_{i=1}^n \sum_{j=1}^n \sum_{k=1}^n a_{ijk} x_i x_j x_k + \cdots$$

17 (3)

18 The simplified equation to a quadratic polynomial containing of only two variables can be19 written as:

20
$$\hat{y} = a_0 + a_1 x_i + a_2 x_j + a_3 x_{ij} + a_4 x_i^2 + a_5 x_j^2$$

21 (4)

where \hat{y} , a and x indicate the anticipated output, the coefficients of polynomial set by algorithm and the input variables, respectively. The main objective in the GMDH model was obtaining a

function that is expected to output this function close to the experimental outputs. Therefore, to
obtain the GMDH structure objective function should be minimized, which it can be described
as:

4
$$e = \sum_{i=1}^{n} (\hat{y}_i - y_i)^2$$
 (5)

where y_i represents the experimental data. Minimization of Eq. (5) can be employed to calculate the values of the coefficients of polynomial (a). These parameters can be computed from multiple regression using the least squares method, which can be achieved by solving the following matrix:

$$9 \quad A = Y^T Y \tag{6}$$

10
$$Y = (1 \ x_i \ x_j \ x_i x_j \ x_i^2 \ x_j^2)$$
 (7)

11
$$X = (a_0 \ a_1 \ a_2 \ a_3 \ a_4 \ a_5)$$
 (8)

12

$$13 \quad A = \begin{bmatrix} 1 & x_i & x_j & x_i x_j & x_i^2 & x_j^2 \\ x_i & x_i^2 & x_i x_j & x_i^2 x_j & x_i^3 & x_i x_j^2 \\ x_j & x_i x_j & x_j^2 & x_i x_j^2 & x_i^2 x_j & x_j^3 \\ x_i x_j & x_i^2 x_j & x_i x_j^2 & x_i^2 x_j^2 & x_i^3 x_j & x_i x_j^3 \\ x_i^2 & x_i^3 & x_i^2 x_j & x_i^3 x_j & x_i^4 & x_i^2 x_j^2 \\ x_j^2 & x_i x_j^2 & x_j^3 & x_i x_j^3 & x_i^2 x_j^2 & x_j^4 \end{bmatrix}$$
(9)

$$14 b = (yY)^T (10)$$

15 The equations can be written as:

16
$$\sum_{i=1}^{n} AX = \sum_{i=1}^{n} b$$
 (11)

17 2. 5. Assessment of models

For assessing the reliability and precision of the suggested models, mean square error
 (MSE) and determination coefficient (R²) were employed.

20
$$MSE = \frac{1}{n} \sum_{i=1}^{n} ((O_i)_{exp} - (O_i)_{prd})^2$$
 (12)

1
$$R^2 = 1 - \frac{\sum_{i=1}^{n} ((O_i)_{prd} - (O_i)_{exp})^2}{\sum_{i=1}^{n} ((O_i)_{exp} - O_m)^2}$$
 (13)

where (O_i)_{exp} shows the *i*th actual value, (O_i)_{prd} presents the *i*th predicted value, and O_m
indicates the mean value of (O_i)_{exp}.

4

5 **3. Results and discussion**

6 **3.1. Characterization of adsorbent**

7 The surface functional groups of the prepared AC is investigated using FTIR and the obtained spectrum is indicated in Fig. 1c. The produced AC revealed several major absorption peaks. The 8 bands achieved at 2931, 2874 cm⁻¹ are due to the C-H stretching, and -CH₃ group of alkane, 9 while the peaks in the range of 2850-3000 cm⁻¹ may be assigned to the dimer OH group of 10 carboxylic acids. The band at 1723 cm⁻¹ shows the C=O stretching. The peaks in the region 11 1400-1505 cm⁻¹ may be assigned to the C-C stretching of aromatic groups. The bands in the 12 range of 1000-1320 cm⁻¹ are attributed to C-O stretching mode in carboxylic acids. The band at 13 731cm⁻¹ indicates the C-H mode out of plane. 14

The XRD pattern of the prepared AC is illustrated in Fig. 1d. The presence of sharp and broad peaks reveals that the AC is both crystalline and amorphous structures. The crystalline nature is about 26% while the amorphous nature is about 74%. Therefore, the XRD results show a mostly amorphous nature of the prepared AC with low crystallinity. The peaks detected in XRD patterns for the AC sample are similar to the (002), (100) and (101) planes which attributed to the graphite peaks (Rajendran et al., 2015).

