Effect of particle size on the viscosity of nanofluids: A review

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ABSTRACT

Nanofluids are potential new generation heat transfer fluids, which have been investigated meticulously, in recent years. Thermophysical properties of these fluids have significant influence on their heat transfer characteristics. Viscosity is one of the most important thermophysical properties that depends on various parameters. Size of the particles used in nanofluids is one of these effecting parameters. In this work, experimental studies considering the particle size effect on the viscosity of the nanofluid have been reviewed. Firstly, comparison of nanofluid and surfactant type, production and measurement methods were considered. Viscosity results of selected studies were evaluated in view of the parameters such as particle size, temperature and concentration. Furthermore, effective viscosity models of nanofluids, which include particle size as a parameter were discussed. The results indicate that there is a discrepancy about the effect of particle size on the viscosity of nanofluids. Moreover, it is observed from the evaluated data that the relative viscosity variation can be almost 40% either upwards or downwards by only altering the particle size.

1. Introduction

Technology driven world enforces the researchers to explore more and more in thermal engineering. Currently, one of the most crucial pursuits of thermal engineers is to provide efforts on new types of heat transfer fluids. Thermal engineers found that the addition of solid particles to a base fluid can provide the fluid a better heat transfer capability. Based on this concept, a new generation fluid named as "nanofluid" has occurred in the field for the last two decades. Typically, water, ethylene glycol, oil, etc. are employed as base fluids, which have naturally poor thermal conductivities. Supplementation of nano-scaled metals, metal oxides or carbon based materials to these base fluids brings out the nanofluids. Although the idea was first conceived by Masuda et al. [1], Choi [2] was the one who had named it as nanofluid. Just after their inventions, a number of nanofluid related papers have increased expeditiously [3] as can be seen in Fig. 1.

Recent literature reveals that nanofluid based systems have an extensive potential area such as, solar collectors [4,5], electronics cooling [6–8], automotive [9,10], nuclear reactor cooling [11], refrigerators [12–14], heat exchangers [15,16]. The potential utilization of such a colloidal mixture for many divergent systems exposed the requisiteness of meticulous investigation on thermal properties of the nanofluids. One of the pioneering studies on the thermal conductivity by Lee et al. [17] concluded that the presence of nanoparticles provides substantially higher thermal conductivity than the same liquid without particle addition. Eastman et al. [18] prepared a nanofluid by adding copper nanoparticles into the ethylene glycol and they observed a thermal conductivity increment up to 40%. Xie et al. [19] studied the thermal conductivity of Al_2O_3–ethylene glycol nanofluid. The conclusion, which is in accordance with the former one, included that the thermal conductivity of the suspension was much higher than the base fluid. Although the goal of adding nano sized particles to a base fluid is

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Nomenclature

T	temperature (°C)
d	diameter (m)
H	inter particle space (m)
C	correction factor
V	velocity (m/s)
m	constant of system properties
h	hydrodynamic
r	thickness of the capping layer (m)
N	Avogadro's number (6.022×10^{23} mol^{-1})
M	molecular weight (kg/mol)

Subscripts

nf	nanofluid

bf	base fluid
p	particle
o	reference
f	fluid

Greek letters

μ	viscosity (Pa s)
φ	volume concentration (%)
ρ	density (kg/m^3)
δ	distance between the centers of particles (m)
α, ω, γ	empirical constants
λ, σ	exponents

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to achieve higher thermal conductivity values, the thermal conductivity is not the sole property that influences the heat transfer. It is also viscosity that is playing a key role on characterizing the heat transfer behavior of a nanofluid [20]. Li et al. [21] was one of the first groups who investigated the transport properties of nanofluids and observed that the viscosity was not only affected by the volume concentration, but also the size of nanoparticles.

Ascending of nanofluid researches on convective heat transfer brought out many viscosity based studies. Pozhar [22] made theoretical and simulation efforts to predict the nanofluids' viscosity at the very beginning. Then, Wang et al. [23] proposed a modified viscosity equation from Einstein's classical viscosity model for suspensions by considering spatial distribution of nanoparticle clusters and adsorption liquid molecules on nanofluid surfaces. Many experimental studies followed them and it is exposed that viscosity of nanofluids is fairly dependent on several parameters such as temperature, volume concentration, aggregation, particle shape, surfactant, particle size, etc. [24,25]. It is also influenced by the ultrasonication period used during nanofluid preparation [26]. Turgut et al. [27] made an experimental effort on measuring the viscosity of TiO_2−water nanofluid. They observed a decrement in viscosity values by increasing temperature. Sundar et al. [28] prepared a review paper on viscosity, which affirms the results of Turgut et al. [27] in terms of temperature. Bahiraei et al. [29] and Sundar et al. [28] conducted experiments to interpret the effect of vol. concentration on viscosity by using Fe_3O_4−water (0.1−1%) and TiO_2−water (0−2%) nanofluids, respectively. They both concluded

that the viscosity was increased by the increase of vol. concentration. Aggregation also plays an important role on the viscosity of nanofluids [30]. Gaganpreet et al. [31] focused on fractal aggregates and interfacial layer around the nanoparticle to determine the rheological behavior of nanofluids. It was found that the increase in effective radius of the aggregates lead to a substantial viscosity increment. In addition to the aggregation, viscosity of nanofluids depends on the particle shape [32]. Timofeeva et al. [32] recommended the use of nanoparticles with spherical shape for lower viscosity values. In accordance with the recommendation of Timofeeva et al. [32], the study of Jeong et al. [33] concluded that the viscosity for the nanofluid with nearly rectangular shape particles were 7.7% higher than that of the one with spherical shape. Stability is an essential point to be ensured for a colloidal mixture. Use of a surfactant can be an effective way to achieve a stable behavior for nanofluids [34]. Li et al. [35] used sodium dodecylbenzenesulfonate (SDBS) as a surfactant for Cu−water suspension. They found out that viscosity of the Cu−water nanofluid increased slightly by increasing the mass concentration of SDBS dispersant. Moreover, a more recent study [36] has employed two types of surfactants to improve the stability of TiO_2, polycarboxylate and trioxadecane acid. They found out that TiO_2 with polycarboxylate surfactant has a higher viscosity than the one with trioxadecane acid. Thus they concluded that the increment of viscosity may be dependent on the surfactant type. The influence of the size of dispersed nanoparticles on viscosity is another critical parameter. Many review studies related with particle size are available in the literature. Sergis et al. [37]
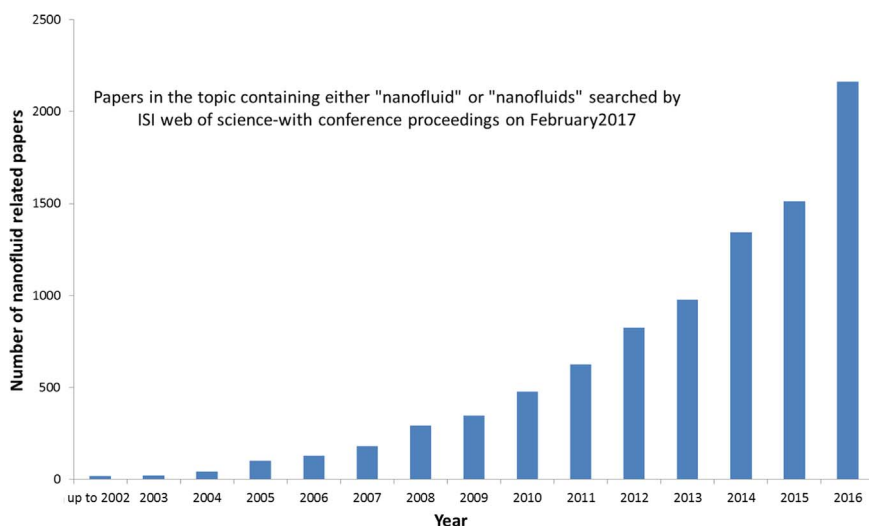