The SEM micrographs of the produced AC surface illustrated the rough surface and cavities on the AC samples as depicted in Fig. 1e. These cavities on the sample surface significantly increase the surface available for dyes and metal ions uptake. A semi-quantitative study of the

AC can be obtained using the EDS analysis. Fig. 1f displays the results of the EDS investigation
for the AC samples. The AC sample indicates the carbon, oxygen and nitrogen content (%
atomic) as 70.57, 24.17 and 5.26, respectively.

4

5 3.2. Impact of pH

6 The solution pH is known as one of the significant factor in the adsorption process because of its influences the surface charge of both adsorbent and dye molecules (Errais et al., 2011; 7 Kumar et al., 2010; Rafatullah et al., 2010). Influence of initial pH of solution on the SY dye 8 uptake with concentration of 15 mg/L, adsorbent dose of 0.2 g, particle size of 150-250 µm, 9 stirrer speeds of 600 rpm and contact times of 35 min is well studied and the results obtained is 10 shown is Fig. 2a. reveals the uptake behavior of SY dye on adsorbent at pH values ranging from 11 1 to 10. As the figure shows, by growing the pH from 1 to 10 the dye removal significantly 12 declines to 21.97% from 83.33%. These findings indicate that our results are in agreement with 13 previous investigations (Celekli et al., 2012; Celekli et al., 2012; Gupta et al., 2010a). It is 14 needed to specify the zero point charge (pH_{zpc}) of adsorbent is one of the main factor to 15 recognize the mechanism of sorption. Fig. 2b shows that the pH_{zpc} of the adsorbent is found to be 16 about 3.0. The adsorbent surface could become positively charged at $pH < pH_{zpc}$, thereby a high 17 electrostatic attraction occurs between positive charges of adsorbent and negative charges of 18 anionic dyes such as SY dye. At higher pH values than pH_{zpc}, the surface of the adsorbent could 19 be negatively charged, which decrease in the percentage removal of anionic dye because of 20 electrostatic repulsion. The maximum percentage dye removal was obtained at pH 1. Hence, this 21 pH value is the optimal value for the rapid adsorption of noxious SY dye. 22

23 **3.3. Impact of particle size**

1 For investigating the effect of particle size on the adsorption of SY dyes, three particle sizes (150-250, 250-425, and 425-850 µm) of AC in a beaker containing 50 mL of the adsorption 2 solution with 10-40 mg/L, 5-35 min, 0.05-0.25 g and 600 rpm was used. The results obtained is 3 shown in Fig. 3, which demonstrates the influence of particle size on adsorption of SY dye with 4 concentration of 10 mg/L and contact time of 35 min. The results of the effect of particle size at 5 6 different contact time is included in the supporting information (Fig. S1). From Fig 3 and Fig S1 it was observed that as the particle size increases from 150-250 to 425-850 µm with dye 7 concentration of 10 mg/L, adsorbent dosage of 0.25 g and contact time of 35 min, the removal 8 percentage decreases from 88.30 to 65.07 %. This is because of increased surface area and large 9 number of available active sites for molecules of noxious SY dye. Similar results have been 10 obtained in previous studies (Celekli et al., 2012; Gupta et al., 2010a; Mui et al., 2010). 11

12 **3.4. Effect of contact time**

Various experiments at five contact times (5, 10, 20, 30 and 35 min) under different operating variables (particle size of 150–850 μ m, adsorbent dosage of 0.05-0.25 g, pH 1, 600 rpm and dye concentration of 10-40 mg/L were performed to assess impacts of contact time on the SY dye adsorption on AC (Figs. 4 and S2). From the results obtained, it is observed that the values of SY dye removal increases with contact time up to 10 mins and then remains constant with further increase in contact time. The fast sorption may be attributed to the abundance of functional groups on the surface of the absorbent during beginning contact time steps.