Fig. 1. Number of publications containing the term nanofluid in literature.

reviewed the anomalous heat transfer modes of nanofluids. They mentioned that the trend seemed to be as effective viscosity increasing while particle size decreasing. Kumar et al. [38] and Mishra et al. [39] reported that there is no report on critical particle size to achieve stability and less agglomeration. Elcioglu et al. [40] emphasized the particle agglomeration possibility. According to their findings, particle agglomeration should be considered while evaluating the particle size effect. Nwosu et al. [41] reviewed the viscosity models available in literature and they concluded that particle and aggregation sizes should be taken into account while proposing new viscosity models in further studies. Sharma et al. [42] suggested that, particle size and particle shape optimization can be carried out for each type of nanofluid which may be helpful in synthesizing a new class of nanofluids with better rheological properties. Bashirnezhad et al. [43] concluded that considering the effect of particle size, aggregation, sonication time, pH at the same time with particle concentration leads to generate more accurate viscosity correlations. In a more recent study, Zhao et al. [44] presented and discussed the data driven modeling of thermalphysical properties of nanofluids for automotive radiator by considering the particle size. According to observations of Akilu et al. [45] it is apparent that contradictions exist in particle size effect studies. They mentioned that such discrepancies can mostly be caused from experimental procedures and instrument calibration. Another review on nanofluid viscosity by Sundar et al. [28], reported a contradiction that three types of conclusions are available in literature in terms of the size effect; increase in relative viscosity by decreasing particle size or by increasing particle size and no significant effect of particle size.

In perusing the nanofluid related literature, there are still discrepancies between papers about the particle size effect on viscosity. This study aims to review and discuss the systematic experimental studies which have investigated the particle size effect on nanofluid viscosity. In other words, data from studies which have made viscosity measurements with same nanofluid sample for different particle sizes are

collected, analyzed and discussed. Although, there are several reviews [25,28,30,38–47] which include the particle size effect as part of an overall nanofluid viscosity review, no review available completely focused on the effect of particle size on the viscosity of nanofluids. Some of these reviews [30,38–40,46,47] only referred to the results of studies, cited in text, and some of them recommended the development of more accurate correlations [25,28] or more quality work [42] in order to be able to comment the particle size effect on the viscosity. Another goal of this work is to discuss the reasons far beyond discrepancies between particle size effect related studies. Authors hope that it is the first time that the particle size effect on nanofluid viscosity is discussed based on samples utilized in the same studies unlike the other existing reviews. Moreover, it is the first time that the parameters which need to be considered are discussed for the investigation of the particle size effect.

2. Experimental studies about the effect of particle size on the viscosity

Many experimental and numerical investigations on the relative viscosity of nanofluids have been conducted. Table 1 indicates the available experimental studies [36,48–67] on the relative viscosity of nanofluids by considering the particle size effect. The table includes specifications of these studies such as; base fluid, nanoparticle type, particle size, particle shape, particle vol. concentration and temperature. It is clearly seen that the most popular base fluid is water and the most commonly used nanoparticle is Al_2O_3. The reason is probably due to the low cost and the high thermal conductivity of Al_2O_3 nanoparticles compared to the other nanoparticles [68].

To perform a more detailed analysis for the available literature, Table 2 is provided. The table involves information of the surfactant type, production and measurement method and the suppliers of experimented samples. Generally, rotational type of viscometer has

Table 1
Summary of process parameters of some experimental investigations on viscosity.

Article	Particle	Base fluid	Particle vol. concentration (%)	Particle size (nm)	Particle shape	Maximum relative viscosity (μ_{nf}/μ_{bf})	Temperature (°C)
Prasher et al. [63]	Al_2O_3	PG(propylene-glycol)	0.5–3	27, 40 and 50	No information	1.3762 (30 °C, 40 nm)	30–60
He et al. [48]	TiO_2	Water	0.6	95, 145 and 210	Spherical	1.0716 (210 nm)	22
Nguyen et al. [49]	Al_2O_3	Water	1–9	36 and 47	No information	3.05 (22 °C, 47 nm)	20–50
Chevalier et al. [53]	SiO_2	Ethanol	1.1–7	35, 94 and 190	Spherical	1.99 (35 nm)	Ambient
Namburu et al. [51]	SiO_2	EG(ethylene-glycol) -water (60:40)	8	20. 50 and 100	Spherical	1.625 (0 °C, 20 nm)	−35–50
Lu et al. [54]	Al_2O_3	Water	5	35, 45 and 90	No information	1.287 (35 nm)	20
Lu et al. [54]	Al_2O_3	EG	5	35, 45 and 90	No information	1.141 (35 nm)	20
Anoop et al. [64]	Al_2O_3	Water	0.51–2.1	45 and 150	Spherical	1.06 (150 nm)	30
Namburu et al. [52]	SiO_2	EG-water (60:40)	6	20, 50 and 100	Spherical	2.232 (50 °C, 20 nm)	−35 to 50
Timofeeva et al. [56]	SiC	Water	4.1	16, 29, 66 and 90	Spherical	1.857 (25 °C, 16 nm)	15–45
Kwek et al. [55]	Al_2O_3	Water	5	12, 28, 32, 80 and 150	No information	1.882 (12 nm)	25
Shanker et al. [57]	Al_2O_3	Glycerol-water (70:30)	< 1	27 and 45	No information	1.29 (80 °C, 27 nm)	30–80
Meriläinen et al. [65]	Al_2O	Water	0.5–4	8.2 and 14–53	Spherical	1.65 (8.2 nm)	10–50
Meriläinen et al. [65]	MgO	Water	0.5–2	21 and 15–47	Rod	1.91 (15–47 nm)	10–50
Meriläinen et al. [65]	SiO_2	Water	0.5–4	6.5, 65 and 28–110	Various types	1.49 (28–110 nm)	10–50
Oliveria et al. [66]	Ag	Water	0.1–0.3	10 and 80	Spherical	1.0458 (10 nm)	Ambient
Esfe et al. [58]	Fe	EG	0.125–3	40, 70 and 100	Spherical	1.385 (45 °C, 40 nm)	26–55
Jarahnejad et al. [36]	Al_2O_3	Water	2.4	200, 250 and 300	Inhomogeneous	1.86 (20 °C, 250 nm)	20–50
Agarwal et al. [60]	Al_2O_3	Kerosene	0.05–0.5	13 and 50	No information	1.134 (65 °C, 13 nm)	25–65
Esfe et al. [59]	Fe	Water	0.03–1	37, 71 and 98	Spherical	1.073 (37 nm)	Ambient
Turgut et al. [50]	Al_2O_3	Water	1–3	10 and 30	Spherical	2.07 (50 °C, 30 nm)	5–50
Minakov et al. [62]	SiO_2	Water	2	10, 16, 25 and 100	No information	1.43 (10 nm)	25
Rudyak et al. [61]	SiO_2	EG	0.67–6.7	18.1, 28.3 and 45.6	No information	1.76 (25 nm)	25

Table 2
Summary of the background information of some experimental investigations on viscosity.