20 **3.5. Impact of dye concentration**

To estimate impact of dye concentration on the removal percentage of dye, experiments
were performed at diverse quantity of adsorbents (0.05-0.25 g) and four dye concentrations (1040 mg/L) for three particle sizes (150–250, 250–425, and 425-850 μm). Figs. 5 and S3

1 demonstrate the variation in removal percentage values versus dye concentration for SY. Results specified that the removal of SY dye significantly decreased with dye concentration. This could 2 be the result of decline in the surface area of available unoccupied sites by enhancing in 3 concentration of dye. Results also showed that value of adsorption capacity improved by 4 5 elevating concentration of dye. The increment in the driving force for mass transfer by 6 improving in concentration of dye could be the reason for this phenomenon. These results are in 7 agreement with the results of previous adsorption investigations (Dehghanian et al., 2015; Ghaedi et al., 2014). 8

9 **3.6. Impact of adsorbent dosage**

To calculate the impact of the adsorbent amount on the uptake of SY dye, five adsorbent 10 dosage (0.05-0.25 g) were used with three particle sizes (150-850 µm) at the dye solution with 11 12 four SY dye concentrations (10-40 mg/L). The result of the amount of adsorbent on the removal percentage of SY dye is displayed in Figs. 5 and S4. As seen from this figure, an enhancement in 13 the dosage of adsorbent from 0.05 to 0.25 g improved the removal percentage values because of 14 enhancement in active site and surface area. The same result was also obtained for the adsorption 15 of methyl orange dye on tin oxide nanoparticles loaded on AC achieved from Pistacia atlantica 16 wood (Ghaedi et al., 2016). 17

18 **3.7. Adsorption kinetics**

For considering the kinetic of SY dye uptake on produced adsorbent Lagergren's pseudofirst-order, the pseudo-second-order, Elovich and intraparticle diffusion were employed. The equation of Lagergren's pseudo-first-order is denoted as (Azizian, 2004; Lagergren, 1898),

22
$$\ln(q_e - q_t) = \ln q_e - k_1 t$$
 (14)

where q_e , q_t and k_1 are the capacity of dye uptake at equilibrium (mg/g), the capacity of dye uptake at time t (mg/g), the rate constant of the first-order reaction (l/min). The pseudo-secondorder can be indicated in the linear form (Ho, 2006; Ho and McKay, 1998).

4
$$t/q_t = 1/(k_2 q_e^2) + (1/q_e).t$$
 (15)

5 where k_2 represents rate constant of the second-order reaction (g/mg min). The Elovich model 6 can be expressed by the following relation (Ho and McKay, 2002; Rudziñski and Everett, 1992).

7
$$q_t = \frac{1}{\beta} \ln(\alpha\beta) + \frac{1}{\beta} \ln t$$
(16)

8 where β is the desorption coefficient (mg g⁻¹ min⁻¹) and α is the initial adsorption rate (g mg⁻¹
9 min⁻²). Finally, the simplified intra-particle diffusion model to achieve the diffusion rate
10 coefficient may be written as below (Weber and Morris, 1963).

11
$$q_t = k_i \cdot t^{0.5} + C$$
 (17)

where k_i represents the rate coefficient (mg g⁻¹ min^{-0.5}). The slope and intercept of the linear 12 plot of q_t vs. $t^{0.5}$ can be used to find k_i and C (mg g⁻¹), respectively. The values obtained for the 13 parameters of kinetic models in order to the removal of SY dye on AC at room temperature, pH 14 1, 600 rpm, 40 mg/L, 150-250 µm and different adsorbent dosage have been shown in Table S2. 15 Based on the high values of R^2 (in the range of 0.9959-0.9984) can be deduced that the pseudo-16 second-order kinetic is appropriate for demonstrating the SY dye uptake on AC. Three steps 17 including pore diffusion, film diffusion and intra-particle transport determine the mechanism of 18 19 the absorption process. The process overall rate is controlled using the slowest of the three steps. To find the mechanisms of SY dye uptake on AC, the intra-particle diffusion model (Eq. 17) was 20 21 used which in this equation C value indicates the boundary layer thickness. Thus, it can be 22 deduced that the pore diffusion is not the only rate-limiting step whereas the rate-controlling step is probably chemical interactions (Ahmad, 2009). 23

1 **3.8.** Adsorption isotherms

The equilibrium adsorption of the SY dye was performed with different adsorbent amount (0.05-0.25 g) with particle size of 150- 250 µm in 50 ml solution of dye with diverse concentrations from 10 - 40 mg/L for 35 minutes at pH 1. Four types of several isotherm models namely Freundlich, Langmuir, Dubinin-Raduskevich (D-R) and Temkin were used to fit the actual data. The isotherm parameters achieved by linear fitting were indicated in Table S3.