Article	Particle	Base fluid	Surfactant	Production method	Company	Measurement device
Prasher et al. [63]	Al$_2$O$_3$	PG	No information	Pulsed plasma process and ultrasonication	Nanotechnologies Inc.	A controlled stress rheometer
He et al. [48]	TiO$_2$	Water	No information	Ultrasonication – 30 min	Degussa (Germany)	Bohlin CVO rheometer with a Mooney cell
Nguyen et al. [49]	Al$_2$O$_3$	Water	Unknown surfactant	A vigorous stirring action	Nanophase Technologies	ViscoLab450 Viscometer
Chevalier et al. [53]	SiO$_2$	Ethanol	No information	Stirring – 2 h	Nano-H S.A.S.	Micromachined capillary viscometers
Namburu et al. [51]	SiO$_2$	EG-water 60:40	No information	–	Nanophase, Inc.	LV DV-II+ Brookfield Viscometer
Lu et al. [54]	Al$_2$O$_3$	Water	No information	Ultrasonication	Nanomaterial Company (Luming, Dalian)	Capillary viscometer
Lu et al. [54]	Al$_2$O$_3$	EG	No information			
Anoop et al. [64]	Al$_2$O$_3$	Water	No information	Laser evaporated physical methods and ultrasonication	Nanophase Technologies	Ubelohde viscometer
Namburu et al. [52]	SiO$_2$	EG-water 60:40	No information	No information	No information	LV DV-II+ Brookfield Viscometer
Timofeeva et al. [56]	SiC	Water	Unknown surfactant	Milling larger pieces of SiC material	Saint Gobain, Northboro, MA	DV-II+ Brookfield Viscometer
Kwek et al. [55]	Al$_2$O$_3$	Water	Cetyltrimethylammonium Bromide (CTAB)	Stirred by a magnetic stirrer before ultrasonification process	Nanostructured and Amorphous Materials	Standard controlled rate rheometer (Contraves LS 40)
Shanker et al. [57]	Al$_2$O$_3$	Glycerol-water 70:30	Sodium Dodecyl Benzene Sulfonate (SDBS)	Stirring 16 h	Sigma-Aldrich Chemicals Ltd, Germany	Programmable R/S+ cylindrical rheometer
Meriläinen et al. [65]	Al$_2$O$_3$	Water	No surfactant		Nanostructured Materials	
Meriläinen et al. [65]	MgO	Water	No surfactant	Ultrasonication – 16 h	Us Nanoresearch Nanomaterials	HAAKE (falling ball) viscometer
Meriläinen et al. [65]	SiO$_2$	Water	No surfactant		Nanostructured Materials	
Oliveria et al. [66]	Ag	Water	No information	High-pressure homogenizer	Nanostructured & Amorphous Materials	Brookfield Viscometer
Esfe et al. [58]	Fe	EG	No information	Ultrasonication 5 h	No information	Brookfield Viscometer
Jarahnejad et al. [36]	Al$_2$O$_3$	Water	Unknown surfactant	Ultrasonication	Unknown	Höppler (falling ball) viscometer
Agarwal et al. [60]	Al$_2$O$_3$	Kerosene	Oleic Acid	Ultrasonication – 30 min for each 0.05% concentration	No information	LVDV-II Brookfield Viscometer
Esfe et al. [59]	Fe	Water	Unknown surfactant	Ultrasonication – 2 h	No information	No information
Turgut et al. [50]	Al$_2$O$_3$	Water	Acetic Acid 0.1–0.3% by wt.	Ultrasonication – 2 min at 70 W	NanoAmor (USA)	Brookfield DV3T rheometer
Mikanov et al. [62]	SiO$_2$	Water	No surfactant	Ultrasonication – 30 min	JSC "Plazmoterm", Moscow	Brookfield DV2T rheometer
Rudyak et al. [61]	SiO$_2$	EG	No information	Ultrasonication	No information	LV DV-II+ Brookfield Viscometer

been used to measure the viscosity of nanofluids and all samples given in the table were produced by the two step method. Additionally, most of the cases involve an ultrasonication process to obtain uniform and stable suspensions.

The relative viscosity of nanofluids as a function of the particle size is shown in Fig. 2. Viscosity values of nanofluids are normalized by the values of base fluids to provide a better comparison. Evaluation of the considered papers in this review exposed that some of them [36,48–50] indicated an increment in the relative viscosity of nanofluids with increasing particle size. He et al. [48] carried out viscosity measurements on TiO₂–water nanofluid with different concentrations (0.25, 0.6 and 1.2 vol%) and different particle sizes (95, 145 and 210 nm) at 22 °C. Bohlin CVO rheometer with a Mooney cell was used for the viscosity measurements. Ultrasonication was applied for 30 min to disperse the particles in water to break down the large agglomerates. They concluded that the relative viscosity of nanofluids increases with increasing particle size and particle concentration. Furthermore, the non-linearity of the dependence of the nanofluid relative viscosity on particle concentration is more considerable than the particle size. Nguyen et al. [49] measured the viscosity of Al₂O₃–water nanofluid in the temperature range of 20–50 °C. Particle vol. concentrations of the nanofluid ranging from 1% to 9% were tested. They applied an ultrasonication for 30 min to mix the nanofluid. Although utilization of a surfactant for the preparation of nanofluids was mentioned, the type of the surfactant was not specified. Viscosity measurement of Al₂O₃– water nanofluid was done by using a piston-type viscometer with two different sizes (36 and 47 nm). The results show that the viscosity of the sample with 47 nm particle size is clearly higher than the sample with 36 nm particle size. The relative viscosity values of these samples seem to be higher when compared to the results of other papers. Moreover, they developed viscosity correlations for water based Al₂O₃ nanofluid for both particle sizes:

$$\frac{\mu_{nf}}{\mu_{bf}} = 0.904e^{0.148\varphi} \,(47\ nm) \tag{1}$$

$$\frac{\mu_{nf}}{\mu_{bf}} = 1 + 0.025\varphi + 0.015\varphi^2 \,(36\ nm) \tag{2}$$

Jarahnejad et al. [36] used two viscometers (a capillary and a falling ball) for the measurements of Al₂O₃–water and TiO₂–water nanofluids in the temperature range of 20–50 °C and the particle concentration of 3–14.3 wt%. They dispersed the nanoparticles in water by high-energy tip sonication. Different surfactants purchased from different companies (octylsilane for Al₂O₃, trioxadecane acid for TiO₂ and polycarboxylate for TiO₂) were added to the base fluid in order to improve shelf-stability of nanofluids. Al₂O₃ based nanofluids have three different sizes of 200, 250 and 300 nm. However, the details of the additives for Al₂O₃ nanofluid was not revealed by the supplier due to their intellectual property rights. The results showed that the increase in viscosity of the sample with 200 nm is lower than the samples with 250 and 300 nm particle sizes at 2.4 vol% concentration, but a general trend cannot be inferred from the results. Furthermore, they made a comparison between both with and without surfactant and the result indicated that the surfactant most likely increases the viscosity. Also they reported that the increment in viscosity of nanofluids might be dependent on the surfactant type; for instance, TiO₂ nanofluids with polycarboxylate surfactant have higher viscosity than the TiO₂ nanofluids with trioxadecane acid. But, the compared nanofluids with different particle sizes (respectively 140 and 200 nm) and surfactants, and the concentration of surfactant is unknown. Therefore, it is not clear that the viscosity increment of nanofluids is completely dependent on the type of surfactant. Turgut et al. [50] studied the particle size effect on the viscosity of Al₂O₃–water nanofluid for two different sizes as 10 and 30 nm. About 6.33 vol% concentrated Al₂O₃–water nanofluids were diluted to three different concentrations, respectively
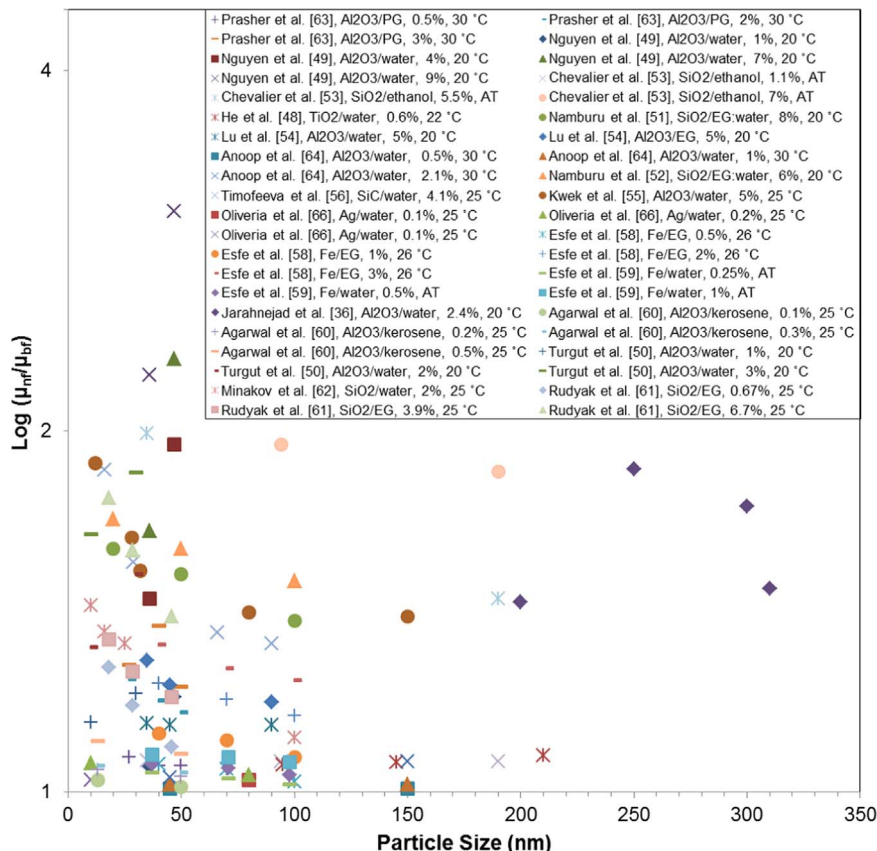

Fig. 2. Selected experimental data for the relationship between relative viscosity and particle size.

1%, 2% and 3%. The diluted nanofluids were sonicated by the probe type ultrasound for 2 min at 70 W power. The concentration of acetic acid as a surfactant with 0.1–0.3% by wt. was used in all samples. Viscosity measurements are done by a Brookfield DV3T Rheometer in the temperature range of 5–50 °C. At all temperatures, there is a linear relationship between the shear stress and the shear rate for all samples, which indicates Newtonian fluid behavior. Moreover, their results depicted that the relative viscosity of Al_2O_3–water nanofluid increases with the increase of the particle size. Furthermore, the viscosity of Al_2O_3 nanofluids with 10 and 30 nm were 1.6 and 1.8 times greater than the viscosity of water, respectively.

From another aspect, results of some studies [51–62] indicated an increment with decrease in particle size. Namburu et al. [51] studied SiO_2–EG/water (60% EG, 40% water by wt.) nanofluid with various diameters of 20, 50 and 100 nm. They measured the viscosity of nanofluids between −35 and 50 °C by a LV DV-II+ Brookfield Programmable Viscometer. They claimed that the nanoparticles were well dispersed and did not aggregate more than a year when they conducted the experiments. In terms of particle size effect evaluation, they only employed 8 vol% concentrated SiO_2–EG/water nanofluid and observed an increment in the relative viscosity values as particle size decreases. In a further study, Namburu et al. [52] confirmed this behavior by using the same nanofluid sample at 6 vol% concentration. Moreover, they presented a viscosity correlation for SiO_2–EG/water nanofluid as a function of temperature, which is valid for 50 nm particle size at 2–10 vol% concentration range.

$$Log\,(\mu_{nf}) = Ae^{-BT} \tag{3}$$

$$A = 0.1193(\varphi)^3 - 1.9289(\varphi)^2 - 2.245(\varphi) + 167.17 \tag{4}$$

$$B = -7 \times 10^{-6}\varphi^2 - 0.0004(\varphi) + 0.0192 \tag{5}$$

Chevalier et al. [53] studied the viscosity of SiO_2–ethanol nanofluid at vol. concentrations from 1.1% to 7% with three different particle sizes (35, 94 and 190 nm). The preparation of the samples was made by stirring them for 2 h. They used a capillary viscometer at ambient temperature for the measurements of the viscosity of the nanofluids. Their results showed that the relative viscosity of nanofluids is largely dependent on the particle size and increases when the particle size is smaller. Also, they compared their results with Krieger-Dougherty equation [69] and reported a good agreement. Lu et al. [54] and Kwek et al. [55] investigated the effect of the particle size on Al_2O_3–water nanofluid at 5 vol% concentration. Lu et al. [54] evaluated the viscosity of nanofluid both numerically and experimentally. Water and EG were employed as the base fluids for preparing the nanofluid samples. To avoid the agglomeration, sonication process was applied. They obtained a good agreement between the numerical results of simplified molecular dynamics (MD) simulation and the experimental data. They reported that the relative viscosity of nanofluids increases with the decrease in the particle size. However, the tendency is almost invariable when the diameter of nanoparticle is greater than 30 nm. Since some viscosity data are lower than that of the base fluid, they have not been shown in Fig. 2 for clarification of the illustration. Kwek et al. [55] added CTAB as a surfactant to the Al_2O_3–water nanofluids to keep the particles well-dispersed in the base fluid. Then, the nanofluids were stirred just before undergoing an ultrasonication process. The viscosity values were observed by the standard control rate rheometer (Contraves LS 40) at 25 °C. Their results indicated that the viscosity of nanofluids is much higher when the particle size is smaller. Eq. (3) proposed by Namburu et al. [52] does not consider the particle size effect. When comparing the values presented by these two studies, it is found that the relative viscosity of Kwek et al. [55] of 80 nm is 1.19 times higher than the value of Lu et al. [54] of 90 nm for the similar nanofluid samples and concentrations. This difference can be related to the surfactant and the producer. Timofeeva et al. [56] investigated the particle size effect on the viscosity of SiC–water nanofluids with

different particle sizes varying from 16 to 90 nm. The viscosity of the nanofluids was measured by using a Brookfield DV-II+ viscometer at a temperature range of 15–45 °C. They stated that the nanofluids with smaller particles provide higher viscosity because of the smaller solid/liquid interfacial area of larger particles. Shanker et al. [57] developed a generalized regression equation to include the particle size effect.

$$\mu_{nf} = \left(1.75 + 16.85\varphi + 23.5\frac{\varphi^2}{d_p^2}\right)\exp(0.015 + 0.15\varphi - 31.3\varphi^2 + 5.65\frac{\varphi}{d_p})T \tag{6}$$