The Langmuir isotherm describes the formation of the uniform monolayer adsorption on the
adsorbent surface (Langmuir, 1916). The linear form of Langmuir equation can be indicated as
follow:

$$10 \qquad \frac{C_e}{q_e} = \frac{1}{q_m K_L} + \frac{C_e}{q_m} \tag{18}$$

where C_e shows concentration of adsorbate at equilibrium (mg/L), q_e is capacity of adsorption at equilibrium (mg/g), q_m displays maximum capacity of monolayer coverage (mg/g) and K_L is constant of Langmuir isotherm (L/mg). Equilibrium parameter or separation factor (R_L) as main characteristics of the Langmuir model can be expressed as follows:

15
$$R_L = \frac{1}{1 + K_L C_0}$$
 (19)

The value of R_L displays whether the nature of adsorption is favorable or unfavorable; linear if $R_L=1$, favorable if $0 < R_L < 1$, unfavorable if $R_L>1$ and irreversible if $R_L=0$. As seen from Table 1, the R_L values were between 0 and 1 representing that Langmuir isotherm is favorable. From the result obtained, the q_m from Langmuir Isotherm model was found to be 5.8377- 30.1205 mg/g, K_L values are between 0.1453 and 0.4287 L/mg. The R^2 values were obtained to be 0.9862-0.9954, demonstrating that the adsorption of SY dye on AC fitted well to the Langmuir Isotherm.

Freundlich isotherm has been applied for describing the adsorption onto heterogonous
 surfaces (Freundlich, 1906). Linearizing equation of the Freundlich isotherm can be indicated as
 follows:

(20)

$$4 \quad \log q_e = \log K_F + \frac{1}{n} \log C_e$$

Where, K_F shows the capacity of adsorption (L/mg). 1/n represents intensity of adsorption and 5 the distribution of the surface heterogeneity and the energy of the active sites; the partition of 6 7 adsorbents between the two phases is independent of the concentration if n=1, normal adsorption if $\frac{1}{n} < 1$ and cooperative adsorption $\frac{1}{n} > 1$. The R² values of 0.8843-0.9353 indicated that 8 Freundlich model was inadequate to explain the association of qe with equilibrium 9 concentrations. The values of K_F were found as 1.9315- 4.9615. The value of 1/n = 0.3884-10 0.5379 showing that the uptake of SY dye onto AC is favorable, while this model is inadequate 11 to designate the relationship between the Ce and q_e because of the low R^2 values. 12

D-R model is usually used for discovering the adsorption mechanism based on the
Gaussian energy distribution onto a heterogeneous surface (Dubinin and Radushkevich, 1947).
The linear form of this model is as follows.

16
$$\ln q_e = \ln q_m - \beta \varepsilon^2$$
 (21)

17
$$\varepsilon = RT \ln(1 + \frac{1}{c_e})$$
 (22)

$$18 E = \frac{1}{\sqrt{-2\beta}} (23)$$

19 where q_m (mg/g), q_e (mg/g), β (mol²/J²), E (J/mol) and ε are maximum uptake capacity, 20 equilibrium adsorption capacity, activity coefficient, mean free energy of adsorption and Polanyi 21 potential. The E-value shows the nature of adsorption to be either chemical if 8<E<16 KJ/mol 22 and physical if E<8 KJ/mol. By the linear regression analysis of D-R isotherm, the values of q_m

1	were measured to 4.7684-20.5426 mg/g. The value of E parameter (0.707-1.118 KJ/mol)
2	indicating that SY dye uptake onto AC could be performed through the physical mechanism. The
3	R^2 values of D-R model were less than of Langmuir, nevertheless based on the relatively high
4	value of R^2 (0.9777-0.9869), it was deduced that the D-R model was also suitable to illustrate the
5	association of q _e with C _e .