Eq. (6) is valid for the range of $30 < T < 80$ °C, $27 < d_p < 45$ nm, $\varphi < 1\%$. Furthermore, Shanker et al. [57] experimentally investigated the particle size effect on the viscosity of Al_2O_3–Glycerol/water (70% Glycerol, 30% water) nanofluid at less than 1 vol% concentration. Their experimental data was not included in Fig. 2 due to the fact that the exact concentrations are not given by the authors. They prepared the samples by adding SDBS as the surfactant with 10% of the nanoparticle weight to the base fluid. Then, the mixture was stirred in a magnetic bath for 10 min. After the preparation of the mixture, the Al_2O_3 nanoparticles were added and stirred again continuously for 16 h. To measure the viscosity of the nanofluids, a programmable R/S+ cylindrical rheometer with a temperature controlled bath was utilized. They concluded that the nanofluid with 27 nm particle size has shown higher viscosity than the one with 45 nm. Esfe et al. [58] used Fe–EG nanofluids with three different particle sizes (40, 70 and 100 nm) and vol. concentrations between 0.125–3%. The Fe–EG suspension was stirred with an ultrasonic bath about 5 h to break down the agglomeration and provide a uniform suspension. A Brookfield viscometer was utilized for the viscosity measurement of nanofluids in the temperature range of 26–55 °C. They concluded that the viscosity of nanofluids increases with the decrease of the particle size. A year later, Esfe et al. [59] carried out an experimental study on Fe–water nanofluids with three different diameters of nanoparticles (37, 71 and 98 nm). They prepared the samples by dispersing the nanoparticles in water using an ultrasonic vibrator for 120 min. An activator was used to cover the nanoparticles to stabilize the suspension; however, the type of the activator was not mentioned in the study. They measured the viscosity ratio for Fe–water under the ambient conditions with six different vol. concentrations varying from 0.0313% to 1%. The measurement method of the viscosity was not mentioned. They concluded that the viscosity of the nanofluids depends on the size of the nanoparticles and increases with the decrease of the particle size. They used the experimental data to make curve fitting for the viscosity of the nanofluid and they proposed a simple equation to correlate viscosity as a function of d_p and φ:

$$\frac{\mu_{nf}}{\mu_{bf}} = 1 + (0.1008\varphi^{0.6974}d_p^{0.44708}) \tag{7}$$

Agarwal et al. [60] examined the effect of the particle size on the viscosity of Al_2O_3–kerosene nanofluid. The viscosity of the nanofluids was measured between 25 and 65 °C by using a Brookfield LVDV-II digital viscometer with a cone type spindle. Oleic acid as a surfactant with 0.3 vol% concentration was added to the nanofluids to prevent particle agglomeration. Different ultrasonication time (30 min for 0.05 vol% to 3 h for 1 vol%) was applied by a disruptor type ultra-sonicator with 20 kHz, 500 W power levels. They conducted the experiments with two different particle sizes of 13 and 50 nm and the vol. concentrations between 0.05–0.5%. They observed that the increase in viscosity for smaller size is larger compared to that of the bigger particles due to the availability of the higher surface area. Rudyak et al. [61] measured the viscosity of SiO_2–EG nanofluid with the particle sizes of 18.1, 28.3 and 45.6 nm. The measurements were performed by a Brookfield LVDV-II+ Brookfield Viscometer at 25 °C. They concluded that the SiO_2–EG nanofluid with smaller particles have higher viscosity than those with larger particles. Minakov et al. [62]

experimentally investigated the viscosity of SiO_2–water nanofluid with different particle sizes (10, 16, 25 and 100 nm). Experiments were carried out by Brookfield DV2T rheometer at 25 °C. They found that the viscosity of nanofluids increases with decreasing particle size.

Furthermore, results of several papers [63–67] indicated a irregular behavior in terms of particle size effect. Prasher et al. [63] conducted an experimental study on Al_2O_3–propylene glycol nanofluid for three different nanoparticle diameters (27, 40 and 50 nm). At the production stage, colloidal mixture was subjected to ultrasonication. A controlled stress rheometer was used for the viscosity measurements between 30 and 60 °C. Their results depicted that the relative viscosity has an inconclusive trend and it is much higher than the value that can be predicted by Einstein's model. They concluded that it is probably caused by the agglomeration of nanoparticles. Anoop et al. [64] measured the Al_2O_3–water nanofluid at 30 °C by using an Ubbelohde viscometer, which works on the principle of evaluating the time required for a particular quantity of fluid to pass through a capillary bore. The Al_2O_3 nanoparticles were dispersed in water by using an ultrasonicator. Their results indicated that the nanofluid with 45 and 150 nm particle sizes has similar relative viscosity at 2 and 4 wt% concentrations. But, the viscosity of the sample with 45 nm was higher than that with 150 nm particle size at 8 wt% concentration. Since the study provided the weight concentrations, they have been converted to vol. concentrations by using Eq. (8) to make them comparable with the other studies:

$$\varphi_{vol} = \frac{\varphi_{wt}\rho_{bf}}{\rho_{nf} + \varphi_{wt}(\rho_{bf} - \rho_{nf})} \qquad (8)$$

Meriläinen et al. [65] presented a detailed study on viscosity of Al_2O_3, MgO and SiO_2 nanofluids using HAAKE falling ball viscometer in a temperature range of 10–50 °C. They reported that the ratio of

nanofluid viscosity to the base fluid viscosity is found to be independent from temperature. Although they prepared the Al_2O_3 (8.2 ± 3.1 and 14–53 nm) and SiO_2 (6.5 ± 1.8, 65 ± 34 and 28–110 nm) nanofluids up to 4 vol%, the highest concentration of MgO (21 ± 10 and 15–47 nm) nanofluid was prepared as 2 vol% due to stability issues. They concluded that the average particle size does not have a significant effect on the viscosity of MgO and SiO_2 nanofluids. However, the viscosity of Al_2O_3 nanofluid increases with smaller particle size.

Oliveria et al. [66] suggested that the most effective method for preventing agglomeration during the preparation of the nanofluid samples is the high-pressure homogenizer method, which consists of two microchannels that divide the main stream into two sub streams. The both streams divided were then recombined in a reacting chamber in which significant increase in the velocity of pressurized liquid streams resulted in the formation of cavitation in the liquid. The high energy of cavitation was used to break the clusters of nanoparticles. They performed their experimental study with Ag–water nanofluid by altering the vol. concentration between 0.1–0.3% using two different particle sizes, namely 10 and 80 nm. Viscosity measurements were carried out at 25 °C by a cone plate viscometer. Their results indicated that the Ag–water nanofluid has not revealed a systematic behavior response to the particle size. Although the relative viscosity of the nanofluid with 80 nm particle size is higher than the one with 10 nm size for 0.1 and 0.3 vol% concentrations, the sample with 10 nm particle size showed higher relative viscosity value than the sample with 80 nm for 0.2 vol% concentration. Yousaf et al. [67] worked on the viscosity of Fe_3O_4–citric acid nanofluid with two different particle sizes (9 ± 3 and 20–30 nm) with the concentrations of 1–10% in wt. The Fe_3O_4–citric acid nanofluid with 20–30 nm was purchased, while the sample with 9 nm was synthesized in the laboratory by the co-

Legend:
- ◆ Prasher et al. [63], Al2O3/PG, 27 nm, 30 ˚C
- ■ Prasher et al. [63], Al2O3/PG, 40 nm, 30 ˚C
- ▲ Prasher et al. [63], Al2O3/PG, 50 nm, 30 ˚C
- × Nguyen et al. [49], Al2O3/water, 36 nm, 20 ˚C
- ✳ Nguyen et al. [49], Al2O3/water, 47 nm, 20 ˚C
- ◆ Chevalier et al. [53], SiO2/ethanol, 35 nm, AT
- ■ Chevalier et al. [53], SiO2/ethanol, 94 nm, AT
- ▲ Namburu et al. [51], SiO2/EG:Water, 20 nm, 20 ˚C
- × Namburu et al. [51], SiO2/EG:Water, 50 nm, 20 ˚C
- ✳ Namburu et al. [51], SiO2/EG:Water, 100 nm, 20 ˚C
- ● Oliveria et al. [66], Ag/water, 10 nm, AT
- + Oliveria et al. [66], Ag/water, 80 nm, AT
- − Esfe et al. [58], Fe/EG, 40 nm, 26 ˚C
- − Esfe et al. [58], Fe/EG, 70 nm, 26 ˚C
- ◆ Esfe et al. [58], Fe/EG, 100 nm, 26 ˚C
- − Agarwal et al. [60], Al2O3/kerosene, 13 nm, 25 ˚C
- − Agarwal et al. [60], Al2O3/kerosene, 50 nm, 25 ˚C
- ■ Esfe et al. [59], Fe/water, 37 nm, AT
- ▲ Esfe et al. [59], Fe/water, 71 nm, AT
- × Esfe et al. [59], Fe/water, 98 nm, AT
- ● Turgut et al. [50], Al2O3/water, 10 nm, 20 ˚C
- + Turgut et al. [50], Al2O3/water, 30 nm, 20 ˚C
- ✳ Rudyak et al. [61], SiO2/EG, 18.1 nm, 25 ˚C
- ● Rudyak et al. [61], SiO2/EG, 28.3 nm, 25 ˚C
- + Rudyak et al. [61], SiO2/EG, 45.6 nm, 25 ˚C

(0 - 100 nm)

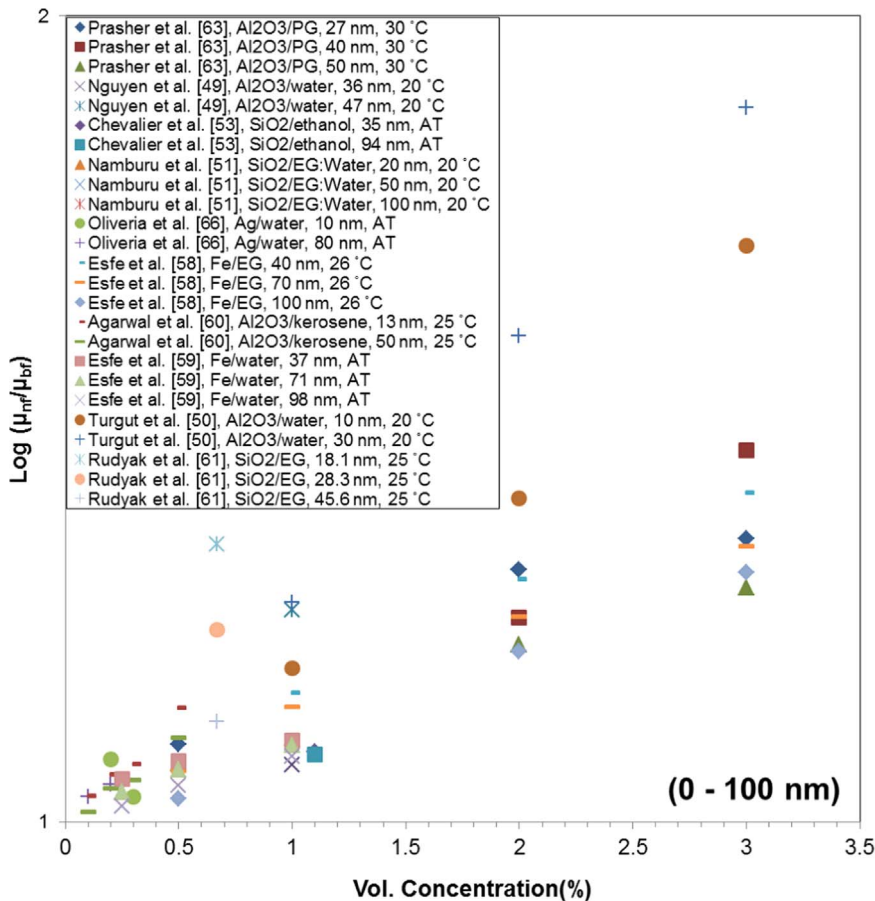Log (μ_{nf}/μ_{bf}) vs Vol. Concentration(%)

Fig. 3. Selected experimental data for the relationship between relative viscosity and vol. concentration.

precipitation method. Since the viscosity of the base fluid was not mentioned in this study, their experimental data was not included in Fig. 2 and Table 1. The viscosity of nanofluids was measured by a Brookfield viscometer with temperature ranges from 25 to 40 °C. Experimental viscosity value of the synthesized sample (smaller size) was higher than that of procured sample (larger size). However, the samples presented different viscosity trends. The viscosity of nanofluid with 20–30 nm particle size was found to increase with concentration, slowly and steadily. On the other hand, even the viscosity of nanofluid with 9 nm particle size indicated the same behavior with the larger sample size until 3.5 wt%. Beyond this point the viscosity values showed a significant increment. They explained that the nanoparticles with smaller sizes have larger surface areas and these nanosized particles have high energy surfaces since 50% of the atoms are at the surface and, therefore, surface properties and chemistry control the nanoparticles' behavior.

Figs. 3 and 4 are provided to understand particle size effect better in the light of vol. concentration and temperature. Fig. 3 presents the variation of selected relative viscosity values in 0—100 nm particle size range. It is shown that almost all experiments indicated relative viscosity increments with increasing vol. concentration, except Oliveira et al. [66] which reported a contradiction. Variations of relative viscosity values of selected studies for temperature variation are portrayed in Fig. 4. According to Fig. 4, temperature influences the relative viscosity, however any systematic behavior cannot be observed.

Comparative analysis of relative viscosity behavior with the particle size and other parameters are reduced and presented in Fig.s 5 and 6. The relative viscosity of nanofluids with 1 vol% concentration was compared as a function of particle size in Fig. 5. For the similar particle concentration and material, the relative viscosity of Turgut et al. [50] of 30 nm is 1.15 and 1.19 times higher than that of Nguyen et al. [49] of 36 nm and Anoop et al. [64] of 45 nm, respectively. Although, Turgut et al. [50] and Nguyen et al. [49] concluded that the relative viscosity of Al_2O_3 nanofluids increases with increase of particle size, findings of Esfe et al. [58,59] with Fe nanofluids contradicted as shown in Fig. 5. Additionally, Anoop et al. [64] and Chevalier et al. [53] obtained almost the same relative viscosity values for different particle sizes with Al_2O_3–water and SiO_2–ethanol nanofluids, respectively. It is hard to

deduce completely the effect of particle size on relative viscosity of nanofluids due to these contradictory results.

In Fig. 6, the relative viscosity of Al_2O_3–water suspension which is the most preferred nanofluid are interpreted in the temperature range of 20–25 °C. It is seen that the samples with 0–50 nm particle size ranges were preferred than the samples with larger sizes. Moreover, it can be stated from the viscosity results of Jarahnejad et al. [36] that employing the samples with larger particle size may cause a nonsystematic behavior. A proper particle size range could have been obtained for nanofluids by conducting more experimental study. Although stability and agglomeration are influenced by the particle size, the above mentioned studies are not complete enough for the interpretation. This makes it difficult to draw a clear conclusion for viscosity behavior that has a relationship with pressure drop.

3. Viscosity models with particle size for nanofluids

Many researches [28,53,69–72] considered the viscosity of nanofluids by comparing the experimental results with the classical models. They reported that classical models failed to show a good estimation of nanofluid viscosity due to not considering the particle size effect. However, several attempts were made on modeling the effective viscosity of nanofluids including the effect of particle size [73–78].

3.1. Theoretical models

Masoumi et al. [73] presented a viscosity model based on Brownian motion, considering the relative velocity between the nanoparticle and the base fluid of nanofluids. The developed model included five parameters (vol. concentration, particle size, temperature, nanoparticle density, and base fluid physical properties) as shown in Eq. (9). The distance between the centers of particles (δ) is evaluated from Eq. (10) which was developed by Sommerfeld [79]. The correction factor (C) was calculated from Eq. (11) to account for simplified assumptions.