The Temkin model supposes that the adsorption heat would reduce linearly and a uniform
distribution of binding energies was used to characterize the adsorption (Temkin and Pyzhev,
1940). The following relation can show this model.

9
$$q_e = B \ln K_T + B \ln C_e \tag{24}$$

$$10 \quad B = \frac{RT}{h} \tag{25}$$

where K_T (L/g) and *b* (J/mol) are Temkin isotherm constant. From linear regression of Temkin isotherm equation revealed in Table 1, the following values were obtained: $K_T = 1.1935-4.5108$ L/g, B=1.2348-7.2020 J/mol and R²=0.9537-0.9842.

14 **3.9. GMGH model**

In this work, the GMDH model was utilized to forecast of removal percentage of SY using 15 AC from aqueous system. Table S1 exhibits the experimental data. The actual data consist 300 16 points while 70% of these data were utilized for training and 30% for testing. The in depended 17 factors for example particle size, initial concentration of dye, adsorbent dosage and contact time 18 have been designated as the inputs and the dye removal (%) has considered as the output of the 19 network. The values of these parameters with related values of R² and MSE were reported in 20 Table 1. To acquire the optimal construction of GMDH neural network model different 21 parameters of GMDH model for instance maximum number of layers, maximum neurons 22 number in a layer, selection pressure and train ratio were investigated. The maximum R² value 23

and the minimum MSE value for the testing data points were used for selection the optimal construction of the GMDH model. It can be detected that the GMDH model with 100 maximum layer numbers, 6 maximum neuron numbers in a layer, 0.1 selection pressure and 0.7 train ratio has good performance for predicting the removal percentage of SY dye onto AC. For testing points the values of R^2 and MSE were found to be 0.9702 and 3.4078 using the optimal GMDH model, respectively. In addition, the actual and anticipated data were compared in Fig. 6. As shown, the results of the MGDH model are in good agreement with the actual data.

8

9 **3.10. MLR model**

10 The common objective of MLR is to learn more about the association among several 11 independent parameters and a dependent parameter. The MLR equation can be written as follow 12 form.

13
$$y = a + b_1 x_1 + b_2 x_2 + \dots + b_n x_n$$
 (26)

where b₁, b₂ and b_n are the coefficients of regression and a is a constant. The same data used in
the training and testing of GMDH model was used to construct and evaluate the MLR model.
The MLR equation to forecast removal percent is shown below.

17
$$Removal \% = 45.347 + 0.222X_1 - 0.612X_2 + 0.348X_3 + 55.542X_4$$
 (27)

where X_1 , X_2 , X_3 and X_4 are particle size (mesh), initial concentration (mg/L), and adsorbent dosage (g). Fig. 6 illustrates the relations between actual and forecasted values achieved from the MLR model. According to this figure, the MLR results are not very close to the actual results and the R² and MSE values were found to be 0.780 and 26.839 for testing data sets, respectively.

22 3.11. Comparison GMDH and MLR models

To compare reliable prediction of GMDH and MLR models for forecasting of removal 1 percent, the MSE, R^2 and the deviations from the actual values were calculated. Fig. 6 shows the 2 distances of the anticipated values using the models built from the experimental values. The 3 figure designated that the deviation distance (-5.0573 to +4.7495) of the forecasted values using 4 MGDH model is lower than the deviation distance of the MLR model (-10.822 to +11.739). 5 Table 4S indicates the values of R^2 and MSE for training and testing data points from both 6 GMDH and MLR models. The values of R^2 and MSE of GMDH model for training and testing 7 subsets were found to be 0.9785, 0.9702 and 2.8362, 3.4078, respectively. The R² and MSE 8 values of MLR model were 0.8434, 0.780 and 20.617, 26.839, respectively. Based on the MSE, 9 R^2 and the deviation interval values, it can be concluded that the GMDH model for predicting of 10 removal percent revealed the more reliable anticipations than the MLR model. 11