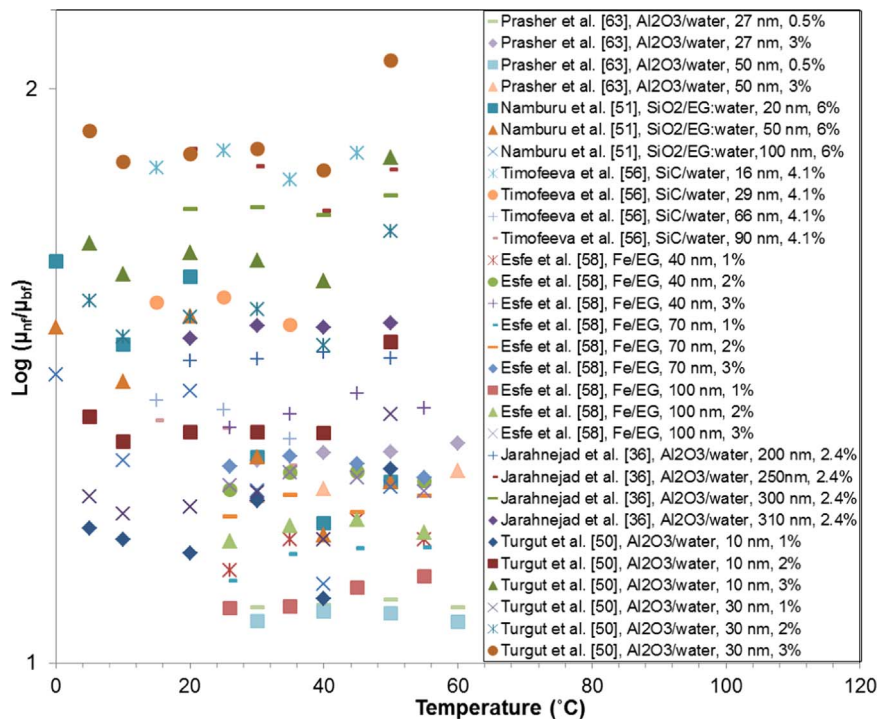$$\mu_{nf} = \mu_{bf} + \frac{\rho_p V_B d_p^2}{72C\delta} \qquad (9)$$

Fig. 4. Selected experimental data for the relationship between relative viscosity and temperature.

Legend:
- Prasher et al. [63], Al2O3/water, 27 nm, 0.5%
- Prasher et al. [63], Al2O3/water, 27 nm, 3%
- Prasher et al. [63], Al2O3/water, 50 nm, 0.5%
- Prasher et al. [63], Al2O3/water, 50 nm, 3%
- Namburu et al. [51], SiO2/EG:water, 20 nm, 6%
- Namburu et al. [51], SiO2/EG:water, 50 nm, 6%
- Namburu et al. [51], SiO2/EG:water,100 nm, 6%
- Timofeeva et al. [56], SiC/water, 16 nm, 4.1%
- Timofeeva et al. [56], SiC/water, 29 nm, 4.1%
- Timofeeva et al. [56], SiC/water, 66 nm, 4.1%
- Timofeeva et al. [56], SiC/water, 90 nm, 4.1%
- Esfe et al. [58], Fe/EG, 40 nm, 1%
- Esfe et al. [58], Fe/EG, 40 nm, 2%
- Esfe et al. [58], Fe/EG, 40 nm, 3%
- Esfe et al. [58], Fe/EG, 70 nm, 1%
- Esfe et al. [58], Fe/EG, 70 nm, 2%
- Esfe et al. [58], Fe/EG, 70 nm, 3%
- Esfe et al. [58], Fe/EG, 100 nm, 1%
- Esfe et al. [58], Fe/EG, 100 nm, 2%
- Esfe et al. [58], Fe/EG, 100 nm, 3%
- Jarahnejad et al. [36], Al2O3/water, 200 nm, 2.4%
- Jarahnejad et al. [36], Al2O3/water, 250nm, 2.4%
- Jarahnejad et al. [36], Al2O3/water, 300 nm, 2.4%
- Jarahnejad et al. [36], Al2O3/water, 310 nm, 2.4%
- Turgut et al. [50], Al2O3/water, 10 nm, 1%
- Turgut et al. [50], Al2O3/water, 10 nm, 2%
- Turgut et al. [50], Al2O3/water, 10 nm, 3%
- Turgut et al. [50], Al2O3/water, 30 nm, 1%
- Turgut et al. [50], Al2O3/water, 30 nm, 2%
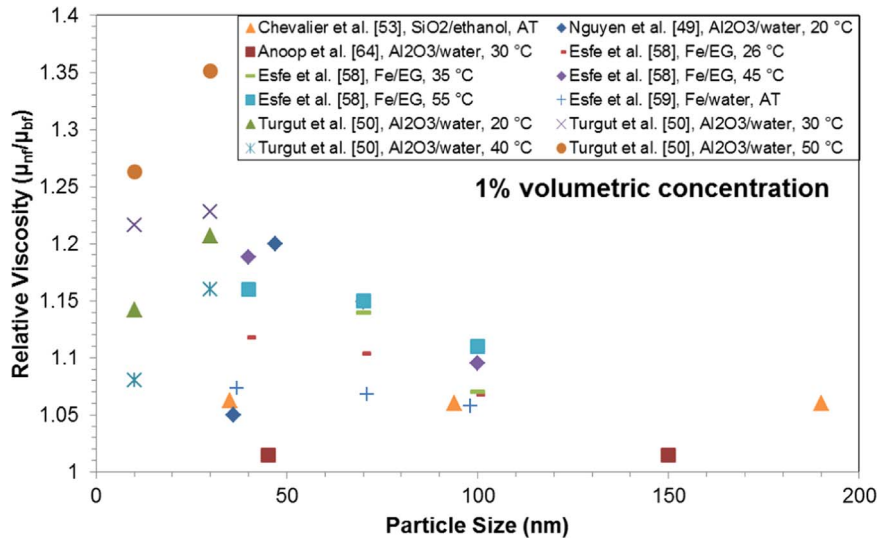- Turgut et al. [50], Al2O3/water, 30 nm, 3%

Fig. 5. Selected experimental data for the relationship between relative viscosity (μ_{nf}/μ_{bf}) and particle size for nanofluids with 1% vol. concentration.

$$\delta = \sqrt[3]{\frac{\pi}{6\varphi}}d_p \tag{10}$$

$$C = \mu_{bf}^{-1}(a\varphi + b) \tag{11}$$

Hosseini et al. [74] developed another viscosity model based on the experimental data of Nguyen et al. [49] for water based Al₂O₃ nanofluid with the influence of vol. concentration, nanoparticle size, thickness of capping layer of the nanoparticles and temperature. They considered a least-squares regression to determine the model parameters, where h is the hydrodynamic vol. concentration of Al₂O₃ nanoparticles, r is the thickness of the capping layer, d_p is the size of nanoparticle, T is the temperature of nanofluid and T_o is the reference temperature, m is the constant that depends on the system properties and α, ω, γ are empirical constants obtained from the experimental data.

$$\frac{\mu_{nf}}{\mu_{bf}} = \exp\left[m + \alpha\left(\frac{T}{T_0}\right) + \omega(\varphi_h) + \gamma\left(\frac{d_p}{1 + r}\right)\right] \tag{12}$$

3.2. Empirical models

Azmi et al. [75] proposed a viscosity model by using different experimental data in the literature on water-based nanofluids of Al₂O₃, CuO, SiO₂, ZnO, and TiO₂ with particle sizes ranging from 20 to 170 nm and vol. concentration lower than 4%. The model was dependent on the effects of vol. concentration, temperature and particle size on the effective viscosity of nanofluids, where C_I is an empirical constant and the exponents α, λ, and σ are equal to 11.3, 0.038 and 0.061, respectively.

$$\frac{\eta_{nf}}{\eta_{bf}} = C_1\left(1 + \frac{\varphi}{100}\right)^{\alpha}\left(1 + \frac{T_{nf}}{100}\right)^{-\lambda}\left(1 + \frac{d_p}{170}\right)^{-\sigma} \tag{13}$$

Khanafer and Vafai [76] developed a general viscosity correlation for the effective viscosity of water based Al₂O₃ nanofluid from curve fitting of the experimental data [49,64,80,81] existing in the literature. The model is valid for Al₂O₃ nanofluids with temperatures between 20 and 70 °C, nanoparticle diameters between 13 and 131 nm and vol. concentrations between 1% and 9%.
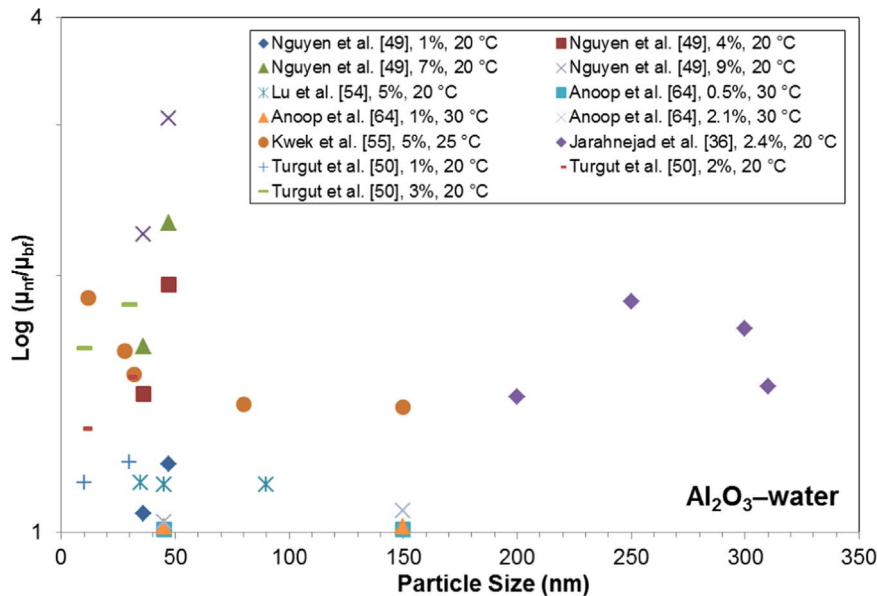

Fig. 6. Selected experimental data for the relationship between relative viscosity (μ_{nf}/μ_{bf}) and particle size for Al₂O₃–water nanofluids in the temperature range of 20 and 30 °C.

$$\mu_{nf} = -0.4491 + \frac{28.837}{T} + 0.574\varphi - 0.1634\varphi^2 + 23.053\frac{\varphi^2}{T^2}$$
$$+0.0132\varphi^3 - 2354.735\frac{\varphi}{T^3} + 23.498\frac{\varphi^2}{d_p^2} - 23.498\frac{\varphi^2}{d_p^2} \tag{14}$$

Corcione [77] formulated a viscosity correlation shown in Eq. (15). He considered various experimental data of nanofluids consisting of Al_2O_3, TiO_2, SiO_2, and Cu nanoparticles where d_p is the particle size, M is the molecular weight of the base fluid, ρ_f is the mass density of base fluid at temperature $T_o = 293$ K, N is the Avogadro's number ($N = 6.022 \times 10^{23}$ mol^{-1}) and d_f is the equivalent diameter of a base fluid molecule (Eq. (16)). Their correlation is valid for a temperature range from 293 to 333 K, vol. concentration range from 0.1% to 7.1% and a particle size ranging between 25 and 200 nm.

$$\frac{\mu_{nf}}{\mu_{bf}} = \frac{1}{1 - 34.87\left(\frac{d_p}{d_f}\right)^{-0.3}\varphi^{1.03}} \tag{15}$$

$$d_f = 0.1\left(\frac{6M}{N\pi\rho_f}\right)^{1/3} \tag{16}$$

Sekhar and Sharma [78] presented a regression equation including the effect of particle concentration, particle size and temperature of the base fluid. It is based on the experimental data [82–85] from the literature. The correlation is valid in the range of $13 < d_p < 100$ nm particle size, $20 < T_{nf} < 50$ °C and $0.01 < \varphi < 4\%$ vol. concentration. They observed that the model was in a good agreement with the experimental data of different authors with a deviation of −10 to +18%.

$$\frac{\mu_{nf}}{\mu_{bf}} = 0.935\left(1 + \frac{T_{nf}}{70}\right)^{0.5602}\left(1 + \frac{d_p}{80}\right)^{-0.05915}\left(1 + \frac{\varphi}{100}\right)^{10.51} \tag{17}$$

Different viscosity models including the particle size effect have been discussed above. It is seen that available models are valid for a limited range in terms of the critical variables. Therefore, it can be concluded that more comprehensive models need to be developed with wide operation ranges for the clear determination of nanofluids' viscosity behavior. The particle size and concentration, aggregation and the temperature must be considered simultaneously for the model development. More thorough experiments including a wide range of particle sizes need to be carried out in the future for reaching universal models.

4. Concluding remarks

Nanofluid related studies keep growing exponentially for the last two decades. However, commercialized application of the subject so far is not common, and many attempts are still being made by the scientific community. Utilized nanofluids in the existing literature show varying viscosity results due to the production method, nanoparticle and base fluid pairing, surfactant and measurement method. One of the prominent parameters which influences the viscosity of nanofluids is the particle size. Nonetheless, the number of studies on the effect of particle size is inadequate.

In this review, papers focused systematically on the size effect on nanofluid viscosity have been considered. It has been observed that there are discrepancies between discussed studies on viscosity values for different particle sizes even when their nanoparticle concentrations are similar. It is also evident that, according to collected data, the relative viscosity can increase up to 40% [56] or decrease up to 37% [49] by merely altering the particle size for the same nanofluid samples. Following are the conclusions drawn from this study that includes some possible reasons of these discrepancies:

- Some of the considered papers indicated an increment in viscosity

values with decreasing particle size, while the others indicated an increment with increase of particle size.
- Production and measurement methods are different among the various studies available in the literatures. This variation restrains to draw a clear conclusion about the particle size effect on viscosity of nanofluids.
- Particle size range of the each study was limited. A remarkable number of discussed papers employed only two or three different particle size, which makes it difficult to have an interpretation about the effect of particle size.
- Among the evaluated studies, it is realized that information about the surfactant types is insufficient or missing. Additionally, evaluated studies are lacking in using surfactant at high temperatures. This is important, since, the physical phenomena between surfactant and nanoparticles may be influenced at high temperatures.
- Even in some cases, particle shape(s) is not introduced in literature. However, the effect of particle size again depends on the particle shape. If the particle size or diameters are the same but the shape is different as being spherical and cylindrical, then viscosity and other properties will differ.
- Since, stability and agglomeration are directly influenced by the particle size distribution of the nanofluid, they need to be considered prior to performing a viscosity study. Size distribution of nanoparticles in liquid should be provided rather than providing size distribution of nanoparticles in powder form.

For future works, wide and systematic range of parameters in terms of particle size, particle concentration and temperature should be employed for eliminating the discrepancies of the particle size effect. This effort will be helpful to develop new well-accepted models. Moreover, presentations of production and measurement methods and type and quantity of surfactant are important for providing better comparisons. Lastly, studies related to the degradation of surfactants functional ability at high temperature and more rigorous stability analyses are needed.

Acknowledgements

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H.D. Koca et al.   Renewable and Sustainable Energy Reviews xxx (xxxx) xxx–xxx

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