12 **4.** Conclusions

Biomaterial of Oak Tree is used for the preparation of AC and the prepared inexpensive 13 adsorbent is characterized using SEM, XRD and FTIR. The prepared adsorbent is 26% 14 crystalline in nature and 74 % amorphous in nature. Effective parameters were investigated and 15 optimized and it was observed that for maximum adsorption, the initial concentration of 10 16 mg/L; adsorbent dose of 0.25 g; pH =1; contact time= 35 min and particle size=150-250 µm is 17 found to be optimized. Comparison of the MLR and GMDH models showed the good 18 predictability of GMDH model for forecasting removal percent of SY dye. The optimal 19 parameters for GMDH model were found to be 100 maximum number of layers, 6 maximum 20 number of neurons in a layer, 0.1-selection pressure and 0.7 train ratio. For training points, the 21 values of R² of 0.9785 and MSE of 2.8362 were obtained using the optimal GMDH model. The 22 results presented that the soft computing model is a good tool for predicting adsorption process. 23

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6	Figure captions:
7	Fig. 1. (a) molecular structures of the sunset yellow dye, (b) a schematic diagram of the used
8	GMDH model, (c) FT-IR spectrum, (d) XRD pattern, (e) SEM image and (f) EDX analysis of
9	the produced AC
10	Fig. 2. (a) Impact of pH solution on the removal of SY dye and (b) adsorbent surface charge as a
11	function of pH
12	Fig. 3. Influence of particle size on the uptake of SY dye onto AC; 10-40 mg/L, 35 min, 0.05-
13	0.25 g, 600 rpm, pH 1 at room temperature
14	Fig. 4. Influence of contact time on the uptake of SY dye onto AC; 10-40 mg/L, 150 –250 μ m,
15	0.05-0.25 g, 600 rpm, pH 1 at room temperature
16	Fig. 5. Influence of initial concentration and adsorbent dosage on the uptake of SY dye onto AC;
17	35 min, 150 –850 μm, 0.05-0.25 g, 600 rpm, pH 1 at room temperature
18	Fig. 6. Anticipated removal percentage plotted versus experimental data and the variation of the
19	values forecasted by MGDH and MLR models from the actual values
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	Table 1	
	Parameters of MGDH model and results of MSE and R^2	

Doromotors	ofMCDU	modal	and rocu	lta of	MCE	and \mathbf{P}^2	
Parameters		model	and resu	Its of	MOL	anu r	

Maximum Number	Maximum	Selection	Train	Train data		Test data	
of Neurons in a	Number	Pressure	Ratio	R^2	MSE	R^2	MSE
Layer	of Layers						
100	1	0.3	0.5	0.7603	31.5594	0.6655	38.1966
100	2	0.3	0.5	0.8312	22.2242	0.7771	25.4549
100	3	0.3	0.5	0.9639	4.7563	0.9537	5.2898
100	4	0.3	0.5	0.9653	4.5695	0.9557	5.0537
100	5	0.3	0.5	0.9696	4.0005	0.9602	4.5400
100	6	0.3	0.5	0.9752	3.2664	0.9663	3.8459
100	7	0.3	0.5	0.9772	3.0033	0.9656	3.9267
100	8	0.3	0.5	0.9755	3.2261	0.9519	5.4894
100	6	1.0	0.5	0.7565	32.0612	0.6658	38.1645
100	6	0.8	0.5	0.7595	31.6614	0.6826	36.2470
100	6	0.5	0.5	0.8329	22.0016	0.7791	25.2275
100	6	0.1	0.5	0.9748	3.3112	0.9670	3.7715
100	6	0.1	0.1	0.8806	15.7237	0.8601	15.9821
100	6	0.1	0.3	0.9597	5.3009	0.9518	5.4990
100	6	0.1	0.7	0.9785	2.8362	0.9702	3.4078
100	6	0.1	0.9	0.9762	3.1394	0.9653	3.9658
50	6	0.1	0.7	0.9715	3.7501	0.9589	4.6961
150	6	0.1	0.7	0.9770	3.0267	0.9627	4.2554









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Highlights

- 1. AC from oak tree wood demonstrates efficient removal of Sunset Yellow dye from water.
- 2. Batch studies reveal optimum performance at pH 1 and contact time of 35 mins
- 3. Modeling reveals a better fit of experimental data with the Langmuir and pseudo-second order model
- 4. GMDH model shows better performance in forecasting removal of the dye.
- 5. Results reveal that soft computing model is a good tool for predicting adsorption performance